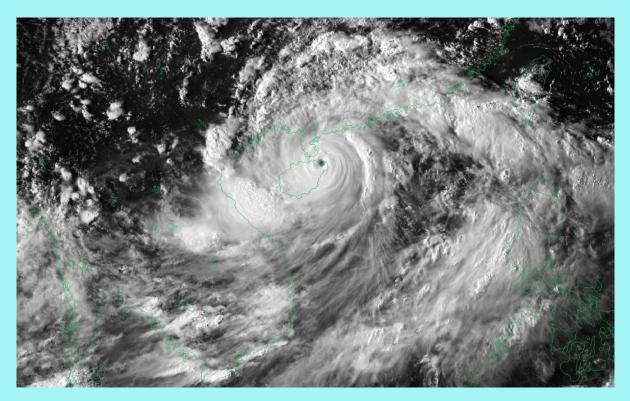
Annual Report on the Activities of the RSMC Tokyo - Typhoon Center 2024



TY YAGI 09 UTC, 6 September 2024

Japan Meteorological Agency

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Introduction

The RSMC Tokyo - Typhoon Center (referred to here as the Center) is a Regional Specialized Meteorological Centre (RSMC) that carries out specialized activities in analysis, tracking and forecasting of western North Pacific tropical cyclones (TCs) within the framework of the World Weather Watch (WWW) Programme of the World Meteorological Organization (WMO). The Center was established at the headquarters of the Japan Meteorological Agency (JMA) in July 1989 following a designation by the WMO Executive Council at its 40th session (Geneva, June 1988).

The Center conducts the following operations on a routine basis:

- (1) Preparation of information on the formation, movement and development of TCs and associated meteorological phenomena
- (2) Preparation of information on synoptic-scale atmospheric situations that affect the behavior of TCs
- (3) Provision of the above information to National Meteorological Services (NMSs), and in particular to United Nations Economic and Social Commission for Asia and the Pacific (ESCAP)/WMO Typhoon Committee Members, in appropriate formats for operational processing

In addition to the routine services outlined above, the Center distributes a series of reports entitled *Annual Report on the Activities of the RSMC Tokyo - Typhoon Center* as operational references for the NMSs concerned. The reports summarize the activities of the Center and review the TCs of the preceding year.

In this issue covering 2024, Chapter 1 outlines routine operations performed at the Center and its operational products, while Chapter 2 reports on its major activities in 2024. Chapter 3 describes atmospheric and oceanic conditions in the tropics and notes the highlights of TC activity in 2024. Chapter 4 presents verification statistics relating to operational forecasts (i.e., official forecasts), results from JMA's numerical weather prediction (NWP) models and other guidance models, Atmospheric Motion Vector (AMV) based Sea-surface Wind (ASWind) data, TC central pressure estimates based on satellite microwave observations and storm surge predictions. Best track data for 2024 TCs of tropical storm (TS) intensity or higher are shown in table and chart form in the appendices.

Chapter 1 Operations at the RSMC Tokyo - Typhoon Center in 2024

The Center's area of responsibility covers the western North Pacific and the South China Sea $(0^{\circ}-60^{\circ}\text{N}, 100^{\circ}-180^{\circ}\text{E})$ including marginal seas and adjacent land areas (Figure 1.1). The Center carries out analysis and forecasting in relation to TCs in the area and also provides the relevant NMSs with RSMC products via the Global Telecommunication System (GTS), the Aeronautical Fixed Telecommunication Network (AFTN), the Internet and other media.

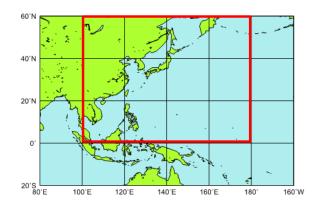


Figure 1.1 Area of responsibility of the RSMC Tokyo -Typhoon Center

1.1 Analysis

TC analysis is performed eight times a day at 00, 03, 06, 09, 12, 15, 18 and 21 UTC, and begins with determination of the TC's center position. Cloud imagery from Himawari-8/9 and microwave imagery from various polar orbiting satellites are the principal sources for this determination, especially for TCs migrating over data-sparse ocean areas. Information on the TC's direction and speed of movement is extracted primarily from six-hourly displacement vectors of the center position.

The maximum sustained wind speed in the vicinity of the TC's center is determined mainly from the Current Intensity (CI) number, which is derived from satellite imagery using the Dvorak method. The central pressure of the TC is then determined from the maximum sustained wind speed with the assumption of a certain pressure profile around the TC. The radii of circles representing winds with speeds exceeding 30 and 50 knots are determined mainly from surface observation, Advanced Scatterometer (ASCAT) observation, HY Scatterometer (HSCAT) observation and ASWind data derived from satellite images in the vicinity of the TC. The size of the central dense overcast area of the TC as observed in satellite imagery is also referenced to determine the radius of 50-knot wind speed circles.

1.2 Forecast

The Center issues TC track forecasts with probability circles, as well as intensity forecasts for tropical depressions (TDs) expected to reach tropical storm (TS) intensity within 24 hours and for TCs with TS intensity or higher up to 120 hours ahead. As a primary basis for TC track forecasts, JMA implements NWP using the Global Spectral Model (GSM) and the Global Ensemble Prediction System (GEPS). The GSM (TQ959, upgraded on 14 March 2023) has a horizontal resolution of approximately 13 km and 128 vertical layers, while GEPS (TQ479; upgraded on 14 March 2023) has 51 members with a horizontal resolution of

approximately 27 km and the same number of vertical layers. GSM horizontal resolution was enhanced from 20 to 13 km in 2023. Further details and recent model improvements are detailed in Appendix 7. Since 2015 the Center has mainly employed a consensus method for TC track forecasts. This approach involves taking the mean of predicted TC positions from multiple deterministic models, including the GSM and other NWP centers' models, such as European Centre for Medium-Range Weather Forecasts (ECMWF), National Centers for Environmental Prediction (NCEP) and United Kingdom Met Office (UKMO) global models.

A probability circle shows the range into which the center of a TC is expected to move with 70% probability at each validation time. The radius for all forecast periods up to 120 hours is determined by the multiple ensemble method, which is solely according to the confidence level based on the cumulative ensemble spread calculated using multiple ensemble prediction systems (EPSs) consisting of ECMWF, NCEP and UKMO global EPSs in addition to GEPS.

In relation to TC intensity, the Center began providing TC intensity forecasts with extended lead times of up to 120 hours in March 2019, based on several tropical cyclone intensity forecast guidance products including Typhoon Intensity Forecasting scheme based on Statistical Hurricane Intensity Prediction Scheme (SHIPS), which is known as TIFS and Logistic Growth Equation Model (LGEM). These schemes were developed by JMA and Meteorological Research Institute (MRI) of JMA. The Center also refers to Hurricane Weather Research and Forecast model (HWRF) and Hurricane Analysis and Forecasting System (HAFS) in NCEP.

1.3 Provision of RSMC Products

The Center prepares and distributes the RSMC bulletins listed below via the GTS or the AFTN when:

- a TC of TS intensity or higher exists in the Center's area of responsibility
- a TD is expected to reach or exceed TS intensity in the area within 24 hours

RSMC products are issued while any TC of TS intensity or higher or any TD expected to reach or exceed TS intensity within 24 hours exists in the Center's area of responsibility. Appendix 6 denotes the code forms of the bulletins.

(1) RSMC Tropical Cyclone Advisory (WTPQ50-55 RJTD: via GTS)

The RSMC Tropical Cyclone Advisory is issued eight times a day after observations made at 00, 03 06, 09, 12, 15, 18 and 21 UTC, and reports the following elements in analysis and in 24-, 48-, 72-, 96- and 120-hour forecasts for TCs:

Analysis Center position

Accuracy of center position determination

Direction and speed of movement

Central pressure

Maximum sustained wind speed (10-minute average)

Maximum gust wind speed

Radii of wind areas over 50 and 30 knots

24-, 48-, 72-, 96- and 120-hour Forecasts¹ Center position and radius of probability circle

Direction and speed of movement

Central pressure

Maximum sustained wind speed (10-minute average)

Maximum gust wind speed

(2) RSMC Guidance for Forecast by GSM (FXPQ20-25 RJTD: via GTS)

The RSMC Guidance for Forecast by GSM reports the results of predictions made by the GSM; which is run four times a day with initial analyses at 00, 06, 12 and 18 UTC. The guidance presents six-hourly GSM predictions for TCs up to 132 hours ahead and reports the following elements:

NWP prediction (T = 006 to 132) Center position

Central pressure*

Maximum sustained wind speed*

(3) RSMC Guidance for Forecast by GEPS (FXPQ30-35 RJTD: via GTS)

The RSMC Guidance for Forecast by GEPS reports the results of predictions made by the GEPS; which is run four times a day with initial analyses at 00, 06, 12 and 18 UTC. The guidance presents the ensemble mean of GEPS six-hourly predictions up to 132 hours ahead and reports the following elements:

NWP prediction (T = 006 to 132) Center position

Central pressure*

Maximum sustained wind speed*

(4) SAREP (IUCC10 RJTD: via GTS)

The SAREP in BUFR format reports the results of TC analysis including intensity information (i.e., the CI number) based on Himawari-8/9 imagery analysis using the Dvorak method. It is issued shortly after observations made for TCs with TS intensity or higher at 00, 03, 06, 09, 12, 15, 18 and 21 UTC (TDs expected to reach TS intensity or higher within 24 hours at 00, 06, 12 and 18 UTC), and reports the following elements:

Satellite imagery analysis Center position

Accuracy of center position determination

Direction and speed of movement Mean diameter of overcast cloud

Apparent past 24-hour change in intensity**

Dvorak Intensity (CI, T, DT, MET, PT number) **

Cloud pattern type of the DT number**

Trend of past 24-hour change**

Cloud pattern type of the PT number**

Type of the final T-number**

¹ At 03, 09, 15 and 21 UTC, 24-, 45-, 69-, 93- and 117-hour forecasts for TCs are reported.

^{*} Predictions of these parameters are given as deviations from those at the initial time.

^{*} Predictions of these parameters are given as deviations from those at the initial time.

^{**} Reported only at 00, 06, 12 and 18 UTC

BUFR/CREX templates for translation into table-driven code forms are provided on the WMO website at https://community.wmo.int/activity-areas/wis/wis-manuals. The SAREP is provided in text format on the Numerical Typhoon Prediction (NTP) website (see 1.7).

(5) RSMC Prognostic Reasoning (WTPQ30-35 RJTD: via GTS)

The RSMC Prognostic Reasoning report provides brief reasoning for TC analysis and forecasts, and is issued at 00, 06, 12 and 18 UTC following the issuance of the RSMC Tropical Cyclone Advisory. The bulletin provides general comments on current positioning, intensity and related changes, synoptic situations such as those of the subtropical high and atmospheric/oceanographic fields, reasoning behind TC track and intensity forecasts (including details of methodology and guidance models), and relevant remarks in plain language.

(6) RSMC Tropical Cyclone Best Track (AXPQ20 RJTD: via GTS)

The RSMC Tropical Cyclone Best Track report provides post-analysis data on TCs of TS intensity or higher. It reports the center position, the central pressure and the maximum sustained wind speed. The best track for each TC is usually finalized three months after the termination of related issuance of the above RSMC bulletins.

(7) <u>Tropical Cyclone Advisory for SIGMET</u> (FKPQ30-35 RJTD: via AFTN, and IWXXM 3.0 format: via AMHS (see 1.4))

As a Tropical Cyclone Advisory Centre (TCAC) within the framework of the International Civil Aviation Organization (ICAO), the Center provides Tropical Cyclone Advisory (TCA) for SIGMET to Meteorological Watch Offices (MWOs) in order to support their preparations of SIGMET information on TCs. These advisories include the following elements in analysis and in 6-, 12-, 18- and 24-hour forecasts:

Analysis Center position

Observed cumulonimbus cloud Direction and speed of movement

Changes in intensity Central pressure

Maximum sustained wind speed (10-minute average)

Forecast Center position

Maximum sustained wind speed (10-minute average)

1.4 Tropical Cyclone Advisory for SIGMET

The Center provides text-format and graphical TCAs in its role as the ICAO TCAC. These include the horizontal extent of cumulonimbus cloud and cloud top height associated with TCs potentially affecting aviation safety, in addition to text-format TCA information. Both text-format and graphical TCAs and related specifications are provided online for users via linkage from the NTP website (see 1.7), and graphical TCAs are also provided to World Area Forecast Centres (WAFCs).

In November 2020, TCAs in IWXXM 3.0 format were introduced and shared on the TCAC Tokyo website, followed by transmission via Air Traffic Services (ATS) Message Handling Services (AMHS) in March 2022. The IWXXM format is detailed in Guidelines for the Implementation of OPMET Data Exchange Using IWXXM, Third Edition (May 2019), ICAO.

1.5 WIS Global Information System Centre Tokyo Server

As designated at the Sixteenth WMO Congress in June 2011, the Center introduced Data Collection or Production Centre (DCPC) service under the Global Information System Centre (GISC) Tokyo for the WMO Information System (WIS) in August 2011. It provides NWP products such as data on predicted fields in grid-point-value (GPV) form and observational values through WIS Data Discovery, Access and Retrieval (DAR) via a GISC Tokyo server (https://www.wis-jma.go.jp/). GSM products with resolution of 0.5 and 0.25 degrees (surface layer) and JMA SATAID (SATellite Animation and Interactive Diagnosis; https://www.wis-jma.go.jp/cms/sataid/) Service are also available from the server through WIS DAR. All products available via the server are listed in Appendix 8.

1.6 RSMC Tokyo - Typhoon Center Website

The RSMC Tokyo - Typhoon Center Website provides TC advisories on a real-time basis and a wide variety of products including TC analysis archives, technical reviews and annual reports on the Center's activities at https://www.jma.go.jp/jma/jma-eng/jma-center/rsmc-hp-pub-eg/RSMC_HP.html. Since November 2012, the website provides experimental TC advisory information in Common Alert Protocol (CAP) format.

1.7 Numerical Typhoon Prediction Website

Since October 2004, the Center has operated the Numerical Typhoon Prediction (NTP) website to assist the NMSs of Typhoon Committee Members in improving their TC forecasting and warning services. The site provides TC track predictions and weather maps of deterministic global NWP models from nine centers (Bureau of Meteorology (BoM, Australia), China Meteorological Administration (CMA, China), Canadian Meteorological Centre (CMC, Canada), Deutscher Wetterdienst (DWD, Germany), ECMWF, Korea Meteorological Administration (KMA, Republic of Korea), NCEP (USA), UKMO (UK) and JMA), ensemble TC track predictions of global EPSs from four centers (ECMWF, NCEP, UKMO and JMA) and a wide variety of products including the results of the Center's TC analysis, upper-air analysis, ocean analysis, storm surge and ocean wave forecasting. All products available on the website are listed in Appendix 9.

1.8 TC Communication platform

The Center's TC communication platform (developed and maintained since July 2019) supports enhanced interaction between operational forecasters in the NMSs of Typhoon Committee Members and the Center, as well as sharing of early-announcement and advance-notice updates. Full-scale operation of the platform was started during the 2021 typhoon season and related discussions have helped to clarify TC status and forecasts. All services provided on the platform are listed in Appendix 9.

Chapter 2 Major Activities of the RSMC Tokyo - Typhoon Center in 2024

2.1 Provision of RSMC Products

The Center provides operational products for TC analysis and forecasting to NMSs via the GTS, the AFTN and other networks. Monthly and annual totals of products issued in 2024 are listed in Table 2.1.

Table 2.1 Monthly and annual totals of products issued by the RSMC Tokyo - Typhoon Center in 2024

Product	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
IUCC10	0	0	0	0	59	3	86	232	266	176	252	21	1095
WTPQ30-35	0	0	0	0	39	2	51	128	156	101	137	14	628
WTPQ50-55	0	0	0	0	78	3	100	255	306	198	269	27	1236
FXPQ20-25	0	0	0	0	36	1	33	100	99	75	70	13	427
FXPQ30-35	0	0	0	0	36	1	33	100	99	75	70	13	427
FKPQ30-35	0	0	0	0	39	1	49	125	150	97	132	13	606
AXPQ20	4	0	0	0	0	0	0	1	1	2	4	10	22

Notes:

IUCC10 RJTD	SAREP (BUFR format)
WTPQ30-35 RJTD	RSMC Prognostic Reasoning
WTPQ50-55 RJTD	RSMC Tropical Cyclone Advisory
FXPQ20-25 RJTD	RSMC Guidance for Forecast by GSM
FXPQ30-35 RJTD	RSMC Guidance for Forecast by GEPS
FKPQ30-35 RJTD	Tropical Cyclone Advisory for SIGMET
AXPQ20 RJTD	RSMC Tropical Cyclone Best Track

2.2 Publications

In November 2024, the Center published the *Annual Report on the Activities of the RSMC Tokyo - Typhoon Center 2023*. The publication is available on the Center's website at https://www.jma.go.jp/jma/jma-eng/jma-center/rsmc-hp-pub-eg/RSMC HP.html.

2.3 Typhoon Committee Attachment Training

In its role as an RSMC, the Center has organized ESCAP/WMO Typhoon Committee Attachment Training annually since 2001 with the support of the WMO Tropical Cyclone Programme and the Typhoon Committee in order to advance the TC analysis and forecasting capacity of Typhoon Committee Members. The course is set under the Category 2 Unit of Tropical Cyclone Forecast Competency as per the Typhoon Committee Region specifications of the Typhoon Committee Operational Manual (TOM).

The 23rd training course was held from 15 to 26 January 2024, both in person and online, with attendees from seven Typhoon Committee Members (Hong Kong China, Lao PDR, Macao China, Malaysia, the Philippines, the Republic of Korea, and Viet Nam), two from the Panel on Tropical Cyclones (PTC) (Saudi Arabia and Sri Lanka), and online participants. This in-person attendance followed three years of online-only implementation due to COVID-19.

The course was enhanced with hands-on training for interactive exercises on satellite analysis techniques and Dvorak analysis. Presentations included content from researchers and Japanese experts from the Typhoon Committee's Hydro and Disaster Risk Reduction group, and from weathercasting professionals, to give a broad perspective and contribute to the UN's EW4All initiative.

The Center is committed to improving forecasting competence, and thereby the capacity of Meteorological Services in the Typhoon Committee region, via training to meet various regional needs, including basic application, state-of-the-art tropical cyclone forecasting and monitoring techniques/methodologies.

2.4 Other Activities in 2024

2.4.1 Upgrades of Numerical Typhoon Prediction Website

The changes outlined below were made to the NTP website in 2024.

- (1) The upgraded <u>Tropical cyclone intensity forecast guidance (TIFS) monitor</u> and <u>Tropical cyclone</u> forecast verification tool became newly available in March 2024.
- (2) Hurricane Analysis and Forecast System (HAFS) became newly available on the TIFS monitor in October 2024.
- (3) <u>JMA GSM extended deterministic track prediction</u> up to 264 hours ahead at 00 and 12 initial time (UTC), became newly available in July 2024.

Chapter 3 Summary of the 2024 Typhoon Season

In 2024, 26 TCs of TS intensity or higher formed over the western North Pacific and the South China Sea. This total was almost the same as the climatological normal² frequency of 25.1. Among these 26 TCs, 13 reached Typhoon (TY) intensity, 3 reached severe tropical storm (STS) intensity and 10 reached TS intensity (Table 3.1).

Table 3.1 List of tropical cyclones reaching TS intensity or higher in 2024

	Tropical Cyclo	ne	I	Duratio	on	(UTC)		Minim	um Cen	tral Pres	sure	Max Wind
				(TS o	r h	igher)		(UTC)	lat(N)	long(E)	(hPa)	(kt)
TY	Ewiniar	(2401)	251200	May	-	301800	May	270000	15.8	122.8	970	75
TS	Maliksi	(2402)	310000	May	-	311200	May	310000	19.8	112.6	998	35
TY	Gaemi	(2403)	200000	Jul	-	261800	Jul	240300	23.9	122.9	935	90
STS	Prapiroon	(2404)	210000	Jul	-	231200	Jul	220600	20.1	108.5	985	55
STS	Maria	(2405)	071800	Aug	_	120600	Aug	081800	29.8	145.6	980	55
TS	Son-tinh	(2406)	110000	Aug	-	131200	Aug	111200	28.8	154.5	994	40
TY	Ampil	(2407)	121200	Aug	-	190000	Aug	151200	31.6	140.8	950	85
TS	Wukong	(2408)	130000	Aug	-	141200	Aug	130000	26.4	150.1	1002	35
TS	Jongdari	(2409)	181200	Aug	-	210000	Aug	190600	26.3	126.0	996	40
TY	Shanshan	(2410)	211800	Aug	-	301200	Aug	271500	28.8	130.3	935	95
TY	Yagi	(2411)	010600	Sep	-	081200	Sep	050000	19.0	115.8	915	105
TS	Leepi	(2412)	050000	Sep	-	061200	Sep	050000	32.2	145.9	1002	35
TY	Bebinca	(2413)	101200	Sep	-	170000	Sep	150000	29.6	127.2	965	75
TS	Pulasan	(2414)	151200	Sep	-	210600	Sep	170000	20.0	140.1	992	45
TS	Soulik	(2415)	181800	Sep	_	191200	Sep	181800	17.5	110.0	992	35
TS	Cimaron	(2416)	240600	Sep	-	260600	Sep	241200	27.9	135.1	998	35
TY	Jebi	(2417)	270000	Sep	-	021200	Oct	010000	32.6	141.7	980	65
TY	Krathon	(2418)	280000	Sep	-	031200	Oct	010000	20.6	119.6	920	105
TS	Barijat	(2419)	060600	Oct	-	110000	Oct	101800	39.2	154.2	985	45
STS	Trami	(2420)	211800	Oct	_	271800	Oct	260600	17.1	111.9	970	60
TY	Kong-rey	(2421)	241800	Oct	-	011200	Nov	300000	19.1	124.8	925	100
TY	Yinxing	(2422)	031200	Nov	-	120600	Nov	070600	18.5	122.4	945	100
TY	Toraji	(2423)	090600	Nov	-	141200	Nov	101800	15.9	123.2	980	70
TY	Man-yi	(2424)	081800	Nov	-	191200	Nov	160000	12.6	126.7	920	105
TY	Usagi	(2425)	111800	Nov	_	160000	Nov	140000	17.2	123.1	940	95
TS	Pabuk	(2426)	220600	Dec	-	241800	Dec	220600	10.5	114.2	1002	35

3.1 Atmospheric and Oceanographic Conditions in the Tropics

In association with the El Niño event that began in boreal spring (March – May) 2023, positive sea surface temperature (SST) anomalies were observed over most of the region, with remarkably positive anomalies from central to eastern parts in boreal winter (December 2023 – February 2024). Tropical convection was enhanced over the equatorial Pacific and the western Indian Ocean, and suppressed from the eastern Indian Ocean to Indonesia.

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 $^{^2}$ The base period for the climatological normal is 1991-2020. The normal was updated in early 2021 based on 30-year data.

Even though the El Niño event ended in boreal spring 2024, remarkably positive SST anomalies were still observed from western to central parts of the equatorial Pacific as the event had persisted since boral spring 2023. In accordance with SST conditions, tropical convective activity was enhanced from the western Indian Ocean to the south of New Guinea Island, and suppressed from the Bay of Bengal to the east of the Philippines.

Boreal summer (June – August) saw remarkably positive SST anomalies in western parts and negative anomalies in eastern parts of the equatorial Pacific. In the Indian Ocean, remarkably positive SST anomalies were observed over a wide area (Figure 3.1 (a)). Since warmer SSTs tend to occur in the tropical Indian Ocean after El Niño events, this SST pattern may be associated with the expired El Niño event. Tropical convective activity was enhanced from eastern North Africa to the western Indian Ocean, from western South Asia to Indonesia and to the southeast of Japan, and suppressed over a wide area of the tropical North Pacific (Figure 3.1 (b)). In the lower troposphere, anti-cyclonic circulation anomalies were seen from the East China Sea to the subtropical western North Pacific in association with enhanced convection from the Indian Ocean to the Maritime Continent, indicating that the southwestward extension of the North Pacific subtropical high was stronger than normal (Figure 3.1 (c)). The anti-cyclonic circulation anomalies observed over the tropical Pacific indicate unfavorable conditions for typhoons, and may have contributed to the reduced number of formations observed until July (see 3.2).

In boreal autumn (September – November), remarkably positive SST anomalies were observed in the western part of the equatorial Pacific, and negative anomalies extended from eastern to central parts. In the Indian Ocean, remarkably positive SST anomalies were still extensively observed, except in areas off Somalia and a few elsewhere. Tropical convective activity was enhanced in the central South Indian Ocean and from the northern South China Sea to the subtropical western North Pacific, and suppressed from the western to central equatorial Pacific. In the lower troposphere, cyclonic circulation anomalies straddling the equator were seen in the eastern Pacific and the Indian Ocean, and anti-cyclonic circulation anomalies straddling the equator were seen from the western to central Pacific.

Atmospheric and oceanographic charts (including monthly mean streamlines at 850 and 200 hPa, outgoing longwave radiations (OLRs)³ with related anomalies, and monthly mean SSTs with related anomalies for the western North Pacific and the South China Sea) are provided on the Tokyo Climate Center website at

https://www.data.jma.go.jp/tcc/tcc/products/clisys/figures/db_hist_mon_tcc.html and https://www.data.jma.go.jp/tcc/tcc/products/elnino/ocean/index_tcc.html.

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³ OLR data were calculated using information provided by the Climate Prediction Center/NOAA at https://ftp.cpc.ncep.noaa.gov/precip/CBO_V1/.

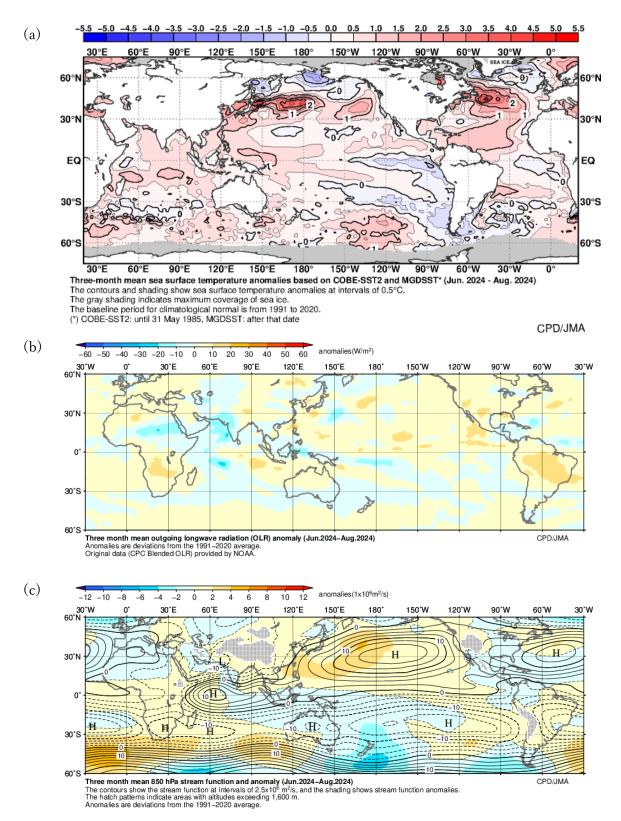


Figure 3.1 Three-month mean (a) sea surface temperature (SST) anomaly, (b) outgoing longwave radiation (OLR) anomaly, and (c) 850-hPa stream function (contours) and related anomaly (shading) in boreal summer (June – August 2024)

The base period for the normal is 1991-2020. (a) The contour interval is 0.5° C. Sea ice coverage areas are shaded in gray. (b) Negative (cold color) and positive (warm color) OLR anomalies show enhanced and suppressed convection, respectively, compared to the normal. Original data is provided by NOAA. (c) The contour interval is 2.5×10^6 m²/s. "H" and "L" denote high- and low-pressure systems, respectively.

3.2 Tropical Cyclones in 2024

A total of 26 named TCs formed over the western North Pacific and the South China Sea in 2024, which was almost the same as the climatological normal. Monthly and normal numbers of named TC formations are shown in Figure 3.2, and the tracks of the 26 TCs are shown in Figure 3.3. Figure 3.4 shows the genesis points of these TCs (dots) and related frequency distribution for past years (1951 – 2023).

The 2024 typhoon season started in May with Ewiniar (2401), which formed over the sea east of Mindanao. A total of 4 had formed by July, which was below the average of 7.8, and the other 22 formed from August onward, which was higher than the average of 17.3. The El Niño event that continued until spring suppressed convection in the tropical western North Pacific until the end of July, as per conditions observed in other post-El Niño summers, and suppressed tropical cyclone genesis. However, the number of named TC formations increased from August onward, probably in association with weakened influence from the El Niño event and enhanced convection from the Philippines to the southeast of Japan in August and September.

The mean genesis point of named TCs was 17.9°N and 134.7°E, representing a north-westward deviation from that of the 30-year average⁴ (16.3°N and 135.9°E) (see Figure 3.4). The mean genesis point of named TCs formed in summer (June to August) was 21.9°N and 136.6°E, with north-eastward deviation from that of the 30-year summer average (18.5°N and 134.2°E), and that of named TCs formed in autumn (September to November) was 16.5°N and 137.3°E, which was almost the same area as that of the 30-year autumn average (16.2°N and 137.0°E).

The mean duration of TCs sustaining TS intensity or higher was 4.8 days, which was shorter than that of the 30-year average (5.2 days). The mean duration of TCs sustaining TS intensity or higher formed in summer was 4.4 days, which was shorter than that of the 30-year average (5.0 days), and the mean duration of TCs sustaining TS intensity or higher formed in autumn was 5.5 days, which was almost the same as that of the 30-year average (5.4 days).

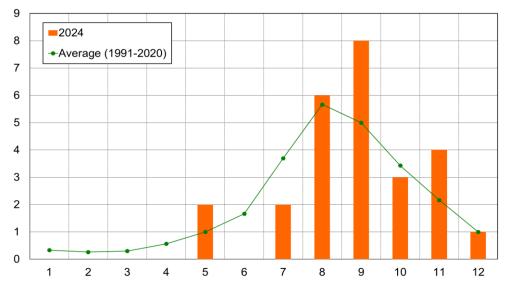


Figure 3.2 Monthly number of named TC formation for 2024 compared to the climatological normal

⁴ The 30-year averaging period is from 1991 to 2020.

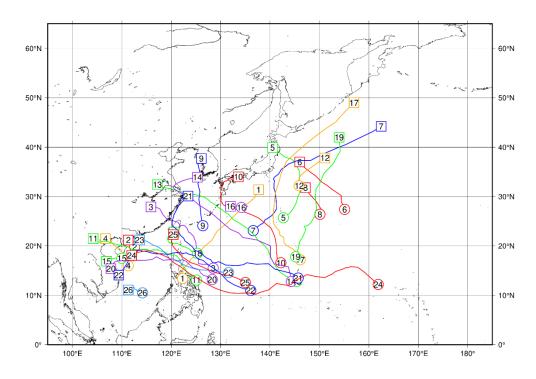


Figure 3.3 Tracks of the 26 named TCs that formed in 2024. TC tracks for those with an intensity of TS or higher are shown.

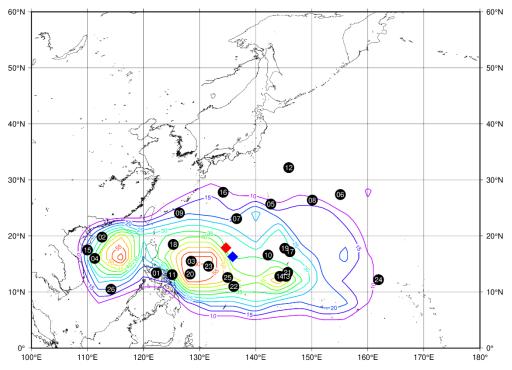


Figure 3.4 Genesis points of the 26 named TCs forming in 2024 (dots) and related frequency distribution for 1951 - 2023 (lines). Red and blue diamond show the mean genesis points of TCs forming in 2024 and the 30-year average period (1991 – 2020), respectively.

Chapter 4 Verification of Forecasts and Other Products in 2024

4.1 Verification of Operational Forecasts

Operational forecasts for the 26 named TCs that formed in 2024 were verified using RSMC TC best track data⁵. The verified elements were forecasts of the center position, central pressure and maximum sustained wind speed (up to five days ahead). In addition to forecast errors, improvement ratios of forecast errors to climatological model were also evaluated to assess operational forecast skill. Forecasts issued at 00, 06, 12 and 18 UTC were included in verification for TCs classified in best track data as TS, STS or TY at both initial and forecast valid times. The position and intensity errors of such operational forecasts are shown in bold face in Appendix 3. (Those for TD before upgrading to TS intensity or higher are indicated in italic face in Appendix 3.)

4.1.1 Center Position

Figure 4.1 shows annual mean errors in TC track forecasts covering periods of 24 hours (since 1982), 48 hours (since 1989), 72 hours (since 1997), 96 hours and 120 hours (since 2009). It can be seen that operational TC track forecasts have steadily improved since 1982, although year-to-year fluctuations are seen due in part to differences in TC characteristics. The improvement observed since 2015 is partially attributed to the introduction of the consensus method using four global numerical models of ECMWF, JMA, NCEP and UKMO for operational forecasts in that year. The errors in 2024 were 71, 106, 152, 245 and 424 km for 24-, 48-, 72-, 96- and 120-hour forecasts, respectively. Forecast errors for 48 and 72 hours in 2024 were the lowest on record, while those for 120-hour forecasts were comparatively high in relation to recent years.

The annual mean improvement ratios in relation to the climatology and persistence model (CLIPER)⁶ for TC track prediction since 2011 are shown in Figure 4.2 to support evaluation of the operational forecast skill. The values are defined as

<u>Mean Position Error (CLIPER) – Mean Position Error (Operational)</u> <u>Mean Position Error (CLIPER)</u>

and positive/negative values indicate that the operational forecasts were better/worse than the CLIPER predictions. Although there are year-to-year fluctuations, it can be seen that operational forecasts have steadily improved in the long term. The annual mean improvement ratios for 24-, 48-, 72-, 96- and 120-hour forecasts in 2024 were 65% (59% in 2023), 77% (69%), 78% (72%), 71% (70%) and 61% (68%), respectively. Forecast improvement ratios for 48 and 72 hours in 2024 were the highest on record.

The details of errors including improvement ratios to CLIPER for each named TC that formed in 2024 are summarized in Table 4.1. Forecasts for Shanshan (2410) was characterized by large errors. This was attributable to the fact that guidance models predicted more northern tracks than reality due to an inability to adequately predict the influence of an upper cold low around the typhoon during its formation and

⁵ Maximum sustained wind speed of TD is not described in best track data or operational forecast. Therefore, maximum sustained wind speed of TD was treated as 30 kt for convenience in verification in 4.1.

⁶ The Center operates the CLIPER model based on Aberson (1998), Neumann (1972) and Merrill (1980). The model uses no information on current atmospheric status, but best track data such as TC center position/central pressure/movement and dates. Multiple regression coefficients for the model were generated from best track data between 1980 and 2010.

development stages.

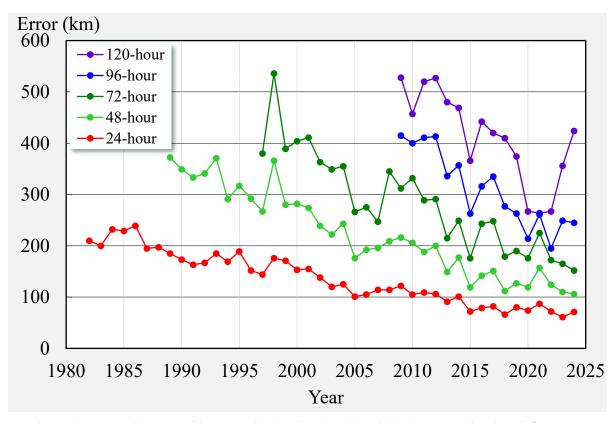


Figure 4.1 Annual mean position errors in 24-, 48-, 72-, 96- and 120-hour operational track forecasts

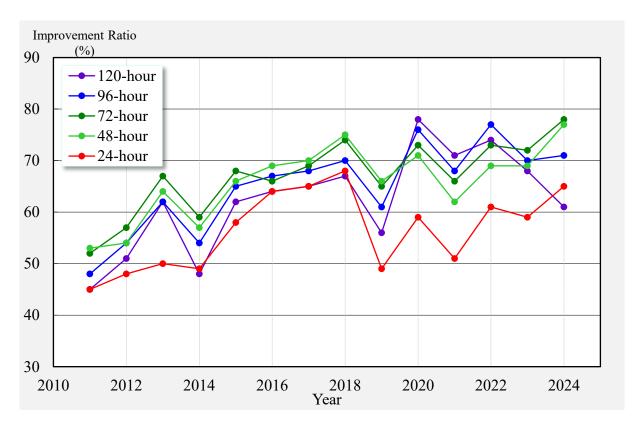


Figure 4.2 Annual mean improvement ratios in 24-, 48-, 72-, 96- and 120-hour operational track forecasts.

Table 4.1 Mean position errors of 24-, 48-, 72-, 96- and 120-hour operational forecasts for each named TC that formed in 2024. S.D., Num. and Impr. represent the standard deviation of operational forecast position errors, number of samples and improvement ratio (see the equation in 4.1.1 for detail), respectively.

	-	-	24	1-hour	Forecas	st	48	3-hour 1	Forecas	t	72	2-hour l	Forecas	st	9	6-hour l	Forecast	t	12	20-hour	Foreca	st
Τ	ropical Cyc	clone	Mean	S.D.	Num.	Impr.	Mean	S.D.	Num.	Impr.	Mean	S.D.	Num.	Impr.	Mean	S.D.	Num.	Impr.	Mean	S.D.	Num.	Impr.
			(km)	(km)		(%)	(km)	(km)		(%)	(km)	(km)		(%)	(km)	(km)		(%)	(km)	(km)		(%)
TY	Ewiniar	(2401)	49	21	17	78	63	32	13	85	71	35	9	90	125	22	5	88	261	0	1	84
TS	Maliksi	(2402)	-	-	0	-	-	-	0	-	_	-	0	-	-	-	0	-	-	-	0	-
TY	Gaemi	(2403)	69	51	23	64	79	35	19	83	108	65	15	82	178	123	11	63	307	91	7	30
STS	Prapiroon	(2404)	57	29	6	71	90	14	2	74	_	-	0	-	-	-	0	-	-	-	0	-
STS	Maria	(2405)	41	21	14	82	57	24	10	91	108	62	6	87	322	21	2	61	-	-	0	
TS	Son-tinh	(2406)	43	26	6	86	111	1	2	84	-	-	0	-	-	-	0		-	-	0	-
TY	Ampil	(2407)	69	34	22	63	96	40	18	70	129	46	14	66	158	59	10	69	187	94	6	79
TS	Wukong	(2408)	138	14	2	56	-	-	0	-	_	-	0	-	-	-	0	-	-	-	0	-
TS	Jongdari	(2409)	38	16	5	87	82	0	1	91	_	-	0	-	-	-	0	-	-	-	0	-
TY	Shanshan	(2410)	63	43	31	66	117	56	27	73	213	156	23	69	583	307	19	34	1227	411	15	-19
TY	Yagi	(2411)	72	55	25	49	111	102	21	62	130	105	17	74	243	149	13	64	368	238	9	51
TS	Leepi	(2412)	105	0	1	27	-	-	0	-	_	-	0	-	-	-	0	-	-	-	0	-
TY	Bebinca	(2413)	74	30	22	71	105	36	18	85	125	67	14	89	143	54	10	90	99	31	6	92
TS	Pulasan	(2414)	127	50	19	71	201	40	13	82	293	74	9	85	343	16	3	84	639	41	2	68
TS	Soulik	(2415)	-	_	0	-	-	-	0	-	_		0	-	-		0	-	-	-	0	
TS	Cimaron	(2416)	51	0	1	77	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TY	Jebi	(2417)	94	58	18	57	116	57	14	77	100	79	10	86	134	53	6	87	129	62	2	92
TY	Krathon	(2418)	51	23	18	64	116	32	14	62	237	32	10	36	360	74	6	7	556	21	2	0
TS	Barijat	(2419)	105	47	12	66	141	84	8	79	157	60	4	82	-	-	0	-	-	-	0	-
STS	Trami	(2420)	76	35	20	59	91	47	16	79	147	108	12	79	198	97	8	82	287	63	4	74
TY	Kong-rey	(2421)	87	79	27	49	90	81	23	74	132	44	19	75	212	50	15	75	335	72	11	75
TY	Yinxing	(2422)	40	29	31	77	76	53	27	81	141	68	23	76	217	115	19	74	260	168	15	78
TY	Toraji	(2423)	52	36	17	54	89	55	13	58	95	28	9	66	145	58	5	63	214	0	1	12
TY	Man-yi	(2424)	98	75	38	50	154	118	34	65	196	147	30	72	145	83	17	83	185	107	13	86
TY	Usagi	(2425)	37	16	13	62	62	30	9	74	61	21	5	84	135	0	1	74	-	-	0	
TS	Pabuk	(2426)	93	29	6	29	120	21	2	58	_		0	_	_	_	0		_		0	
An	nual Mean ((Total)	71	53	394	65	106	74	304	77	152	107	229	78	245	197	150	71	424	416	94	61

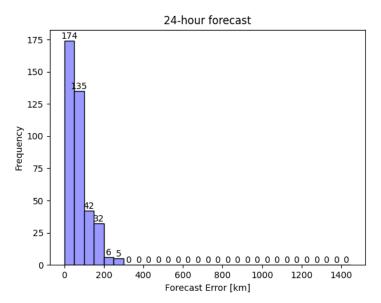


Figure 4.3 Histogram of 24-hour forecast position errors in 2024 (Histograms for 48-, 72-, 96- and 120-hour forecasts are available in Appendix 5 Figure A5.1 and A5.2)

Figure 4.3 shows a histogram of 24-hour forecast position errors (histograms for 48-, 72-, 96- and 120-hour forecasts are available in Appendix 5 Figure A5.1 and A5.2). About 89% (95% in 2023) of 24-hour forecasts, 96% (95%) of 48-hour forecasts, 98% (97%) of 72-hour forecasts, 91% (89%) of 96-hour forecasts and 80% (82%) of 120-hour forecasts had errors of less than 150, 300, 450, 500 and 600 km, respectively.

Figure 4.4 shows scatter diagrams of 48-hour forecast position errors in longitudinal/latitudinal direction and cross-track/along-track direction (Scatter diagrams of 24-, 72-, 96- and 120-hour forecasts are available in Appendix 5 Figure A5.3 and A5.4). While mean position biases are relatively small, fast bias for Shanshan (2410) during and after recurvature and northward bias for Man-yi (2424) before recurvature are seen.

Table 4.2 presents the mean hitting ratios and radii of 70% probability circles⁷ provided in operational forecasts for each named TC that formed in 2024. The term hitting ratio here is used to describe the ratio of the number of 70% probability circles within which the actual TC center fell to the total number of circles. The annual mean radius of circles provided in 24-hour position forecasts was 92 km (86 km in 2023), and their hitting ratio was 75% (80%). The corresponding values for 48-hour forecasts were 160 km (148 km in 2023) and 81% (76%), those for 72-hour forecasts were 230 km (217 km in 2023) and 78% (75%), those for 96-hour forecasts were 291 km (284 km in 2023) and 69% (68%), and those for 120-hour forecasts were 372 km (370 km in 2023) and 62% (61%).

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⁷ Probability circle: a circular range in which a TC is expected to be located with a probability of 70% at each forecast period

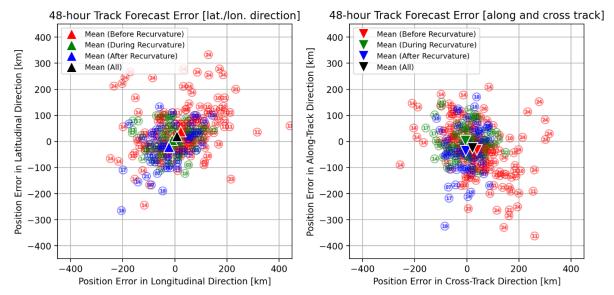


Figure 4.4 Scatter diagrams of 48-hour forecast position errors in longitudinal/latitudinal direction (left) and cross-/along-track direction (right) in 2024. (Scatter diagrams of 24-, 72-, 96- and 120-hour forecasts are available in Appendix 5 Figure A5.3 and A5.4.) Red, green and blue circles with TC numbers denote biases for each initial time in the stages before, during and after recurvature, respectively. Red, green and blue triangles indicate mean biases in the stages before, during and after recurvature, respectively. The definition of the stages is based on the direction of movement of each TC at individual prediction times (Figure 4.5). Black triangles indicate mean bias for all initial time.

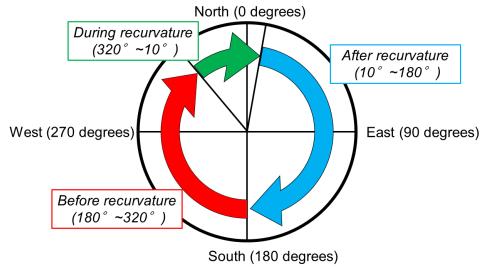


Figure 4.5 Definition of the stages before, during and after recurvature based on TC direction as calculated from positions at individual prediction times and those observed six hours prior.

Table 4.2 Mean hitting ratios (%) and radii (km) of 70% probability circles provided in 24-, 48-, 72-, 96- and 120-hour operational forecasts for each named TC that formed in 2024. Num. represents the number of samples.

	*	-	24-h	our Fo	recast	48-h	our Fo	recast	72-h	our Fo	recast	96-h	our Fo	recast	120-	hour Fo	orecast
	Tropical Cy	clone	Ratio	Num.	Radius	Ratio	Num.	Radius									
			(%)		(km)	(%)		(km)									
TY	Ewiniar	(2401)	94	17	96	100	13	177	100	9	264	100	5	332	100	1	519
TS	Maliksi	(2402)	_	0	-	_	0	-	-	0	-	_	0	-	-	0	_
TY	Gaemi	(2403)	78	23	97	100	19	173	100	15	254	91	11	306	71	7	382
STS	Prapiroon	(2404)	67	6	86	100	2	148	-	0	-	-	0	-	-	0	-
STS	Maria	(2405)	100	14	89	100	10	163	100	6	265	50	2	324	-	0	-
TS	Son-tinh	(2406)	100	6	102	100	2	185	-	0	-	-	0	-	-	0	-
TY	Ampil	(2407)	64	22	76	78	18	130	86	14	208	100	10	292	100	6	372
TS	Wukong	(2408)	0	2	97	-	0	-	-	0	-	-	0	-	-	0	-
TS	Jongdari	(2409)	100	5	81	100	1	157	-	0	-	-	0	-	-	0	-
TY	Shanshan	(2410)	81	31	90	74	27	163	57	23	237	16	19	309	0	15	398
TY	Yagi	(2411)	60	25	80	62	21	141	76	17	221	69	13	311	78	9	439
TS	Leepi	(2412)	0	1	78	-	0	-	-	0	-	-	0	-	-	0	-
TY	Bebinca	(2413)	91	22	99	100	18	191	100	14	283	100	10	357	100	6	431
TS	Pulasan	(2414)	47	19	116	62	13	202	33	9	276	0	3	309	0	2	398
TS	Soulik	(2415)	-	0	-	_	0	-	-	0	-	_	0	-	-	0	_
TS	Cimaron	(2416)	100	1	93	-	0	-	-	0	-	-	0	-	-	0	-
TY	Jebi	(2417)	61	18	113	93	14	209	90	10	282	100	6	343	100	2	491
TY	Krathon	(2418)	89	18	84	71	14	140	30	10	207	17	6	278	0	2	333
TS	Barijat	(2419)	50	12	115	88	8	204	100	4	294	-	0	-	-	0	-
STS	Trami	(2420)	75	20	99	81	16	166	67	12	228	75	8	278	75	4	366
TY	Kong-rey	(2421)	70	27	87	83	23	137	89	19	191	67	15	254	45	11	318
TY	Yinxing	(2422)	90	31	82	89	27	143	87	23	204	68	19	269	73	15	345
TY	Toraji	(2423)	88	17	70	85	13	119	100	9	161	80	5	213	100	1	278
TY	Man-yi	(2424)	58	38	97	56	34	160	63	30	220	88	17	256	85	13	321
TY	Usagi	(2425)	92	13	76	100	9	139	100	5	215	100	1	324	-	0	
TS	Pabuk	(2426)	67	6	117	100	2	204	-	0		-	0		-	0	
A	nnual Mean	(Total)	75	394	92	81	304	160	78	229	230	69	150	291	62	94	372

4.1.2 Central Pressure and Maximum Wind Speed

Figure 4.6 shows annual means of root mean square errors (RMSEs) for TC central pressure and maximum wind speed forecasts covering periods of 24 hours, 48 hours (since 2001), 72 hours (since 2003) 96 hours and 120 hours (since 2019). The values for maximum wind speed forecasts for individual TCs are available in Appendix 5 Table A5.1.

Operational TC intensity forecasts have improved with the introduction of intensity forecast guidance, but no change trend has been seen in recent years. The annual RMSEs of central pressure for 24-, 48-, 72-96- and 120-hour forecasts were 10.9 hPa (12.8 hPa in 2023), 13.4 hPa (16.9 hPa), 16.5 hPa (18.0 hPa), 20.4 hPa (20.6 hPa) and 23.8 hPa (22.2 hPa), respectively. The corresponding values for maximum wind speed were 5.3 m/s (5.1 m/s in 2023), 6.2 m/s (7.2 m/s), 7.3 m/s (7.9 m/s), 8.6 m/s (9.2 m/s) and 10.5 m/s (10.4 m/s), respectively. 48-hour forecast errors in 2024 were the lowest on record for both central pressure and maximum wind speed, while 120-hour forecast errors were the worst on record.

Figure 4.7 shows annual mean improvement ratios for central pressure and maximum wind speed forecasts in relation to a guidance model based on climatology and persistence (Statistical Hurricane Intensity Forecast; SHIFOR⁸) to highlight operational forecast skill. The values are defined as

$\frac{\text{RMSE}(\text{SHIFOR}) - \text{RMSE}(\text{Operational})}{\text{RMSE}(\text{SHIFOR})}$

with positive/negative values indicating better/worse operational forecasts than SHIFOR predictions. It can be seen that the operational TC intensity forecasts have improved recently, with minimal year-to-year fluctuations. The annual mean improvement ratios of central pressure for 24-, 48-, 72-, 96- and 120-hour forecasts were 27% (13% in 2023), 44% (18%), 37% (12%), 14% (-6%) and -4% (-9%), respectively. The corresponding values of maximum wind speed were 17% (17% in 2023), 37% (26%), 36% (30%), 24% (22%) and 2% (14%), respectively. The ratios for 48-hour forecast in 2024 were the highest on record for both.

The details of errors in operational central pressure forecasts, including improvement ratios to SHIFOR for each named TC that formed in 2024, are summarized in Table 4.3. The data for maximum wind speed forecasts are available in Appendix 5 Table A5.1. Forecasts for Yagi (2411) and Kong-rey (2421) were characterized by large errors attributed to the difficulty of estimation for track and rapid intensification and weaking.

Figure 4.8 shows a histogram of maximum wind speed errors for 24-hour forecasts (Histograms for 48-, 72-, 96- and 120-hour forecasts are also available in Appendix 5 Figure A5.7 and A5.8). Approximately 58% (56% in 2023) of 24-hour forecasts had errors of less than ± 3.75 m/s, with figures of ± 6.25 m/s for 74% (63%) of 48-hour forecasts, ± 6.25 m/s for 70% (59%) of 72-hour forecasts, ± 8.75 m/s for 71% (66%) of 96-hour forecasts and ± 8.75 m/s for 67% (60%) of 120-hour forecasts. The histograms of central pressure errors are also available in Appendix 5 Figure A5.5 and A5.6.

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⁸ The Center operates the SHIFOR model based on Jarvinen and Neumann (1979). The explanatory variables include TC analysis data (center position, central pressure and maximum sustained wind speed, and related temporal variation from best track data) and date. Multiple regression coefficients for the model were generated from best track data for named TCs forming between 1977 and 2010.

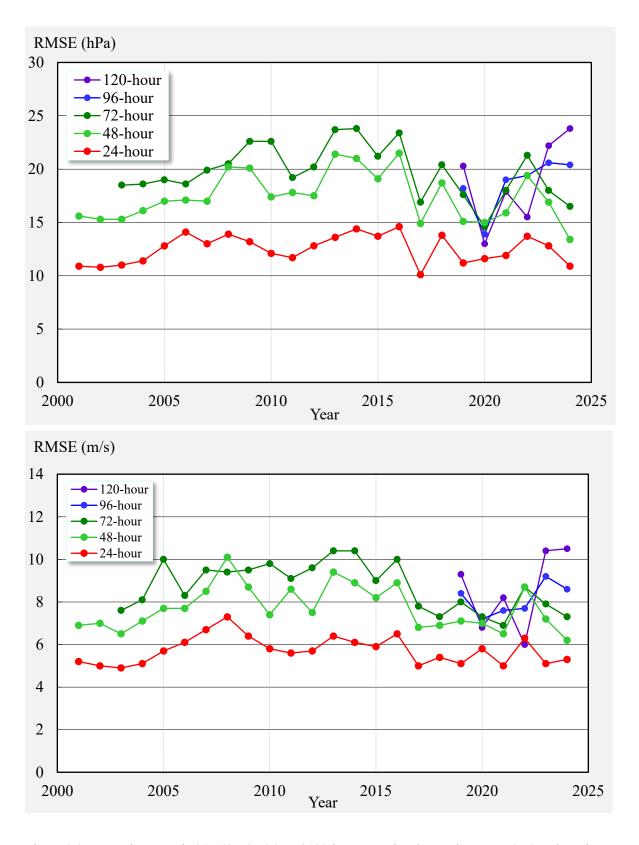


Figure 4.6 Annual RMSEs in 24-, 48, 72-, 96- and 120-hour operational central pressure (top) and maximum wind speed (bottom) forecasts

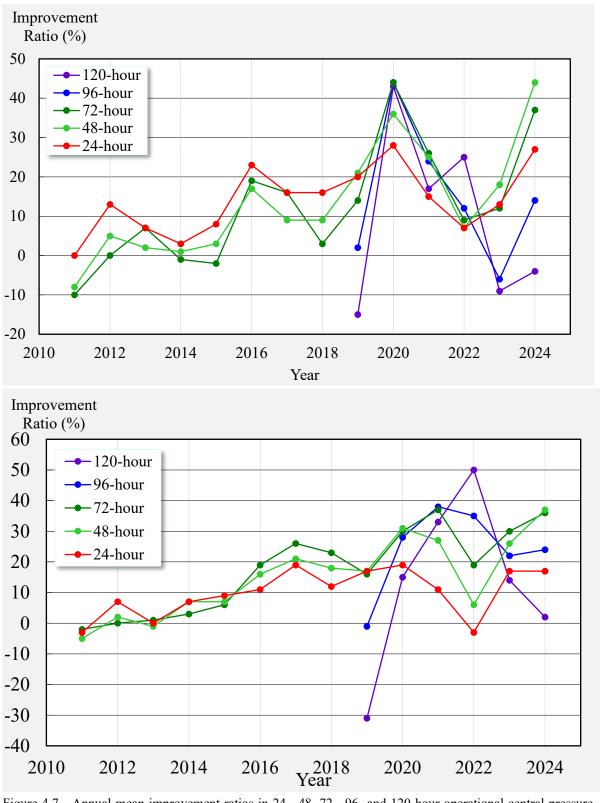


Figure 4.7 Annual mean improvement ratios in 24-, 48, 72-, 96- and 120-hour operational central pressure (top) and maximum wind speed (bottom) forecasts

Table 4.3 Mean errors of 24-, 48-, 72-, 96- and 120-hour operational central pressure forecasts for each named TC that formed in 2024. Num. and Impr. represent the number of samples and improvement ratio of RMSEs (see the equation in 4.1.2 for detail), respectively.

			24	1-hour F	orecast	t	4	8-hour I	Foreca	st	7	2-hour I	Forecas	t	9	6-hour I	Forecas	t	12	0-hour F	orecas	st
	Tropical Cyclon	e	Error	RMSE 1	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE 1	Num.	Impr.
			(hPa)	(hPa)		(%)	(hPa)	(hPa)		(%)	(hPa)	(hPa)		(%)	(hPa)	(hPa)		(%)	(hPa)	(hPa)		(%)
TY	Ewiniar (2	2401)	4.2	13.9	17	-56	-2.8	13.3	13	22	-2.1	7.8	9	66	-2.8	3.9	5	85	-4.0	4.0	1	88
TS	Maliksi (2	2402)	_	_	0	_	_	_	0	_	_	_	0	_	_	_	0	_	_	_	0	_
TY	Gaemi (2	2403)	-1.0	5.1	23	68	-0.4	10.4	19	40	-0.9	12.2	15	20	-8.5	22.0	11	-29	-24.0	27.1	7	-54
STS	Prapiroon (2	2404)	6.2	7.5	6	15	9.0	9.1	2	48	-	-	0	-	-	-	0	-	-	-	0	_
STS	Maria (2	2405)	-4.1	8.1	14	-16	-3.7	6.7	10	23	-2.0	5.7	6	-135	-1.0	6.1	2	38	-	-	0	-
TS	Son-tinh (2	2406)	-1.3	3.1	6	57	7.0	7.1	2	63	-	-	0	-	-	-	0	-	-	-	0	_
TY	Ampil (2	2407)	-0.7	6.4	22	45	1.9	4.6	18	74	9.6	11.6	14	45	14.5	15.9	10	8	14.0	14.2	6	-100
TS	Wukong (2	2408)	0.0	0.0	2	100	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TS	Jongdari (2	2409)	-0.8	3.8	5	50	-4.0	4.0	1	80	-	-	0	-	-	-	0	-	-	-	0	-
TY	Shanshan (2	2410)	-6.3	15.5	31	11	-8.4	17.4	27	36	-8.0	20.1	23	23	2.4	20.6	19	3	17.3	24.1	15	-30
TY	Yagi (2	2411)	7.4	19.6	25	17	18.8	25.9	21	31	26.2	35.1	17	12	24.4	37.4	13	-3	13.3	28.6	9	-6
TS	Leepi (2	2412)	2.0	2.0	1	56	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TY	Bebinca (2	2413)	-3.8	7.1	22	41	-4.2	10.5	18	44	-3.4	8.4	14	58	2.8	4.1	10	79	2.7	7.3	6	73
TS	Pulasan (2	2414)	0.6	1.9	19	78	0.5	1.7	13	93	-0.4	1.3	9	97	-3.3	3.5	3	93	-1.0	1.4	2	97
TS	Soulik (2	2415)	-	-	0	-	_	-	0	-	-	-	0	-	-	-	0	-	-	-	0	
TS	Cimaron (2	2416)	4.0	4.0	1	-111	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TY	Jebi (2	2417)	1.3	6.2	18	35	0.4	5.0	14	73	3.2	6.0	10	72	11.5	12.6	6	26	8.5	8.9	2	65
TY	Krathon (2	2418)	2.3	17.3	18	4	7.9	22.8	14	27	18.0	23.8	10	26	3.3	16.1	6	14	-10.0	10.0	2	21
TS	Barijat (2	2419)	0.4	3.0	12	49	1.6	4.3	8	69	1.8	2.7	4	86	-	-	0	-	-	-	0	-
STS	Trami (2	2420)	-1.6	5.0	20	59	-2.8	4.8	16		-7.9	10.2	12	40	-6.3	9.5	8	44	-8.8	11.1	4	52
TY	Kong-rey (2	2421)	0.1	12.9	27	18	0.7	12.6	23	50	2.7	15.1	19	37	3.5	25.7	15	-8	-0.5	37.2	11	-55
TY	Yinxing (2	2422)	1.6	6.7	31	58	5.0	9.8	27	39	6.7	14.0	23	-9	3.5	8.2	19	36	2.9	4.3	15	67
TY	Toraji (2	2423)	-1.2	4.3	17	59	-0.6	2.8	13	86	-0.7	2.4	9	91	-0.8	3.8	5	87	-2.0	2.0	1	94
TY	2 (2424)	4.5	12.4	38	28	7.4	13.3	34	58	10.5	17.5	30	50	20.9	28.3	17	7	17.4	33.0	13	-7
TY	Usagi (2	2425)	-1.5	17.1	13	38	2.9	22.6	9	23	-9.8	11.7	5	57	-8.0	8.0	1	77	-	-	0	
TS	Pabuk (2	2426)	-1.7	2.4	6	68	-4.0	4.0	2	81	-		0	-	_		0	-	-		0	
	Annual Mean (Tot	tal)	0.3	10.9	394	27	1.9	13.4	304	44	3.9	16.5	229	37	6.1	20.4	150	14	5.6	23.8	94	-4

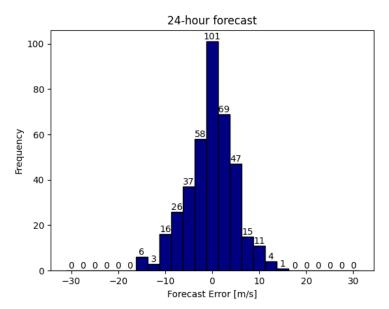


Figure 4.8 Histogram of 24-hour forecast maximum wind speed errors in 2024 (Histograms for 48-, 72-, 96- and 120-hour forecasts are also available in Appendix 5 Figure A5.7 and A5.8).

[Reference]

Aberson, S. D., 1998. Five-day tropical cyclone track forecasts in the North Atlantic basin, *Weather and Forecasting*, **13**, 1005-1015.

Jarvinen, B. R. and C. J. Neumann, 1979: Statistical forecasts of tropical cyclone intensity, *NOAA Tech. Memo. NWS NHC-10*, 22 pp.

Neumann, C. J., 1972: An alternate to the Hurran (hurricane analog) tropical cyclone forecasting system. NOAA Tech. Memo. NWS SR 62, 23 pp.

Merrill, R. T., 1980: A statistical tropical cyclone motion forecasting system for the Gulf of Mexico. *NOAA Tech. Memo. NWS NHC 14*, 21 pp.

4.2 Verification of Timing of First-issued Operational Forecasts

The Center issues TC track forecasts with probability circles and intensity forecasts when a TC of TS intensity or higher is present or expected within 24 hours in its area of responsibility. Accordingly, initial forecasts for individual TCs are also used as 24-hour genesis forecasts in addition to track and intensity forecasts.

Table 4.4 shows differences between initial times of first forecast and upgrade times in best track data/real-time provisional analysis data for individual named TCs in 2024. In several cases, differences were shorter than the ideal for 24 hours due to sub-optimal numerical model prediction.

Table 4.4 Lead times of operational forecasting for upgrade to TS intensity or higher. "First forecast", "Upgrade (Best/Prov.)" and "Lead time (Best/Prov.)" are the initial time of the first forecast for individual named TCs, the time when the TC was upgraded to TS intensity or higher in best track data/provisional analysis, and the time difference between the two, respectively.

Т	ropical Cyc	clone	First Forecast	Upgrade (Best)	Upgrade (Prov.)	Lead Time (Best) Lead T	ime (Prov.)
TY	Ewiniar	(2401)	00UTC 23 May	12UTC 25 May	00UTC 26 May	60 h	72 h
TS	Maliksi	(2402)	06UTC 30 May	00UTC 31 May	06UTC 31 May	18 h	24 h
TY	Gaemi	(2403)	12UTC 19 Jul	00UTC 20 Jul	06UTC 20 Jul	12 h	18 h
STS	Prapiroon	(2404)	06UTC 19 Jul	00UTC 21 Jul	03UTC 21 Jul	42 h	45 h
STS	Maria	(2405)	12UTC 06 Aug	18UTC 07 Aug	18UTC 07 Aug	30 h	30 h
TS	Son-tinh	(2406)	12UTC 10 Aug	00UTC 11 Aug	09UTC 11 Aug	12 h	21 h
TY	Ampil	(2407)	00UTC 12 Aug	12UTC 12 Aug	18UTC 12 Aug	12 h	18 h
TS	Wukong	(2408)	00UTC 13 Aug	00UTC 13 Aug	06UTC 13 Aug	0 h	6 h
TS	Jongdari	(2409)	18UTC 18 Aug	12UTC 18 Aug	18UTC 18 Aug	-6 h	0 h
TY	Shanshan	(2410)	00UTC 21 Aug	18UTC 21 Aug	18UTC 21 Aug	18 h	18 h
TY	Yagi	(2411)	00UTC 01 Sep	06UTC 01 Sep	12UTC 01 Sep	6 h	12 h
TS	Leepi	(2412)	06UTC 05 Sep	00UTC 05 Sep	06UTC 05 Sep	-6 h	0 h
TY	Bebinca	(2413)	18UTC 09 Sep	12UTC 10 Sep	12UTC 10 Sep	18 h	18 h
TS	Pulasan	(2414)	06UTC 15 Sep	12UTC 15 Sep	12UTC 15 Sep	6 h	6 h
TS	Soulik	(2415)	00UTC 16 Sep	18UTC 18 Sep	00UTC 19 Sep	66 h	72 h
TS	Cimaron	(2416)	00UTC 25 Sep	06UTC 24 Sep	03UTC 25 Sep	-18 h	3 h
TY	Jebi	(2417)	06UTC 26 Sep	00UTC 27 Sep	06UTC 27 Sep	18 h	24 h
TY	Krathon	(2418)	18UTC 26 Sep	00UTC 28 Sep	00UTC 28 Sep	30 h	30 h
TS	Barijat	(2419)	00UTC 07 Oct	06UTC 06 Oct	06UTC 09 Oct	-18 h	54 h
STS	Trami	(2420)	06UTC 20 Oct	18UTC 21 Oct	18UTC 21 Oct	36 h	36 h
TY	Kong-rey	(2421)	00UTC 24 Oct	18UTC 24 Oct	21UTC 24 Oct	18 h	21 h
TY	Yinxing	(2422)	00UTC 03 Nov	12UTC 03 Nov	18UTC 03 Nov	12 h	18 h
TY	Toraji	(2423)	18UTC 08 Nov	06UTC 09 Nov	06UTC 09 Nov	12 h	12 h
TY	Man-yi	(2424)	00UTC 09 Nov	18UTC 08 Nov	06UTC 09 Nov	-6 h	6 h
TY	Usagi	(2425)	00UTC 10 Nov	18UTC 11 Nov	18UTC 11 Nov	42 h	42 h
TS	Pabuk	(2426)	00UTC 22 Dec	06UTC 22 Dec	06UTC 23 Dec	6 h	30 h

4.3 Verification of Numerical Models (GSM, GEPS)

GSM and GEPS provide primary information for use by JMA forecasters in making operational TC track and intensity forecasts. The details of GSM and GEPS and information on recent related improvements are given in Appendix 7. GSM and GEPS predictions were verified with RSMC TC best track data and predictions using the persistency (PER) method. All TC forecast verifications were conducted for both systems.

4.3.1 GSM Prediction

1) Center Position

GSM annual mean position errors observed since 1997 are presented in Figure 4.9. In 2024, the annual mean errors for 30-, 54-, 78-, 102- and 126-hour⁹ predictions were 94 km (85 km in 2023), 146 km (144 km), 224 km (225 km), 367 km (337 km) and 587 km (466 km), respectively. The mean position errors of 18-, 30-, 42-, 54-, 66-, 78-, 90-, 102-, 114- and 126-hour predictions for each named TC are given in Table 4.5.

Table 4.6 shows relative GSM performance compared with results obtained using the PER method¹⁰. In this comparison, TCs were classified into the three life stages of before, during, and after recurvature. The definition of the stages is based on the direction of movement of each TC at individual prediction times (Figure 4.5). The table indicates that GSM results outperformed those of the PER method throughout the forecast period beyond 18 hours from the initial time, and that the ratios of error reduction for the GSM compared to the PER method were about 59% (52% in 2023), 69% (64%), 76% (70%), 76% (69%), 71% (65%) and 63% (62%) for 18-, 30-, 54-, 78-, 102- and 126-hour predictions, respectively.

About 81% (87% in 2023) of 30-hour predictions (histograms showing the position errors of 30-, 54-, 78-, 102- and 126-hour predictions are shown in Appendix 5 Figure A5.9 and A5.10) had errors of less than 150 km, while 92% (92%) of 54-hour predictions had errors of less than 300 km, and 93% (92%) of 78-hour predictions had errors of less than 450 km.

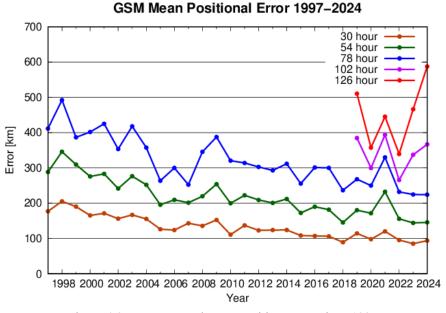


Figure 4.9 GSM annual mean position errors since 1997

⁹ 30-, 54-, 78-, 102- and 126-hour GSM predictions are used as primary information by forecasters creating 24-, 48-, 72-, 96- and 120-hour operational forecasts, respectively.

¹⁰ The PER method is based on the assumption that a TC holds the same movement throughout the forecast period, and linear extrapolation for the latest 12-hour track of the TC is applied to create TC track forecasts. Position errors with the PER method are used to evaluate the relative performance of operational forecasts and model predictions.

Table 4.5 GSM mean position errors (km) for each named TC that formed in 2024. The number of samples is given in parentheses.

Tropi	cal Cyclone	!	T=	-18	T=	:30	T=	:42	T=	:54	T=	:66	T=	78	T=	90	T=	102	T=	114	T=1	26
TY	2401	EWINIAR	77.1	(25)	107.6	(23)	137.3	(21)	179.8	(19)	214.0	(17)	248.2	(15)	321.5	(13)	438.2	(11)	528.4	(9)	657.4	(7)
TS	2402	MALIKSI	33.0	(5)	93.6	(3)	144.5	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2403	GAEMI	101.9	(31)	112.1	(29)	122.6	(27)	124.4	(25)	142.6	(23)	162.5	(21)	182.0	(18)	226.7	(17)	312.9	(15)	357.6	(13)
STS	2404	PRAPIROON	67.1	(11)	94.6	(9)	130.2	(7)	196.8	(5)	264.4	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
STS	2405	MARIA	58.0	(22)	74.7	(20)	81.2	(18)	93.5	(16)	108.9	(14)	138.5	(12)	163.0	(10)	243.8	(8)	466.4	(6)	1008.8	(4)
TS	2406	SON-TINH	61.9	(9)	102.3	(7)	187.4	(5)	245.3	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2407	AMPIL	49.7	(25)	63.0	(23)	86.2	(21)	106.6	(19)	123.6	(17)	163.0	(15)	209.7	(13)	246.0	(11)	318.1	(9)	320.8	(7)
TS	2408	WUKONG	106.3	(7)	155.2	(5)	242.5	(3)	283.1	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TS	2409	JONGDARI	49.6	(6)	42.8	(4)	55.5	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2410	SHANSHAN	44.6	(42)	66.7	(40)	90.3	(38)	121.1	(36)	183.3	(34)	288.7	(32)	468.4	(30)	682.2	(28)	881.8	(24)	1201.3	(23)
TY	2411	YAGI	69.6	(26)	100.8	(24)	140.2	(22)	186.3	(20)	224.6	(18)	277.3	(16)	370.8	(14)	529.6	(12)	708.8	(10)	937.6	(8)
TS	2412	LEEPI	55.1	(9)	63.3	(5)	89.4	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2413	BEBINCA	70.4	(26)	100.2	(24)	141.1	(22)	163.7	(20)	203.0	(18)	247.6	(16)	298.1	(14)	353.0	(12)	372.7	(10)	379.5	(8)
TS	2414	PULASAN	108.2	(20)	121.9	(18)	167.5	(16)	225.0	(14)	288.5	(12)	415.3	(10)	577.0	(7)	748.4	(3)	888.7	(2)	-	(-)
TS	2415	SOULIK	177.0	(10)	177.9	(8)	185.2	(5)	259.1	(3)	480.0	(2)	666.0	(2)	-	(-)	-	(-)	-	(-)	-	(-)
TS	2416	CIMARON	59.9	(6)	60.4	(4)	116.8	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2417	JEBI	79.8	(24)	106.5	(22)	127.2	(20)	139.0	(18)	144.3	(15)	122.0	(12)	127.1	(10)	163.3	(8)	199.3	(6)	275.1	(3)
TY	2418	KRATHON	55.2	(25)	95.4	(23)	123.0	(21)	153.4	(18)	212.8	(16)	271.6	(13)	359.0	(12)	475.6	(11)	548.1	(8)	676.2	(6)
TS	2419	BARIJAT	105.0	(18)	134.3	(16)	157.9	(14)	135.8	(12)	129.8	(10)	180.7	(8)	246.6	(6)	332.3	(4)	356.2	(1)	-	(-)
STS	2420	TRAMI	80.6	(25)	112.1	(25)	134.8	(22)	169.5	(21)	235.8	(19)	325.1	(17)	426.4	(15)	566.0	(13)	692.4	(12)	858.7	(10)
TY	2421	KONG-REY	81.7	(30)	98.3	(28)	109.0	(26)	112.1	(24)	119.8	(22)	140.2	(20)	170.9	(18)	201.0	(16)	261.5	(14)	353.3	(12)
TY	2422	YINXING	54.8	(34)	68.0	(32)	82.8	(30)	108.1	(28)	134.5	(26)	169.5	(24)	192.6	(22)	218.3	(20)	267.7	(18)	324.8	(16)
TY	2423	TORAJI	49.7	(21)	66.2	(19)	93.3	(16)	130.0	(14)	121.8	(11)	176.7	(9)	221.2	(7)	257.2	(5)	204.6	(3)	-	(-)
TY	2424	MAN-YI	67.1	(41)	95.3	(39)	133.1	(37)	166.7	(35)	196.7	(33)	216.3	(30)	228.6	(28)	241.5	(26)	248.0	(24)	240.6	(22)
TY	2425	USAGI	59.6	(20)	76.9	(18)	92.1	(16)	121.8	(14)	163.3	(12)	193.3	(10)	234.7	(8)	282.3	(6)	343.8	(4)	454.9	(2)
TS	2426	PABUK	86.2	(10)	106.7	(8)	179.5	(6)	285.3	(4)	224.1	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
All	Annual	Mean	71.5	(528)	94.0	(476)	120.4	(419)	145.8	(367)	176.9	(323)	224.2	(282)	285.2	(245)	366.5	(211)	454.5	(175)	587.3	(141)

Table 4.6 Mean position errors (km) of GSM and PER method predictions for the 26 named TCs that formed in 2024 in the stages before, during and after recurvature. The number of samples is given in parentheses. IMPROV is the ratio of error reductions in GSM results to those observed using the PER method.

TIME	MODEL	Bef	ore	Dur	ing	Afte	er	Al	1
T=18	GSM	77.9	(310)	58.3	(119)	67.5	(99)	71.5	(528)
	PER	170.4	(310)	167.9	(119)	196.1	(99)	174.7	(528)
	IMPROV	54.3	%	65.3	%	65.6	%	59.0	%
T=30	GSM	98.4	(277)	80.3	(109)	97.1	(90)	94.0	(476)
	PER	289.9	(277)	300.7	(109)	363.8	(90)	306.4	(476)
	IMPROV	66.1	%	73.3	%	73.3	%	69.3	%
T=42	GSM	128.3	(247)	94.4	(92)	125.5	(80)	120.4	(419)
	PER	428.3	(247)	446.9	(92)	528.7	(80)	451.5	(419)
	IMPROV	70.0	%	78.9	%	76.3	%	73.3	%
T=54	GSM	159.9	(211)	106.8	(84)	150.2	(72)	145.8	(367)
	PER	583.9	(211)	538.3	(84)	738.1	(72)	603.7	(367)
	IMPROV	72.6	%	80.2	%	79.7	%	75.9	%
T=66	GSM	187.5	(188)	138.4	(69)	187.0	(66)	176.9	(323)
	PER	736.7	(188)	714.0	(69)	863.8	(66)	757.8	(323)
	IMPROV	74.6	%	80.6	%	78.4	%	76.7	%
T=78	GSM	230.4	(166)	194.1	(55)	234.4	(61)	224.2	(282)
	PER	891.6	(166)	862.1	(55)	1051.0	(61)	920.4	(282)
	IMPROV	74.2	%	77.5	%	77.7	%	75.6	%
T=90	GSM	264.0	(144)	322.2	(43)	310.3	(58)	285.2	(245)
	PER	1032.2	(144)	1009.7	(43)	1227.8	(58)	1074.5	(245)
	IMPROV	74.4	%	68.1	%	74.7	%	73.5	%
T=102	GSM	326.6	(126)	424.2	(31)	426.5	(54)	366.5	(211)
	PER	1176.9	(126)	1134.8	(31)	1492.4	(54)	1251.5	(211)
	IMPROV	72.3	%	62.6	%	71.4	%	70.7	%
T=114	GSM	394.7	(108)	576.4	(20)	539.9	(47)	454.5	(175)
	PER	1290.4	(108)	1299.6	(20)	1811.3	(47)	1431.3	(175)
	IMPROV	69.4	%	55.6	%	70.2	%	68.3	%
T=126	GSM	487.6	(88)	888.5	(15)	699.2	(38)	587.3	(141)
	PER	1392.2	(88)	1558.4	(15)	2017.3	(38)	1578.4	(141)
	IMPROV	65.0	%	43.0	%	65.3	%	62.8	%

2) Central Pressure and Maximum Wind Speed

The mean errors of 30-, 54-, 78-, 102- and 126-hour GSM central pressure predictions in 2024 were +1.6 hPa (+0.4 hPa in 2023), +3.2 hPa (-0.5 hPa), +5.5 hPa (-1.8 hPa), +6.6 hPa (-1.6 hPa) and +5.6 hPa (-2.6 hPa), respectively. Their root mean square errors (RMSEs) were 12.8 hPa (15.3 hPa in 2023) for 30-hour predictions, 16.0 hPa (18.7 hPa) for 54-hour predictions, 19.6 hPa (23.8 hPa) for 78-hour predictions, 21.7 hPa (27.4 hPa) for 102-hour predictions and 23.9 hPa (27.5 hPa) for 126-hour predictions. The biases in 30-, 54-, 78-, 102- and 126-hour maximum wind speed predictions were -1.7 m/s (-0.4 m/s in 2023) with an RMSE of 8.2 m/s (8.1 m/s), -2.7 m/s (-0.4 m/s) with a RMSE of 9.9 m/s (10.0 m/s), -4.0 m/s (-0.4 m/s) with a RMSE of 11.0 m/s (12.2 m/s), -4.9 m/s (-1.5 m/s) with a RMSE of 12.1 m/s (13.3 m/s) and -4.9 m/s (-1.9 m/s) with a RMSE of 12.7 m/s (13.0 m/s), respectively.

Figure 4.10 shows histograms of central pressure errors and maximum wind speed errors in 30-hour GSM predictions. The GSM exhibited a small positive bias in central pressure prediction, and tended to underestimate the wind speed of TCs.

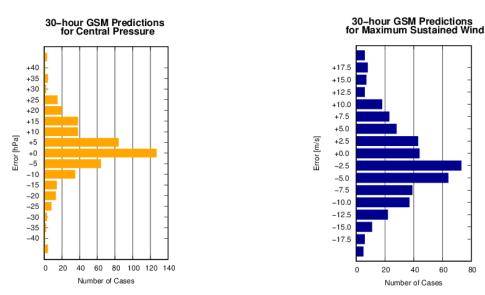


Figure 4.10 Error distribution of GSM 30-hour intensity predictions in 2024. The figure on the left shows error distribution for central pressure, while the one on the right shows that for maximum wind speed (the error distributions of 54-, 78-, 102- and 126-hour predictions are shown at the Appendix 5 Figure A5.11 and A5.12).

4.3.2 GEPS Prediction

1) Ensemble Mean Center Position

GEPS took over the role of the Typhoon Ensemble Prediction System (TEPS), and has been providing ensemble forecasts for TCs since January 2017. GEPS and TEPS annual mean position errors observed since 2008 are presented in Figure 4.11. In 2024, the mean position errors of GEPS ensemble mean forecasts for 18-, 30-, 42-, 54-, 66-, 78-, 90-, 102-, 114-, and 126-hour predictions for each named TC are given in Table 4.7. The annual means of ensemble mean position errors for 30-, 54-, 78-, 102- and 126-hour predictions were 105 km, 163 km, 250 km, 386 km and 607 km, respectively. These position errors of GEPS ensemble mean forecasts are larger than those of the GSM (see 4.3.1).

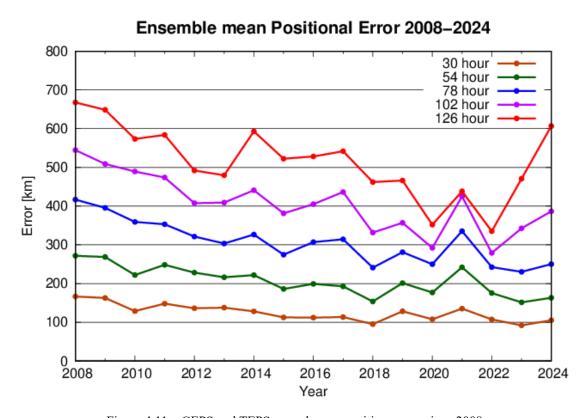


Figure 4.11 GEPS and TEPS annual mean position errors since 2008

Table 4.7 Mean position errors (km) of GEPS ensemble mean forecasts for each named TC that formed in 2024. The number of samples is given in parentheses.

Tropi	cal Cyclone	;	T=	:18	T=	:30	T=	42	T=	:54	T=	:66	T=	-78	T=	90	T=	102	T=	114	T=1	26
TY	2401	EWINIAR	80.1	(25)	118.5	(20)	130.7	(16)	139.9	(14)	137.6	(11)	171.8	(9)	224.1	(8)	260.4	(7)	360.9	(5)	519.1	(4)
TS	2402	MALIKSI	39.2	(5)	106.7	(3)	163.7	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2403	GAEMI	106.3	(31)	133.1	(29)	148.4	(27)	161.3	(25)	185.4	(23)	207.9	(21)	223.7	(19)	251.2	(17)	322.5	(15)	393.0	(13)
STS	2404	PRAPIROON	77.7	(11)	103.7	(9)	173.1	(6)	259.7	(4)	389.9	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
STS	2405	MARIA	57.3	(22)	74.0	(20)	75.0	(18)	87.0	(16)	99.9	(14)	151.4	(12)	239.6	(10)	409.6	(8)	623.2	(6)	997.4	(4)
TS	2406	SON-TINH	63.3	(9)	97.6	(7)	167.1	(5)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2407	AMPIL	51.2	(25)	72.0	(23)	101.7	(21)	124.3	(19)	142.4	(17)	172.5	(15)	204.1	(13)	220.9	(11)	281.7	(9)	274.9	(7)
TS	2408	WUKONG	110.0	(6)	170.2	(4)	227.4	(3)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TS	2409	JONGDARI	39.2	(6)	38.5	(4)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2410	SHANSHAN	53.9	(42)	73.4	(40)	99.7	(38)	134.4	(36)	198.1	(34)	299.2	(32)	441.5	(30)	620.7	(28)	850.1	(26)	1080.2	(24)
TY	2411	YAGI	84.1	(26)	121.7	(24)	169.3	(22)	221.2	(20)	278.9	(18)	357.5	(16)	475.4	(14)	643.8	(12)	859.3	(10)	1126.4	(8)
TS	2412	LEEPI	59.7	(9)	67.5	(4)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2413	BEBINCA	73.0	(26)	104.4	(24)	127.3	(22)	148.2	(20)	175.7	(18)	203.3	(16)	249.1	(14)	309.0	(11)	335.9	(10)	351.9	(8)
TS	2414	PULASAN	103.5	(21)	119.3	(19)	138.7	(17)	182.5	(15)	225.7	(13)	340.5	(11)	453.3	(8)	575.9	(5)	606.0	(2)	708.6	(2)
TS	2415	SOULIK	183.6	(13)	177.1	(11)	178.8	(9)	316.6	(7)	516.6	(5)	776.1	(3)	1216.0	(1)	-	(-)	-	(-)	-	(-)
TS	2416	CIMARON	59.2	(6)	51.0	(4)	110.4	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2417	JEBI	95.7	(24)	125.4	(22)	156.4	(20)	187.2	(17)	212.8	(15)	223.5	(13)	259.7	(10)	358.8	(6)	475.0	(4)	619.5	(3)
TY	2418	KRATHON	57.6	(25)	91.5	(23)	131.1	(21)	165.6	(19)	229.9	(17)	291.6	(15)	345.4	(13)	442.8	(11)	499.7	(9)	570.0	(7)
TS	2419	BARIJAT	107.5	(18)	150.2	(16)	177.1	(14)	166.4	(12)	171.0	(10)	248.2	(8)	406.2	(6)	618.3	(4)	805.1	(2)	-	(-)
STS	2420	TRAMI	95.1	(28)	121.4	(26)	158.2	(24)	196.2	(22)	255.5	(20)	325.8	(18)	416.3	(16)	530.4	(14)	671.8	(12)	853.4	(10)
TY	2421	KONG-REY	80.5	(31)	100.4	(29)	116.7	(27)	134.4	(25)	154.3	(23)	182.3	(21)	221.6	(19)	276.9	(17)	334.2	(15)	425.5	(13)
TY	2422	YINXING	64.2	(34)	89.6	(32)	110.7	(30)	145.8	(28)	174.4	(22)	205.3	(20)	208.6	(18)	228.3	(16)	277.2	(14)	373.0	(10)
TY	2423	TORAJI	59.3	(21)	90.4	(19)	128.8	(17)	167.1	(15)	200.5	(13)	224.8	(11)	246.5	(7)	235.8	(5)	177.5	(2)	-	(-)
TY	2424	MAN-YI	78.1	(41)	114.7	(37)	153.9	(36)	186.1	(34)	215.1	(32)	250.5	(30)	261.3	(27)	272.1	(24)	272.9	(22)	257.1	(20)
TY	2425	USAGI	59.8	(20)	80.7	(18)	112.0	(16)	133.9	(14)	170.0	(12)	230.6	(10)	273.7	(8)	311.8	(6)	349.1	(4)	414.1	(2)
TS	2426	PABUK	113.8	(10)	138.7	(8)	212.4	(6)	238.9	(4)	164.6	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
All	Annual	Mean	78.4	(535)	105.1	(475)	134.5	(418)	163.2	(366)	198.7	(320)	250.2	(281)	308.9	(241)	386.4	(202)	484.4	(167)	606.5	(135)

2) Spread-Skill Relationship

Although position errors of GEPS ensemble mean forecasts were larger than those of the GSM, GEPS provides useful information on the reliability of TC track forecasts with its ensemble spread. Figure 4.12 shows the relationship between 6-hourly cumulative ensemble spreads in TC position forecasts and ensemble mean forecast position errors in 126-hour prediction. In an ideal EPS with a large number of samples, significant positional errors are observed when the ensemble spread is large. The figure shows a weak positive correlation between ensemble spread and ensemble mean errors.

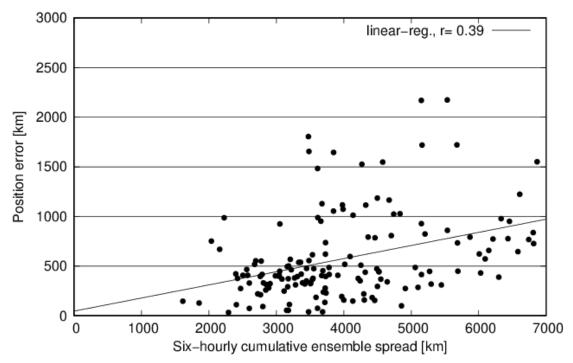


Figure 4.12 Relationship between six-hourly cumulative ensemble spread in TC position forecasts (km) and ensemble mean forecast position errors (km) in 126-hour predictions in 2024. The solid line represents a linear regression fit, with a correlation coefficient (r) of 0.39.

4.4 Verification for Other Guidance Models

4.4.1 Verification by WGNE

The Center utilizes other guidance models in addition to JMA's NWP models for operational TC track and intensity forecasting, including global deterministic NWP models from seven other centers (BOM, CMC, DWD, ECMWF, KMA, NCEP and UKMO). These models (as well as the Meteo France (FRN) model) are verified under the framework of WGNE (the Working Group on Numerical Experimentation), which is a collaborative working group for development of Earth system models (design, implementation, error diagnosis and model revision) across the full range of temporal and spatial scales. JMA works on intercomparison of these models under this framework. Figures 4.13 and 4.14 show the results of the verification for center positions and 72-hour intensity forecasts by WGNE.

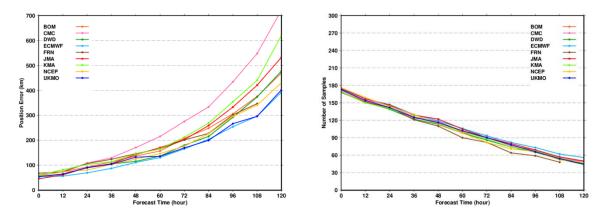


Figure 4.13 (Left) Positional errors for 2024 named TCs. The tropical depression (TD) stage and the extratropical cyclone (L) stage of targeted TCs is also included in this verification. (Right) Sample numbers.

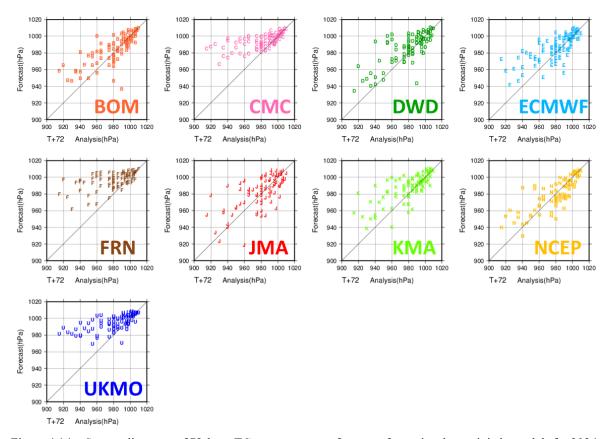


Figure 4.14 Scatter diagrams of 72-hour TC center pressure forecasts from nine deterministic models for 2024. The tropical depression (TD) stage and the extra-tropical cyclone (L) stage of targeted TCs are also included in this verification.

4.4.2 Verification of Intensity Guidance Models

Table 4.8 shows mean central pressure and maximum wind speed errors in TIFS and LGEM intensity guidance and related consensus. This section describes a verification of the latest guidance data available for each initial time of real-time operation conducted for RSMC operational forecasting.

Table 4.8 Mean errors and RMSEs of central pressure (top) and maximum wind speed (bottom) forecasts from intensity guidance models produced by the Center in 2024. Num. represents the number of samples.

		24-h	our For	ecast	48-h	our For	ecast	72-h	our For	ecast	96-h	our For	ecast	120-1	nour For	ecast
Predict	ion	Error	RMSE	Num.	Error	RMSE	Num.									
		(hPa)	(hPa)		(hPa)	(hPa)		(hPa)	(hPa)		(hPa)	(hPa)		(hPa)	(hPa)	
Intensity guidance	TIFS	-1.8	11.6	389	-2.9	14.9	297	-1.6	16.7	225	-1.6	18.5	154	-0.1	20.6	95
model	LGEM	0.9	12.6	389	1.2	14.9	297	0.9	15.7	225	-1.8	18.7	154	-2.8	24.2	95
Consensus method	TIFS&LGEM	-0.5	11.6	389	-0.8	14.1	297	-0.4	15.7	225	-1.7	18.2	154	-1.4	21.9	95

-		24-h	our For	ecast	48-h	our For	ecast	72-h	our For	ecast	96-h	our For	ecast	120-l	nour Fo	recast
Predict	ion	Error	RMSE	Num.												
		(m/s)	(m/s)		(m/s)	(m/s)		(m/s)	(m/s)		(m/s)	(m/s)		(m/s)	(m/s)	
Intensity guidance	TIFS	-0.3	5.5	389	-0.1	7.0	297	-1.2	7.5	225	-2.0	8.4	154	-2.8	10.0	95
model	LGEM	-0.7	5.9	389	-0.3	6.9	297	-0.6	7.4	225	-0.3	8.5	154	-0.3	10.8	95
Consensus method	TIFS&LGEM	-0.5	5.6	389	-0.2	6.9	297	-0.9	7.3	225	-1.1	8.3	154	-1.6	10.2	95

4.5 Verification of AMV-based Sea-surface Winds (ASWinds)

JMA produces Atmospheric Motion Vectors (AMVs) using successive satellite imagery from the Himawari-8/9 geostationary satellite. These are derived from the Full-disk observation conducted every 10 minutes and Region 3 tropical cyclone observation conducted over an area of 1,000 square kilometers every 2.5 – 5 minutes. Since July 2017, the Center has used the AMV-based Sea-surface Winds (ASWinds) product based on low-level AMVs (assigned below 700 hPa level) to estimate sea-surface winds in the vicinity of TCs. The ASWinds are derived at intervals of 10 – 30 minutes with frequent and wide-ranging wind distribution information. Figure 4.15 shows the distributions of ASWinds derived using the Full-disk and Region 3 observations by Himawari-9 for TY Shanshan (2410). The wide-area coverage and high temporal resolution of ASWinds data are also expected to support real-time determination of 30-kt wind radii for TC areas where low-level clouds appear in Himawari-8/9 imagery together with surface wind observations from satellite microwave scatterometers such as the ASCAT units on board MetOp polar-orbiting satellites (referred to here as "ASCAT winds").

The Center verified the quality of ASWinds data from Visible (B03: $0.64~\mu m$) and Infrared (B13: $10.4~\mu m$) with respect to ASCAT wind data in the vicinity of 26 TCs occurring in 2024 (Table 4.9). Wind speed biases in ASWinds data from Full-disk and Region 3 observation were small at -0.7 to -0.5 m/s, and -0.4 to -0.2 m/s, respectively. Vector differences in ASWinds from Region 3 observation were slightly larger than those from Full-disk observation, which suggested that the use of high-frequency Region-3 observation data supports tracking to determine the movement of low-level cloud associated with mesoscale phenomena.

The mean distribution of ASWinds data from Full-disk and Region-3 observation (Figure 4.16) for 2024 suggests that the representation of Region-3 ASWinds is higher than that of Full-disk ASWinds, particularly near TC centers. This is attributed to the higher temporal frequency of Region-3 imagery.

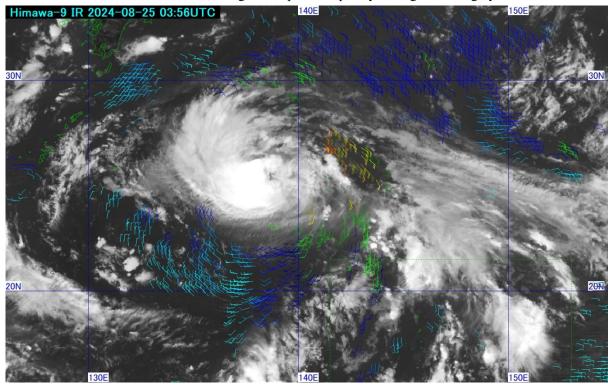


Figure 4.15 ASWinds derived from a series of Himawari-9 Full-disk and Region 3 Infrared (B13) images for TY Shanshan (2410) at 0356 UTC on 25 August 2024.

Table 4.9 Vector Differences and biases of ASWinds (0.85 < QI: Quality Indicator) with reference to ASCAT winds within a square of 20 degrees centered at the TC center for 26 TCs in 2024.

(a) ASWind (Full-disk)

	Number of	Vector Difference	Bias
	collocations	[m/s]	[m/s]
B03 (VIS)	378047	1.8	-0.5
B13 (IR)	324036	1.9	-0.7

(b) ASWind (Region 3)

	Number of	Vector Difference	Bias
	collocations	[m/s]	[m/s]
B03 (VIS)	846744	2.6	-0.2
B13 (IR)	740367	2.8	-0.4

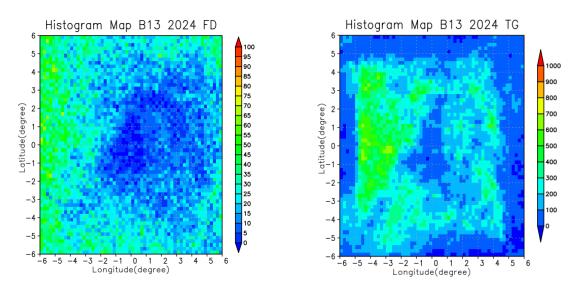


Figure 4.16 Spatial distributions of Full-disk (left) and Region 3 (right) ASWind data derived from Infrared (B13) images within a square of 12 degrees centered at TC center for 26 TCs in 2024.

4.6 Verification of TC Central Pressure Estimates Based on Satellite Microwave Observations

The Center uses TC central pressure (Minimum Sea Level Pressure, or MSLP) estimates based on TC warm core intensity (i.e., the maximum temperature anomaly near the TC center) from microwave sounders on board polar-orbiting satellites as reference for the Center operational TC analysis. The Advanced Microwave Sounding Unit-A (AMSU-A) of the NOAA and MetOp series of polar-orbiting satellites has been used for MSLP estimation since 2013. The Center also began to use data from the Advanced Technology Microwave Sounder (ATMS) on board the Suomi-NPP and JPSS-1 (NOAA-20) satellites in 2015. The higher spatial resolution of ATMS observation (32 km at the sub-satellite point) as compared to AMSU-A (48 km) enables more accurate determination of warm core intensity. Figure 4.17 shows the MSLP estimates based on AMSU-A and ATMS observations (referred to here as AMSU/ATMS estimates) together with MSLP estimates based on the Dvorak technique (Dvorak estimates) and a product based on consensus between AMSU/ATMS estimates and Dvorak estimates (CONSENSUS) for TY Ampil (2407).

Table 4.10 shows the results of AMSU and ATMS estimate verification with respect to JMA best track data for 2015 - 2024 together with Dvorak TC intensity estimates and CONSENSUS. The biases and root mean square errors (RMSEs) of AMSU estimates were -5.5 to 2.7 hPa and 8.9 to 14.0 hPa, respectively (Table 4.10a). It should be noted that the RMSE of CONSENSUS between AMSU estimates and Dvorak estimates is consistently smaller than that for AMSU and Dvorak estimates over a period of 10 years, which is attributed to the benefits of independent information from the satellite microwave observation. The RMSE for ATMS estimates was smaller than that for AMSU (Table 4.10b), which indicates that the higher resolution of ATMS observation as compared to AMSU leads to more accurate determination of TC warm core intensity. As with the AMSU estimate result, the RMSEs of CONSENSUS between ATMS and Dvorak estimates were smaller than those of ATMS and Dvorak estimates. The superiority of CONSENSUS to individual estimates is seen in bias comparison.

Use of AMSU/ATMS estimates via CONSENSUS is expected to support the Center's operational TC intensity analysis, particularly when in-situ observation data are scarce and operational TC intensity analysis depends largely on the Dvorak estimates.

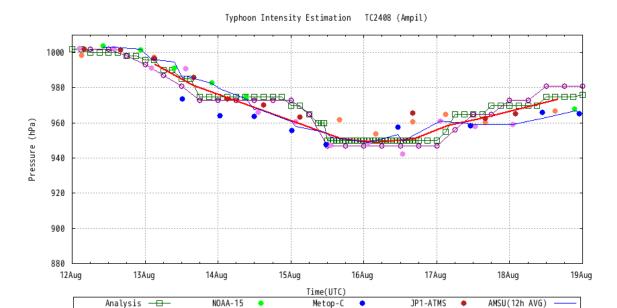


Figure 4.17 Time-series representation of Dvorak MSLP estimates, microwave-based MSLP estimates (AMSU and ATMS), CONSENSUS between Dvorak and AMSU/ATMS estimates and JMA analysis for TY Ampil (2407) on the Numerical Typhoon Prediction (NTP) website

NPP-ATMS

Table 4.10 (a) Bias and RMSE of Dvorak MSLP estimates, AMSU MSLP estimates and CONSENSUS between Dvorak and AMSU estimates with respect to the best track data for the previous 10 years (2015 - 2024); (b) as per (a) but for ATMS estimates

(a) BIAS and RMSE of central pressure estimates to best track for AMSU

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	Year	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024
BIAS	AMSU	1.3	2.7	-2.9	-3.1	-2.5	-5.5	-2.9	-1.9	-0.6	-0.4
(hPa)	Dvorak	0.1	-2.1	-2.0	-0.4	-2.9	-2.8	-2.1	-1.8	-0.3	-3.1
	Consensus	0.3	-0.8	-2.6	-1.5	-3.2	-4.0	-2.8	-2.2	-0.8	-2.3
RMSE	AMSU	12.8	13.8	10.0	12.4	11.7	14.0	13.1	11.3	12.6	8.9
(hPa)	Dvorak	7.5	9.6	7.2	7.0	9.2	8.4	7.9	6.5	8.6	9.0
	Consensus	6.8	8.2	6.7	6.7	7.6	7.9	6.6	6.3	6.2	6.7
Nun	ber of Data	819	595	569	680	645	478	703	473	398	470

(b) BIAS and RMSE of central pressure estimates to best track for ATMS

<u>/</u>		1									
	Year	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024
BIAS	ATMS	3.0	4.1	1.8	0.9	1.9	0.9	1.7	1.1	2.9	1.9
(hPa)	Dvorak	-0.5	-1.4	-2.0	-0.9	-3.7	-3.6	-2.1	-2.7	-1.4	-1.4
	Consensus	0.8	0.3	-0.7	-0.3	-1.9	-1.8	-0.9	-1.2	-0.1	-0.3
RMSE	ATMS	11.9	13.0	8.7	11.4	9.9	9.0	10.9	8.1	11.8	8.1
(hPa)	Dvorak	7.8	8.5	7.9	7.9	9.7	9.6	8.5	8.0	8.3	8.2
	Consensus	6.1	7.1	6.3	7.0	7.1	6.0	6.0	5.7	5.4	5.9
Numb	er of Data	229	190	193	224	244	148	159	116	136	139

4.7 Verification of Storm Surge Prediction

Storm surge predictions have been provided since 2011 via the Numerical Typhoon Prediction (NTP) website to Typhoon Committee Members within the framework of the Storm Surge Watch Scheme (SSWS). The Asia-area storm surge ensemble prediction system has been operational and probabilistic forecast products up to five days ahead have been provided since August 2022. For details of the system and the SSWS forecast products, refer to Hasegawa et al. (2023) on the NTP website. Verification of deterministic storm surge predictions was conducted on data from 10 stations (Table 4.11) for which sea level observation information is provided on the University of Hawaii Sea Level Center (UHSLC) database website (https://uhslc.soest.hawaii.edu/data/?fd) and the Global Sea Level Observing System (GLOSS) website (https://www.ioc-sealevelmonitoring.org/index.php) for all named TCs that formed in 2024. Hourly hindcast data (from T = -5 to T = 0) and forecast data (from T = 1 to T = 132) were compared with observation data. Ensemble predictions were also verified with information including data from the Shek Pik tide station (Hong Kong) for TY Yagi (2411).

Table 4.11 Stations used for verification

	Station	Abbreviation	Member	Data Source
1	Quarry Bay	QB	Hong Kong, China	UHSLC
2	Shek Pik	SP	Hong Kong, China	GLOSS
3	Langkawi	LK	Malaysia	UHSLC
4	Legaspi Port	LG	the Philippines	UHSLC
5	Manila South Harbor	ML	the Philippines	UHSLC
6	Subic Bay	SB	the Philippines	UHSLC
7	Quy Nhon	QN	Viet Nam	UHSLC
8	Vung Tau	VT	Viet Nam	UHSLC
9	Busan	BS	Republic of Korea	GLOSS
10	Apra Harbor	AP	U.S.A.	UHSLC

Table 4.12 Storm surges exceeding 0.5 m observed at 10 stations for each named TC that formed in 2024

Station	Named TC	Storm surge [m]
SP	Yagi (2411)	0.55
QB	Krathon (2418)	0.59
SP	Krathon (2418)	0.54
QB	Trami (2420)	0.51
SP	Trami (2420)	0.52
QB	Man-yi (2424)	0.61
SP	Man-yi (2424)	0.65

4.7.1 Deterministic Prediction

Storm surges exceeding 1.0 m were not observed in any of 10 stations in 2024 (Table 4.12). Figure 4.18 shows scatter diagrams of modeled storm surges (hindcast and forecast) against observation data. Verification results for 2024 indicate that deterministic predictions are generally consistent with observation data, although prediction errors are somewhat large for T+97-120.

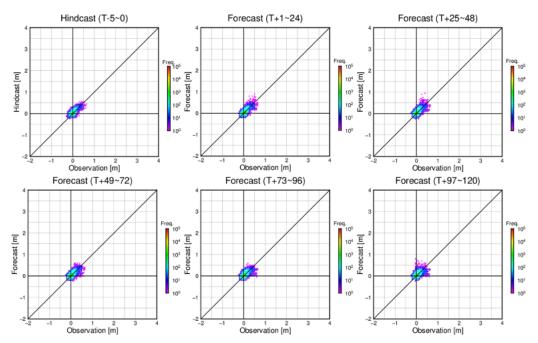


Figure 4.18 Scatter diagrams of modeled storm surges against observation data from 10 stations for all the named TCs that formed in 2024 (top left: hindcast; others: forecast).

The verification results shown in Figure 4.18 may be insufficient to evaluate model accuracy for TCs, given that there were sparse observation data for verification and/or that remarkable storm surges were not observed at most stations. Accordingly, additional verification was conducted using data from stations in Japan, where sufficient observation data are available and TCs frequently approach or make landfall. Although the characteristics of model forecasts may vary by region, the system is considered to have comparable accuracy at storm surge watch scheme stations.

Figure 4.19 shows scatter diagrams of modeled storm surges (forecast) against observation data from around 200 stations (operated by JMA, the Ports and Harbours Bureau, the Japan Coast Guard, and the Geospatial Information Authority of Japan) in Japan. The verification period is from January to December 2024, and cases of TCs are extracted. Eleven named TCs approached the country, including STS Maria (2405) and TY Shanshan (2410) making landfall. The diagrams indicate that forecasts for Japan compare well with observed storm surges, although some predictions exhibit significant errors (mainly due to large track prediction errors of TY Shanshan (2410)). Naturally, prediction errors increase with lead time.

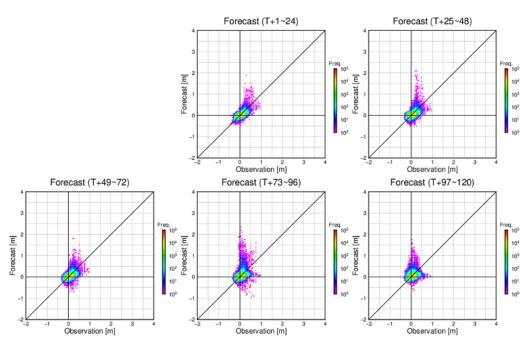


Figure 4.19 Scatter diagrams of modeled storm surges (forecast) against observation data from around 200 stations (operated by JMA, the Ports and Harbours Bureau, the Japan Coast Guard, and the Geospatial Information Authority of Japan) in Japan for TCs in 2024. All plots are three-hourly maximum values.

4.7.2 Ensemble Prediction

Figure 4.20 presents threat scores of ensemble prediction in Japan for TCs in 2024. The verification period and observation data used are as per those for deterministic forecast verification in 4.7.1. The results show low scores throughout the forecast period, even though the storm surge threshold was set to a relatively low 0.5 m. These reduced scores are attributed to significant prediction errors for specific typhoons (e.g., TY Shanshan (2410), 4.7.1) and a low number of remarkable storm surges.

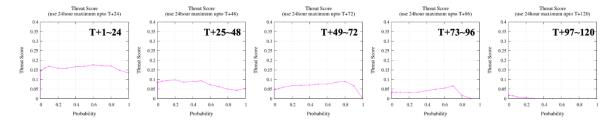


Figure 4.20 Threat scores of the ensemble prediction system for each probability against storm surges exceeding 0.5 m at around 200 stations in Japan in 2024.

4.7.3 Case Study

In September 2024, TY Yagi (2411) crossed Luzon Island in the Philippines and moved westward over the South China Sea, developing to a maximum sustained wind speed of 105 kt and a minimum pressure of 915 hPa. Figure 4.21 shows the best track and all predicted tracks (official forecast and 51 tracks calculated using GEPS) covering the 72-hour period before the storm surge peaked in Shek Pik. The official forecast competently predicted the track, and temporal variations in the storm surge with the typhoon approaching were also appropriately predicted for Shek Pik (Figure 4.22; observed maximum: 0.55 m; predicted maximum: 0.51 m).

In the ensemble system, tracks were moderately spread around the official forecast track (Figure 4.21), and were considered suitable for evaluation of potential storm surges. The system predicted the potential for storm surges exceeding 1.0 m around Hong Kong and Hainan Island (Figure 4.23). In Shek Pik, some members predicted significantly large storm surges (ensemble maximum 2.49 m; Figure 4.24), although no such conditions were actually observed. However, it is notable that the system was able to capture the risk of remarkable storm surges in the early stages of typhoon approach.

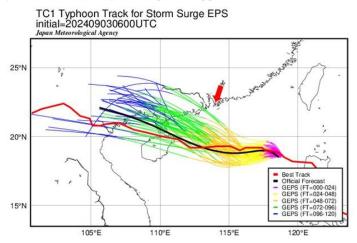


Figure 4.21 Best track and predicted tracks for TY Yagi (2411). In the figure, colored thin lines show the 51 tracks from GEPS members, and the bold red and black lines show the best track (6-hourly data) and the official forecast, respectively. The red arrow shows the location of Shek Pik.

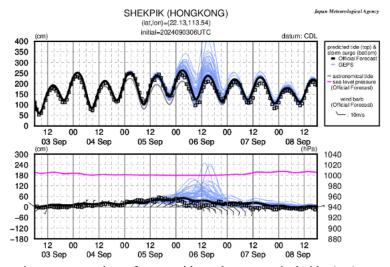


Figure 4.22 Time-series representation of storm tide and astronomical tide (top), storm surge, sea-level pressure and surface wind (bottom) for Shek Pik. Squares show hourly observation data.

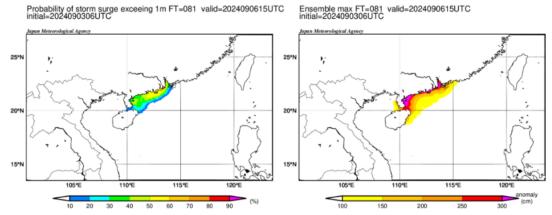


Figure 4.23 Probability of storm surges exceeding 1.0 m (left) and ensemble maxima (right).

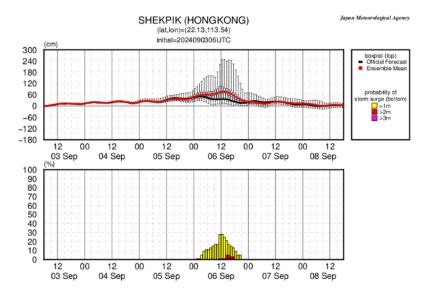


Figure 4.24 Time-series representation of storm surge boxplots (top), storm surge probability bars (bottom) for Shek Pik.

[Reference]

Hasegawa. H., N. Kohno, and H. Hayashibara, 2012: JMA's Storm Surge Prediction for the WMO Storm Surge Watch Scheme (SSWS). *RSMC Tokyo-Typhoon Center Technical Review*, **14**, 13-24.

Hasegawa. H., N. Kohno, M. Higaki, and M. Itoh, 2017: Upgrade of JMA's Storm Surge Prediction for WMO Storm Surge Watch Scheme (SSWS). *RSMC Tokyo-Typhoon Center Technical Review*, **19**, 26-34.

Hasegawa. H., J. Sugano, T. Fukuura and M. Higaki, 2023: Upgrade of JMA's Storm Surge Prediction for WMO Storm Surge Watch Scheme (SSWS) in 2022. *RSMC Tokyo-Typhoon Center Technical Review*, **25**, 1-14.

Appendices

Appendix 1 RSMC Tropical Cyclone Best Track Data in 2024

Color Colo					Central				-			Central							Central			
TY CAPMINAR (2403) TY GAMM (2403) THE ALL PROPERTY AND ALL P	Date	e/Time	Center	Position	pressure	Max Wind	CI num	. Grade	Date/Time			pressure	Max Wind	CI num.	. Grade	Date/Time	Center	Position	pressure	Max Wind	CI num.	Grade
Mart		(UTC)							(UTC)							(UTC)						
24/08 64 1235 1066 - 10 TD 19/08 126 1225 1026 - 10.5 TD 10.5 TD 19/08 126 1225 1026 - 10.5 TD 10.5						(401)							403)							405)		
24/12 103 123 106 104 105 107	May					-							-							-		
24/16 13.23 1066 - 20 TO 19/16 146 126 106 - 15 TO 106 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 100 20 2																				_		
24/06 123 1233 1064 - 20 TD 29/07 152 1255 1002 40 20 41 41 41 41 41 41 41 4						_							-							_		
250.00 123 1238 1066 - 20 170 290.00 162 1279 100 00 00 25 175 100.00 25 175 100.00 25 175 100.00 25 175													25							_		
287-16 13-7 12-18 1900 - 2.0 TO 297-12 163 1208 908 40 25 TS 697-18 201 41-1 998 - 15 TO 257-18 13-7 12-18 1900 - 2.0 TO 297-18 1900 -						_														_		
227/16 13.4 122.3 1000 35 25 75 20.1 10.5 122.7 124.8 14.8 29.8 -1.5 10.5 10.5 122.6 124.8																				_		
24.00 14.1 12.14 948 50 30 51 30 30 51 30 51 30 51 30 51 30 51 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 51 30 30 30 51 30 30 30 51 30 30 30 30 30 30 30 3																				_		
240.00 14.1 121.4 994 50 20 STS 210.00 10.4 125.00 91.00 30 STS 207.10 225.01 240.00 14.00 220.00 22																				_		
28.00 14.3 12.17 19.00 15.0 3.5 575 21.17 16.5 12.25 19.5																				_		
24/16 15 1222 890 65 40 TY 21/18 163 1225 890 60 35 STS 006/00 224 140 994 40 25 TS 27/10 172 1225 190 65 40 TY 99/16 224 143 990 40 25 TS 27/10 172 1239 190 190 172 1230 1230 172 1230 1230 172 1230 123																07/18	25.7	142.7	996	35	2.0	TS
247.08 15.5 122.5 975 70 4.5 TV 22.00 17.2 125.5 980 65 4.0 TV 08.072 27.6 14.6 12.5 18.5 19.5 10.5						65										08/00	26.6	144.0	994	40	2.5	TS
27/00 15.8 122.8 970 75 50 TY 22/12 12.5 980 65 4.0 TY 08/18 28.8 43.6 809 50 35 STS 22/14 17.2 12.5 23.9 37.0 50 TY 22/12 12.5 23.0 37.0 50 TY 08/18 28.8 43.6 809 50 35 STS 22/14 17.2 17.2 23.9 37.0 30 TY 22/12 12.5 30.0 30 TY 08/18 28.8 43.6 809 50 30 STS 23.0		26/18	15.5	122.5	975	70	4.5	TY								08/06	27.6	144.7	990	45	2.5	TS
27/12 12 12 13 13 14 15 15 15 15 15 15 15		27/00	15.8	122.8	970	75	5.0	TY								08/12	28.7	145.3	985	50	3.0	STS
27/16 174 172 172 172 172 173 175		27/06	16.4	123.5	970	70	5.0	TY								08/18	29.8	145.6	980	55	3.5	STS
227.16 17.8 17.8 17.8 17.5 17.5 17.7 23.00 19.5 12.1 97.0 75 5.0 TY 09.7 31.40 98.0 55 3.5 STS 220.00 18.1 12.5 12.5 97.5 65 4.5 TY 23.00 20.1 22.0 17.0 75 5.0 TY 09.7 20.1 4.1 4.1 4.1 4.1 1.1 1.1 1.1 1.1 1.1 1		27/12	17.2	123.9	970	70	5.0	TY								09/00	30.8	146.0	980	55	3.5	STS
224/10 21.1 128.2 975 65 4.5 TY 224/15 226 1249 965 75 5.0 TY 000/18 34.2 1460 960 55 5.5 STS 224/18 23.0 1293 975 66 4.5 TY 234/15 226 1239 965 6.5 5.5 TY 10/09 380 1460 965 50 3.5 STS 224/08 23.1 13.6 960 10 4.0 STS 23/12 13.1 33.4 94.6 5.5 - TY 10/10 37.6 146.2 965 3.5 STS 224/08 23.1 13.6 960 10 4.0 STS 23/12 13.1 33.4 94.6 5.5 - TY 10/10 37.6 146.2 965 3.5 STS 224/08 23.1 13.6 960 10 4.0 STS 23/12 13.1 33.4 94.6 5.5 - TY 10/10 37.6 14.2 960 50 3.5 STS 24/09 23.1 13.6 96.0 10 4.0 STS 23/12 13.1 13.4 94.6 5.5 - TY 10/10 37.6 14.4 180 50 1.0 STS 24/09 23.1 13.6 96.0 10 4.0 STS 24/09 23.1 12.3 95.0 0 - TY 11/10 37.8 143.6 98.0 50 1.0 STS 24/09 23.1 12.3 95.0 0 - TY 11/10 37.8 143.6 98.0 50 1.0 STS 24/09 24.1 12.2 96.0 ST		27/18	17.8	124.5	970	70	5.0	TY				970										
28.11 29.11 1922 97.5 65 4.5 TY 23.18 22.8 23.5 50.8 0.5 TY 10.00 30.0 140.0 88.5 45.5 TS		28/00	18.5	125.5	975	65	4.5	TY	23/06	20.7		970	75	5.0	TY							
28.00 29.0		28/06	19.8	126.6	975	65	4.5	TY	23/12	22.0	124.5	965	75	5.0	TY							
29/00 243 1309 380 80 40 40 57S 23/21 251 1234 845 85 58 77 70 70 71 365 1852 800 50 30 57S		28/12	21.1		975	65	4.5		23/15	22.6	123.9	955	80	-	TY							
28/06 28/2 1316 880 80 STS 24/06 238 1232 846 88 5.5 TV 10/18 890 80 30 30 STS 28/07 28/2 1318 88 80 80 STS 24/08 238 1232 846 88 5.5 TV 11/08 37, 1433 980 50 30 STS 28/08 24 1219 980 60 TV 11/08 37, 1433 980 50 30 STS 28/08 24 1219 980 60 TV 11/08 37, 1433 980 50 30 STS 30/07 28 3183 398 40 25 TS 24/08 24 1219 980 60 TV 11/12 37, 1433 980 50 STS 30/08 28 38 38 38 38 38 38 3						65	4.5		23/18	22.8	123.5	950	85	5.5	TY							
29/19 28 1322 380 60 40 51 St 29/19 29 1 37 St 34/00 20 122 38 35 St 34/00 20 122 38 35 St 34/00 20 20 120 37 St 34/00 20 20 120 30 30 St 35 St 34/00 20 20 120 37 St 34/00 20 20 20 120 37 St 34/00 20 20 20 120 37 St 34/00 20 20 20 20 20 20 20 20 20 20 20 20 2									23/21	23.1	123.4	945	85	-	TY							
24 13 13 13 13 13 13 13 1									24/00	23.6	123.2	945	85	5.5	TY							
24/18 275 1344 980 80 80 85 85 85 85 85											122.9	935		-								
24 19 25 19 19 26 19 27 28 19 29 28 28 30 30 30 30 30 30 30 3																						
30/10/2 289 1399 986 40 2.5 TS 24/16 24.9 121.9 990 95																						
30/12 288 138.9 998 40 2.0 TS																						
31/10 31/4 1377 598																					3.0	
310 330 1401 1000						40																
31/106 349 1432 996 L 25/106 252 119/ 91/5 950 50 45 STS 12/00 390 1417 992 45 30 TS 31/12 365 1468 994 L 25/18 257 1183 980 45 40 TS 31/12 365 1468 994 L 25/18 257 1183 980 45 40 TS 31/18 360 1509 992 L 26/00 264 1183 985 45 40 TS 31/106 405 1592 992 L 26/00 264 1183 985 45 40 TS 31/106 405 1592 992 L 26/00 264 1183 985 45 40 TS 31/10 31 1551 1992 992 L 26/00 264 1183 985 45 40 TS 31/10 31 1551 1992 992 L 26/00 264 1183 985 45 40 TS 31/10 31 1551 1992 992 L 26/00 26/12 279 1185 992 - 25 TD 31/10 1184 300 1665 992 L 26/18 279 1155 992 - 25 TD 31/10 1184 300 1665 992 L 26/18 279 1155 992 - 25 TD 31/10 1184 300 1665 992 L 27/10 286 1147 996 TD 31/10 1417 4134 1390 1006 - 20 TD 31/10 1417 4134 1390 1006 - 10 TD 31/10 1417 4134 1415 1000 - 10 TD 31/10 1417 4134 1415 1415 1415 1415 1415 1415 1415																					_	
31/12 365 1648 994 L						_	_													45	3.0	
31/18 380 1509 992 L 28/08 275 1182 985 40 35 TS 12/12 404 1405 985 - 30 TS 12/12 404 1405 985 - 25 TD 10/106 405 1582 992 L 28/08 275 1187 985 35 30 TS 12/12 414 1390 1004 - 2.0 TD 10/112 415 1502 992 L 28/08 275 1187 985 35 3.0 TS 12/12 414 1390 1004 - 2.0 TD 10/112 415 1502 992 L 28/08 275 1187 985 35 3.0 TS 12/12 414 1390 1004 - 2.0 TD 10/112 415 1502 992 L 28/08 275 1187 985 35 3.0 TS 12/12 414 1390 1004 - 2.0 TD 10/12 415 1502 992 L 28/08 275 1187 992 - 2.5 TD 13/06 423 1390 1004 - 2.0 TD 10/10 14/12 415 1900 - 1.5 TD 10/10 14/12 415 1900 -						_	_									12/03	39.3	141.2	994	40	-	TS
Jun. 01/00 991 1551 992 L 26/06 275 1175 992 992 L 28/12 279 1168 990 35 3.0 TS 12/12 404 1398 1002 - 2.5 TD 01/06 405 1592 992 L 28/12 279 1168 990 35 3.0 TS 12/18 411 1394 1002 - 2.0 TD 01/18 430 1685 992 L 28/12 279 1168 990 35 3.0 TS 12/18 411 1394 1002 - 2.0 TD 01/18 430 1685 992 L 27/00 284 1152 996 - 2.5 TD 13/06 423 1390 1004 - 2.0 TD 02/06 465 1743 992 L 27/00 284 1152 996 - 2.5 TD 13/06 423 1390 1006 - 2.0 TD 02/06 462 1791 992 L 27/06 286 1147 996 TD 13/18 422 1390 1006 - 2.0 TD 02/06 462 1791 998 98 D 04 27/18 286 1145 996 TD 14/06 414 1394 1006 - 1.5 TD 04/06 285 1199 1000 TD 14/06 414 1944 418 1006 - 1.5 TD 04/06 285 1199 1000 0.5 TD 04/06 285 1199 1000 0.5 TD 04/06 285 1199 1000 0.5 TD 04/06 285 1199 1000 1.5 TD 04/07 1410 1410 1410 1418 1415 1006 - 1.5 TD 04/07 1410 1410 1410 1410 1410 1410 1410 14						_	_									12/06	39.9	140.5	998	-	3.0	TD
OFFICE Contemporary Contempora	Jun.					_	_									12/12	40.4	139.8	1002	-	2.5	TD
01/12 41.5 16.29 992 L 20/18 27.9 115.5 993 - 2.5 TD 13/06 41.4 139.0 1004 - 2.0 TD 01/18 43.0 168.5 992 L 27/06 28.4 115.2 996 - 2.5 TD 13/12 42.2 139.0 1006 - 2.0 TD 02/02 44.6 174.3 992 L 27/06 28.6 114.7 996 TD 13/18 42.2 139.0 1006 - 2.0 TD 02/12 47.9 184.9 988 Dut 27/12 29.1 114.0 998 TD 14/16 41.2 14.0 14.1 19.4 1006 - 1.5 TD 28/06 29.5 113.6 998 TD 14/06 41.2 14.0 1006 - 1.5 TD 14/06 41.2 14.0 14.1 19.4 10.0 1.0 1.5 TD 14/06 41.2 14.0 14.1 19.4 10.0 1.5 TD 14/06 41.2 14.0 14.1 19.4 10.0 1.5 TD 14/06 41.2 14.0 14.1 19.4 10.0 1.0 1.5 TD 14/06 41.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0						_	_									12/18	41.1	139.4	1002	-	2.0	TD
01/18 43,0 168,5 992 L 27/00 28,4 115,2 894 - 2.5 TD 13/06 42,3 139,0 1004 - 2.0 TD 10/06 20/07 20						_	_									13/00	41.4	139.0	1004	-	2.0	TD
Control Cont						_	_									13/06	42.3	139.0	1004	-	2.0	TD
02/06 462 1791 992 L 27/12 29.1 114.0 998 TD 13/06 42.1 39.4 1006 - 15.5 TD 28/07 124.0 1006 - 15.5 TD 14/06 41.2 1402 1006 1006 - 15.5 TD 14/06 41.2 1402 1006 - 15.5 TD 14/06 41						_	_									13/12				-		
		02/06	46.2	179.1	992	-	-	L					_							-		
Date/Time Center Position Center Position Center Position Center Cen		02/12	47.9	184.9	988	-	-	Out												-		
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TS MALIKSI (2402) TS M													_				41.6	141.5	1006	-	1.5	
May 30/00 18.0 111.9 1002 0.0 TD 29/00 1.0 TD 29/00 1.0 TD 29/00 -	Date	e/Time	Center	Position		Max Wind	CI num.	Grade					_			14/18						Dissip.
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30/12 18.3 111.9 1000 - 1.0 TD						_										(UTC)						
Solid 18.9 11.2 10.00 - 1.5 TD 11.5 TD 11.5 TD 11.5 TS STS PRAPIROON (2404) 11.6 10.00						_			Date/Time	Center	Position		Max Wind	CI num.	Grade		TS	SON-	-TINH ((2406)		
31/00 198 11/26 998 35 1.5 TS		30/18	18.9	112.2	1000	-	1.5	TD	(UTC)	Lat (N)	Lon (E)		(k+)			Aug. 10/12	26.5	154.1	1000	-	0.5	TD
31/06 20.3 111.9 998 35 1.5 TS Jul. 20/00 14.6 115.6 1002 - 0.0 TD 11/00 27.8 155.0 996 35 1.0 IS 31/18 21.8 111.5 1000 - 1.5 TD 20/06 15.3 115.1 1002 - 0.5 TD 11/106 27.8 155.0 996 35 1.5 TS 31/18 21.8 111.5 1000 - 2.0 TD 20/06 15.3 115.1 1002 - 0.5 TD 11/12 28.8 154.5 994 40 2.0 TS 10/10 23.4 111.8 1004 - 1.5 TD 20/18 16.1 112.1 1000 - 1.5 TD 11/18 30.2 154.4 996 35 2.0 TS 10/10 23.5 112.3 1004 - 1.5 TD 20/18 16.1 112.1 1000 - 1.5 TD 11/18 30.2 154.4 996 35 2.0 TS 10/10 23.5 112.3 1004 - 1.5 TD 21/06 16.6 111.3 998 35 2.0 TS 12/00 31.5 152.5 998 35 2.0 TS 10/18 24.8 115.2 1006 - 0.5 TD 21/06 16.6 111.3 998 35 2.0 TS 12/06 32.3 151.5 998 35 2.0 TS 12/06 24.8 115.2 1006 - 0.5 TD 21/06 16.6 111.3 998 35 2.0 TS 12/12 32.9 150.5 998 35 2.0 TS 12/06 24.8 115.2 1006 - 0.5 TD 21/06 16.6 111.3 998 35 2.0 TS 12/12 32.9 150.5 998 35 2.0 TS 12/06 24.8 115.2 1006 - 0.5 TD 21/06 16.6 111.3 998 35 2.0 TS 12/12 32.9 150.5 998 35 2.0 TS 12/06 24.8 115.2 1006 - 0.5 TD 21/12 17.5 110.6 996 40 2.0 TS 12/12 32.9 150.5 998 35 2.0 TS 12/06 24.8 12/00 1004 L 22/06 21.1 108.5 996 55 3.5 STS 13/06 36.1 146.7 1000 35 1.5 TS 12/06 23.8 12/3 1004 L 22/06 20.1 108.5 985 55 3.5 STS 13/06 36.1 146.7 1000 35 1.5 TS 12/06 23.8 12/3 1004 L 22/12 20.5 108.1 985 55 3.5 STS 13/06 36.1 146.7 1000 35 1.5 TS 12/06 23.8 12/3 10.0 10.4 L 22/18 10.0 10.0 TD 14/18 38.7 145.6 1006 - 1.5 TD 14/18 24.9 13.4 14.8 10.0 10.4 L 22/18 21.1 107.8 985 55 3.5 STS 13/06 36.1 146.7 1000 35 1.5 TS 12/12 23.9 150.5 998 35 1.5 TS 13/06 36.1 146.7 1000 4.5 TS TD 14/18 38.7 145.6 1006 - 1.0 TD 14/18 24.9 13.4 14.8 1004 L 23/12 21.5 106.7 994 TD 14/18 44.6 150.4 1004 L 23/12 21.5 106.6 994 TD 14/18 44.6 150.4 1004 L 24/08 21.5 106.6 994 TD 15/04 47.5 15.7 1000 L 10/10 10.0 10.0 10.0 10.0 10.0 10.0 10.		31/00	19.8	112.6	998	35	1.5	TS	(610)					1		10/18	26.8	155.0	998	-	1.0	TD
31/12 21 11.3 1000 - 1.5 1D 20/06 15.3 115.1 1002 - 0.5 TD 11/12 28.8 154.5 994 40 2.0 TS 31/18 21.8 111.5 1000 - 2.0 TD 20/12 15.7 113.6 1002 - 1.0 TD 11/12 28.8 154.5 994 40 2.0 TS 01/06 23.5 112.3 1004 - 1.5 TD 20/18 16.1 112.1 1000 - 1.5 TD 11/18 30.2 154.4 996 35 2.0 TS 01/12 240 113.4 1004 - 1.0 TD 21/00 16.0 111.3 998 35 2.0 TS 01/18 24.8 115.2 1006 - 0.5 TD 21/06 16.6 111.1 998 35 2.0 TS 01/18 24.8 115.2 1006 - 0.5 TD 21/06 16.6 111.1 998 35 2.0 TS 02/06 24.8 12.0 1004 - 1.			20.3	111.9		35			Jul 20/00				· \2704	•	TD							
Jun. 01/00						-							_									
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01/106	Jun.					-																
01/12 24.0 113.4 1004 - 1.0 ID 21/06 16.6 111.1 998 35 2.0 TS 12/06 32.3 151.5 998 35 2.0 TS 02/00 24.9 116.4 1006 - 5 TD 21/12 17.5 110.6 996 40 2.0 TS 12/12 32.9 150.5 998 35 2.0 TS 02/00 24.8 12.0 1004 - L 21/18 18.6 110.2 992 45 2.5 TS 12/18 34.2 149.2 998 35 2.0 TS 02/06 24.8 12.0 1004 - L 22/00 19.5 109.2 990 50 3.0 STS 13/00 35.2 147.8 1000 35 1.5 TS 02/18 23.8 124.2 1002 - L 22/06 20.1 108.5 985 55 3.5 STS 13/06 36.1 146.7 1000 35 1.5 TS 02/18 23.8 124.2 1002 - L 22/18 21.1 107.8 985 55 3.5 STS 13/18 38.7 145.6 1006 - 1.5 TD 03/06 24.0 128.2 1002 - L 22/18 21.1 107.8 985 55 3.5 STS 13/18 38.7 145.6 1006 - 1.5 TD 03/18 24.1 129.8 1002 - L 23/06 21.6 107.6 992 35 2.5 TS 14/06 41.7 146.5 1006 - 1.0 TD 03/18 24.5 131.6 1002 - L 23/06 21.6 107.6 992 35 2.5 TS 14/06 41.7 146.5 1006 - 1.0 TD 04/00 24.8 133.7 1004 - L 23/12 21.5 106.7 994 - 2.0 TD 14/12 43.4 148.0 1004 - TD 04/06 24.8 133.1 1004 - L 23/18 21.5 106.4 994 - TD 14/18 44.6 150.4 1004 - TD 04/18 24.9 137.3 1008 - L 24/18 21.5 106.6 994 - TD 15/06 47.3 15.7 1000 - L 24/18 24.9 137.3 1008 - L 24/18 24.9 137.3 1008 - L 24/18 21.5 106.6 994 - TD 15/06 47.5 157.7 1000 - L 24/18 24.9 137.3 1008 - L 24/18 20.8 107.4 994 - TD 15/06 45.7 157.7 1000 - L 24/18 20.8 107.4 994 - TD 15/06 45.7 157.7 1000 - L 24/18 20.8 107.4 994 - TD 15/06 45.7 158.4 990 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18 20.8 107.4 994 - TD 15/12 47.6 161.0 996 - L L 24/18						-							35									
02/00						_																
02/06						_	0.5		21/12	17.5	110.6											
02/12 23.8 123.3 1004 L 22/06 20.1 108.5 985 55 3.5 STS 13/06 36.1 146.7 1000 35 1.5 TS 02/18 23.8 124.2 1002 L 22/12 20.5 108.1 98.5 55 3.5 STS 13/12 37.0 146.0 1004 - 1.5 TD 03/06 24.0 128.2 1002 L 22/18 21.1 107.8 985 55 3.5 STS 13/18 38.7 145.6 1006 - 1.5 TD 03/12 24.1 129.8 1002 L 23/06 21.6 107.5 990 45 3.0 TS 14/00 39.8 145.7 1006 - 1.0 TD 03/18 24.5 131.6 1002 L 23/06 21.6 107.6 992 35 2.5 TS 14/06 41.7 146.5 1006 - 1.0 TD 03/18 24.5 131.6 1002 L 23/12 21.5 106.7 994 - 2.0 TD 14/12 43.4 148.0 1004 - 1.0 TD 04/06 24.8 133.7 1004 L 23/12 21.5 106.7 994 - 2.0 TD 14/18 44.6 150.4 1004 - TD 04/06 24.8 135.1 1004 L 23/18 21.5 106.4 994 TD 14/18 44.6 150.4 1004 TD 04/12 24.9 136.4 1006 L 24/00 21.6 106.5 994 TD 15/06 47.5 157.7 1002 L 04/18 24.9 137.3 1008 L 24/10 21.7 106.6 994 TD 15/06 47.5 157.7 1000 L 05/06 24.8 138.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 138.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 16/18 50.9 179.0 984 L 16/18						_	_						45									
02/18 23.8 124.2 1002 - L 22/16 20.1 108.5 985 55 3.5 STS 13/12 37.0 146.0 1004 - 1.5 TD 03/00 23.9 126.4 1004 - L 22/18 21.1 107.8 985 55 3.5 STS 13/18 38.7 145.6 1006 - 1.5 TD 03/06 24.0 128.2 1002 - L 23/00 21.5 107.5 990 45 3.0 TS 14/00 39.8 145.7 1006 - 1.0 TD 03/18 24.5 131.6 1002 - L 23/06 21.6 107.6 992 35 2.5 TS 14/06 41.7 146.5 1006 - 1.0 TD 03/18 24.5 131.6 1002 - L 23/18 21.5 106.7 994 - 2.0 TD 14/12 43.4 148.0 1004 - 1.0 TD 04/06 24.8 133.7 1004 - L 23/18 21.5 106.7 994 - TD 14/18 44.6 150.4 1004 - TD 04/12 24.9 136.4 1006 - L 24/00 21.6 106.5 994 - TD 15/06 47.3 154.7 1002 - L 24/00 21.6 106.5 994 - TD 15/06 47.3 154.7 1002 - L 24/00 21.6 106.5 994 - TD 15/06 47.5 157.7 1000 - L 24/00 21.6 106.5 994 - TD 15/06 47.5 157.7 1000 - L 24/06 21.7 106.6 994 - TD 15/06 47.5 157.7 1000 - L 24/18 20.8 107.4 994 - TD 15/06 47.5 157.7 1000 - L 24/18 20.8 107.4 994 - TD 15/06 45.8 173.1 988 - L L 25/00 Dissip.						_	_					990	50		STS							
03/00						_	_		22/06	20.1	108.5	985	55	3.5	STS							
03/06						_						985										
03/12 24.1 129.8 1002 L 23/06 21.5 107.6 992 45 3.0 1S 14/06 41.7 146.5 1006 - 1.0 TD 03/18 24.5 131.6 1002 L 23/12 21.5 106.7 994 - 2.0 TD 14/12 43.4 148.0 1004 - 1.0 TD 04/06 24.8 133.7 1004 L 23/18 21.5 106.4 994 TD 14/18 44.6 150.4 1004 TD 04/12 24.9 136.4 1006 L 24/00 21.6 106.5 994 TD 15/00 47.3 154.7 1002 L 04/18 24.9 137.3 1008 L 24/06 21.7 106.6 994 TD 15/06 47.5 157.7 1000 L 05/06 24.8 139.0 1010 L 24/12 21.7 106.6 994 TD 15/12 47.6 161.0 996 L 05/06 24.8 139.0 1010 L 24/12 21.7 106.6 994 TD 15/12 47.6 161.0 996 L 05/06 24.8 139.0 1010 L 24/12 21.7 106.6 994 TD 15/12 47.6 161.0 996 L 05/06 24.8 139.0 1010 L 24/12 21.7 106.6 994 TD 15/12 47.6 161.0 996 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/18						_	_					985	55	3.5	STS							
03/18						_	_															
04/00						_	_						35									
04/06						_	_						-							_		
04/12 24.9 136.4 1006 L 24/00 21.6 106.5 994 1D 15/06 47.5 157.7 1000 L 04/18 24.9 137.3 1008 L 24/06 21.7 106.6 994 TD 15/12 47.6 161.0 996 L 05/00 24.8 138.0 1010 L 24/12 21.7 106.6 994 TD 15/12 47.6 161.0 996 L 05/06 24.8 139.0 1010 L 24/18 20.8 107.4 994 TD 15/18 47.0 164.4 992 L 05/12 105/12						_														_	_	
04/18 24.9 137.3 1008 - L 24/16 21.7 106.6 994 - ID 15/12 47.6 161.0 996 - L 05/00 24.8 138.0 1010 - L 24/12 21.7 106.6 994 - TD 15/12 47.6 161.0 996 - L L 05/06 24.8 139.0 1010 - L 24/18 20.8 107.4 994 - TD 15/18 47.0 164.4 992 - L 05/06 24.8 139.0 1010 - L 25/00 Dissip. Distip. Dissip. Dissip.						_	_													_	_	
05/00 24.8 138.0 1010 - L 24/12 21.7 106.6 994 - ID 15/12 47.0 161.0 996 - L 05/06 24.8 139.0 1010 - L 24/18 20.8 107.4 994 - ID 15/18 47.0 161.0 996 - L 05/06 24.8 139.0 1010 - L 25/00 Dissip. 16/06 45.7 168.4 992 - L 16/06 45.8 173.1 988 - L 16/18 16/18 176.3 986 - L 16/18 50.9 179.0 984 - L 16/18 50.9 179.0 984 - L						_	_													_	_	
05/06 24.8 139.0 1010 - L 24/18 20.8 107.4 994 1D 15/18 47.0 164.4 992 L 05/12 Dissip. 16/06 45.8 173.1 988 L 16/12 47.8 176.3 986 L 16/18 50.9 179.0 984 L						_	-							-						_	_	
05/12 Dissip. 25/00 Dissip. 10/04 43.7 168.4 990 L 16/06 45.8 173.1 988 L 16/12 47.8 176.3 986 L 16/18 50.9 179.0 984 L						_	-			20.8	107.4	994	-	-						_	_	
16/06 45.8 1/3.1 988 L 16/12 47.8 176.3 986 L 16/18 50.9 179.0 984 L									25/00						Dissip.					_	-	
16/18 50.9 179.0 984 L																				_	_	
																				_	_	
17/UU 53.6 180.9 978 Out																				_	_	
																17/00	JJ.6	160.9	9/8	_	-	Out

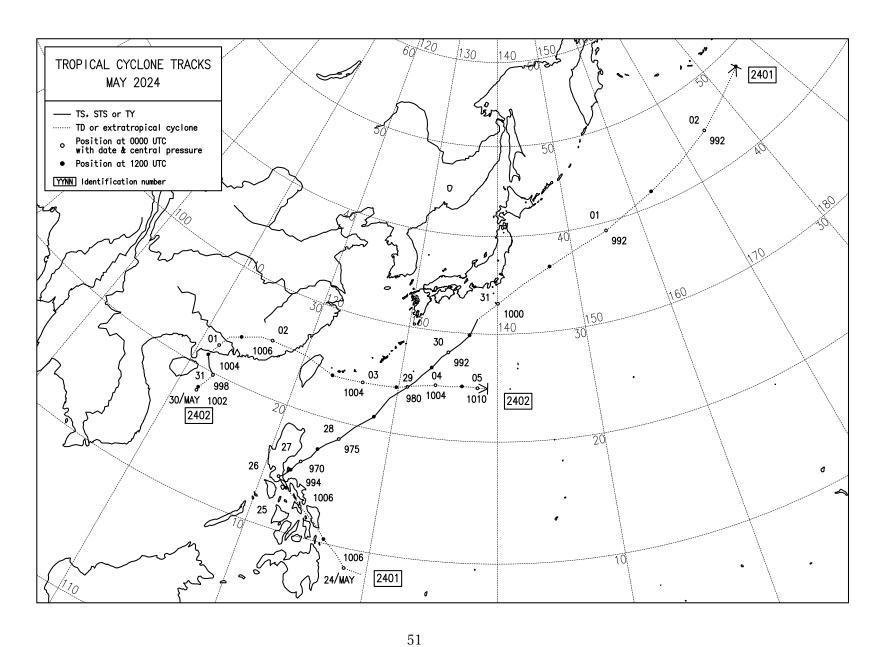
Date	/Time	Center	Position	Central pressure	Max Win	d CI num.	Grade	Dat	e/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade	Date/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)				(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)			(UTC)		Lon (E)	(hPa)	(kt)		
		Т	Y AMI	PIL (24	07)						JONG	DARI	(2409)				TY	SHAN	SHAN	(2410)		
Aug.	11/12	21.7	134.9	1002	-	0.0	TD	Aug.	18/00		126.8	1004	-	0.0	TD	Aug. 20/0		147.7	1008	-	0.0	TD
	11/18			1000	-	0.5	TD		18/06	23.8	126.5	1000	-	0.5	TD	20/1:			1010	-	0.0	TD
	12/00			1000	-	1.0	TD		18/12 18/18	24.1	126.4 126.2	998	35 35	1.0	TS TS	20/18			1008	_	0.0	TD
	12/06 12/12		136.1 136.6	998	35	1.5	TD TS		19/00	24.6	126.2	998 998	35 35	1.5 2.0	TS	21/00 21/00			1008 1008	_	0.5 1.0	TD TD
	12/12		137.1	996 996	35	1.5 2.0	TS		19/06	26.3	126.0	996	40	2.0	TS	21/1			1006	_	1.5	TD
	13/00		137.9	994	40	2.5	TS		19/12	27.6	125.9	996	40	2.0	TS	21/18			1002	35	2.0	TS
	13/06		138.7	990	45	3.0	TS		19/18	29.4	125.6	996	40	2.0	TS	22/0			1000	40	2.5	TS
	13/12		139.0	985	55	3.5	STS		20/00	31.0	125.8	998	40	2.0	TS	22/0	16.6	141.6	998	45	3.0	TS
	13/18	25.5	139.4	975	60	4.0	STS		20/06	32.6	125.4	998	35	2.0	TS	22/1:			990	55	3.5	STS
	14/00		140.3	975	60	4.0	STS		20/12		126.0	1002	35	2.0	TS	22/18			985	60	3.5	STS
	14/06			975	60	4.0	STS		20/18 21/00	36.6 37.7	125.4 126.1	1004 1006	35	_	TS TD	23/00			985	60 60	3.5 3.5	STS STS
	14/12			975	60	4.0	STS		21/06	39.0	127.9	1006	_	_	TD	23/0 23/1		141.4 141.4	985 985	60	3.5	STS
	14/18 15/00		141.3 141.2	975 970	60 65	4.0 4.0	STS TY		21/12		130.3	1006	_	-	TD	23/1			985	60	3.5	STS
	15/06	30.6	141.1	965	70	4.5	TY		21/18	42.3	132.1	1004	-	-	TD	24/0			980	65	3.5	TY
	15/09			955	80	-	TY		22/00	42.1	133.7	1002	-	-	L	24/0	21.7	141.0	980	65	4.0	TY
	15/12			950	85	5.5	TY		22/06	43.6	136.0	1000	-	-	L	24/13	22.3	140.8	980	65	4.0	TY
	15/15	32.0	140.8	950	85	-	TY		22/12	44.7	138.3	1000	-	-	L.	24/18			980	65	4.0	TY
	15/18	32.6	140.8	950	85	5.5	TY		22/18						Dissip.	25/0			980	65	4.0	TY
	15/21		140.9	950	85	-	TY									25/00 25/1			980	65 65	4.0	TY TY
	16/00		140.7	950	85	5.5	TY									25/12			980 980	65	4.0 4.0	TY
	16/03		140.8	950	85 95	- 5.5	TY									26/0		133.8	980	65	4.0	TY
	16/06 16/09			950 950	85 85	5.5 –	TY TY									26/0			980	65	4.0	TY
	16/12			950 950	85 85	5.5	TY										27.7		980	65	4.0	TY
	16/15	35.5	142.3	950	85	-	TY									26/1			975	70	-	TY
	16/18		142.9	950	85	5.5	TY									26/18			970	75	5.0	TY
	17/00	36.6	143.8	950	85	5.5	TY									26/2		131.0	960	80	-	TY
	17/06	37.3	145.6	955	70	5.0	TY									27/00 27/00			950 950	85 85	5.5 –	TY TY
	17/12			960	65	4.5	TY									27/0			950	85	5.5	TY
	17/18		150.1	965	60	4.0	STS									27/0			950	85	-	TY
	18/00			970	55	3.5	STS									27/1:			940	90	6.0	TY
	18/06 18/12			970 975	55 50	3.0 3.0	STS STS									27/1	28.8	130.3	935	95	-	TY
	18/18		160.7	975	50	2.5	STS									27/18			935	95	6.0	TY
	19/00			976	-	2.5	L									27/2			935	95	-	TY
	19/06	46.1	164.8	976	-	-	L									28/00		130.1	935	95	6.0	TY
	19/12	47.9	167.8	976	-	-	L									28/0: 28/0			935 935	95 95	6.0	TY TY
	19/18			972	-	-	L									28/0			935	95	-	TY
	20/00			964	-	-	L									28/1:			935	90	5.5	TY
	20/06		170.5	960	-	_	L									28/1		130.0	940	85	-	TY
	20/12 20/18		171.4 172.3	962 968	_	_	L L									28/18	31.3	130.0	945	85	5.0	TY
	21/00		174.8	968	_	_	L									28/2			955	75	-	TY
	21/06		178.1	972	_	_	Out									28/2			955	75	-	TY
																29/00 29/00			960 970	75 65	4.5	TY TY
																29/0			980	55	4.0	STS
Date	/Time	Center	Position	Central pressure	Max Wind	d CI num.	Grade									29/0			985	50	-	STS
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)											29/13			990	45	3.5	TS
		TS	WUK	ONG (2	408)											29/1	32.9	130.6	992	40	-	TS
Aug.	11/18	23.9	146.7	1002	-	0.0	TD									29/18			992	40	3.0	TS
	12/00		147.9	1004	-	0.5	TD									29/2			992	40	-	TS
	12/06		148.6	1004	-	1.0	TD									30/00			994	35	2.5	TS
	12/12			1006	_	1.0	TD										33.7 33.8	131.9 132.4	994 994	35 35	2.5	TS TS
	12/18 13/00			1004 1002	35	1.0 1.5	TS											133.6	996	-	2.5	TD
	13/06			1002	35	2.0	TS										33.6		996	_	2.5	TD
	13/12			1002	35	2.0	TS										33.3		996	-	2.5	TD
	13/18			1002	35	2.0	TS											135.9	996	-	2.0	TD
	14/00	29.2	149.2	1002	35	2.0	TS										32.9		996	-	2.0	TD
	14/06			1002	35	2.0	TS										33.1		998	-	2.0	TD
	14/12			1006	-	2.0	TD									Sep. 01/00		137.0 136.9	1002 1002	_	1.5	TD TD
	14/18			1006	-	1.5	TD											136.9	1002	_	1.5 -	TD
	15/00 15/06			1008 1008	_	1.5 1.5	TD TD									01/18		100.0	1000			Dissip.
	15/12			1008	_	1.5	TD									01/10						ooip.
	15/18			1008	_	_	TD															
	16/00			1008	-	-	TD															
	16/06			1008	-	-	TD															
	16/12		160.5	1006	-	-	L															
	16/18			1006	-	-	L															
	17/00			1004	-	-	L															
	17/06			1004	-	-	L															
	17/12 17/18			1004	_	_	L															
	18/00		175.0 176.4	1004 1004	_	_	L L															
	18/06			1004	_	_	L															
	18/12			1008	-	_	Ĺ															
	18/18		179.6	1008	-	-	Ĺ															
	19/00	39.5	179.8	1010	-	-	L															
	19/06	39.7	180.1	1010	-	-	Out															

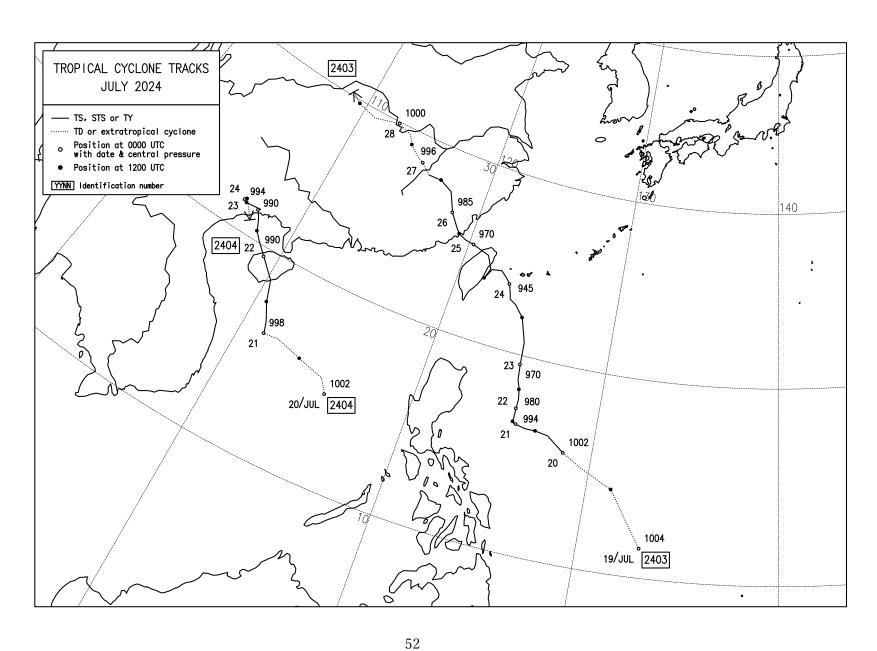
Date	/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade	Date/Tim	е	Center	Position	Central pressure	Max Wind	CI num.	Grade	Date	/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)			(UT	C)	Lat (N)	Lon (E)	(hPa)	(kt)				(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)		
			TY YA	GI (24	11)					TY	BEBI	NCA (2	2413)					T	s sou	LIK (2	415)		
Aug.	31/12			1004	-	1.5	TD	Sep. 09/		10.1		1002	-	0.5	TD	Sep.			126.0	998	-	0.0	TD
C	31/18 01/00	12.1 12.1	127.6	1004 1002	_	2.0	TD TD	10/		11.1	147.0	1002	_	1.0	TD		15/06	16.8	126.5	996	-	0.0	TD
Sep.	01/00	13.1	126.4 125.1	1002	35	2.0 2.0	TS	10/ 10/		11.9 12.8	146.3 145.4	1000 998	35	1.5 2.0	TD TS		15/12 15/18	16.9 17.3	126.0 125.6	998 996	_	0.5 1.0	TD TD
	01/12	14.0	124.4	1000	35	2.0	TS	10/		13.5	144.2	998	35	2.5	TS		16/00	17.2	125.1	998	_	1.5	TD
	01/18	14.5	123.2	996	40	2.5	TS	11/		13.9	143.2	996	40	2.5	TS		16/06	17.4	124.7	996	-	1.5	TD
	02/00	15.3	122.9	994	45	2.5	TS	11/	06	14.5	142.3	996	40	2.5	TS		16/12	17.5	123.3	996	-	2.0	TD
	02/06	16.2		994	45	2.5	TS	11/		15.1	141.6	996	40	2.5	TS		16/18	17.7	121.9	996	-	1.5	TD
	02/12 02/18	17.3 18.1	121.7 121.0	996 1000	40 35	2.5 2.0	TS TS	11/		16.4	140.8	996	40	2.5	TS		17/00	17.7	119.8	998	_	1.5	TD
	03/00	18.2	119.6	996	40	2.5	TS	12/ 12/		18.0 19.2	140.0 139.6	992 992	45 45	3.0 3.0	TS TS		17/06 17/12	17.2 17.3	119.6 118.6	996 996	_	1.5 1.5	TD TD
	03/06	18.5	119.0	992	45	2.5	TS	12/		20.4	138.6	992	45	3.0	TS		17/12	17.3	117.7	996	_	1.5	TD
	03/12	18.8	118.7	990	50	3.0	STS	12/		21.1	137.6	992	40	3.0	TS		18/00	17.5	115.5	996	_	1.5	TD
	03/18	18.9	118.3	980	60	3.5	STS	13/	00	22.1	136.9	994	40	3.0	TS		18/06	17.3	113.4	996	-	1.5	TD
	04/00	19.0	117.6	970	70	4.0	TY	13/		23.4	135.6	990	45	3.0	TS		18/12	17.3	111.3	996	-	1.5	TD
	04/06 04/12	19.2 19.2	117.4 117.0	955 940	80 90	5.0 5.5	TY TY	13/		24.7	133.7	990	45	3.0	TS		18/18	17.5	110.0	992	35	1.5	TS
	04/12	19.2		925	100	6.0	TY	13/ 14/		25.3 26.4	132.6 131.6	985 985	50 50	3.0 3.0	STS STS		19/00 19/06	17.5 17.0	108.3 107.3	992 992	35 35	2.0 2.0	TS TS
	05/00	19.0	115.8	915	105	6.5	TY	14/		26.9	130.8	980	55	-	STS		19/12	16.9	107.3	996	_	2.0	TD
	05/06	19.3	115.1	915	105	6.5	TY	14/		27.4	130.2	980	55	3.0	STS		19/18	16.9	106.5	998	_	2.0	TD
	05/12	19.3	114.2	915	105	6.5	TY	14/	09	27.8	129.5	980	55	-	STS		20/00	16.7	105.6	998	-	1.5	TD
	05/18	19.2	113.0	915	105	6.5	TY	14/		28.1	129.2	975	60	4.0	STS		20/06	17.1	104.6	1000	-	1.5	TD
	06/00 06/06	19.2 19.8	112.2 111.3	915 915	105 105	6.5 6.5	TY TY	14/		28.5	128.6	975	60	- 4 E	STS			17.1	103.9	1002	-	-	TD
	06/06	20.0	111.3	930	95	6.5 5.5	TY	14/ 15/		28.9 29.6	128.0 127.2	970 965	65 75	4.5 5.0	TY TY		20/18						Dissip.
	06/18	20.3	109.0	945	85	5.0	TY	15/		30.1	127.2	965	75 75	5.0	TY								
	07/00	20.5	108.1	940	85	5.0	TY	15/		30.1	124.8	965	75 75	5.0	TY	Date	/Time	Center	Position	Central	Max Wind	CI num.	Grade
	07/06	21.0	107.0	935	90	5.5	TY	15/		30.6	123.3	970	70	4.5	TY		(UTC)	Lat (N)		pressure (hPa)	(kt)		
	07/12	20.9	106.0	980	55	4.5	STS	16/	00	31.0	121.8	980	65	4.0	TY		(010)			RON (
	07/18 08/00	20.8	105.7 105.1	992 996	40 35	4.5 4.0	TS TS	16/		31.4	120.5	985	60	4.0	STS	Sep.	23/06		129.3	1008	,	0.5	TD
	08/06	21.3	104.9	996	35	3.5	TS	16/ 16/		31.7 31.9	119.3 118.0	992 1000	50 35	3.5 3.0	STS TS		23/12	28.7	131.3	1006	_	1.0	TD
	08/12	21.5	104.2	998	-	3.0	TD	17/		32.4	117.2	1004	-	2.5	TD		23/18	28.3	132.8	1004	-	1.5	TD
	08/18	22.1	103.5	1000	-	3.0	TD	17/		32.9	116.4	1004	_	2.0	TD		24/00	27.9	133.6	1002	-	1.5	TD
	09/00	22.4	103.0	1000	-	2.5	TD	17/	12	33.1	116.1	1006	-	-	TD		24/06	27.8	134.2	1000	35	1.5	TS
	09/06	22.0	101.4	1000	-	2.0	TD	17/		33.3	115.6	1008	-	-	TD		24/12	27.9 28.0	135.1 135.4	998 998	35 35	2.0 1.5	TS TS
	09/12 09/18	21./	100.7	1000	-	2.0	TD Dissip.	18/		33.5	115.3	1008	-	-	TD		24/18 25/00	28.4	134.9	998	35	1.5	TS
	09/10						Dissip.	18/		33.8	115.1	1008	-	-	TD		25/06	28.2	133.9	998	35	1.5	TS
								18/	12						Dissip.		25/12	27.8	133.3	998	35	1.5	TS
Date	/Time	Cente	r Position	Centra	l	d CInum	Grade										25/18	28.0	132.9	998	35	1.5	TS
				preceur		u Oi nun	i. Grade																
	(UTC)) Lon (E	pressur		u Cinun	i. Grade	Date/Tim	e	Center	Position	Central	Max Wind	d CI num	n. Grade		26/00	28.2	132.4	998	35	2.0	TS
		Lat (N) Lon (E	pressur	e (kt)	d Ginun				Center		Central pressure (hPa)	Max Wind	d CI num	n. Grade		26/00 26/06	28.2 28.0	132.0	1002		2.0 2.0	TD
		Lat (N) Lon (E	pressur (hPa)	e (kt) 412)	0.0	TD			Lat (N)	Lon (E)	pressure (hPa)	(kt)	d CI num	ı. Grade		26/00 26/06 26/12	28.2 28.0 28.1	132.0 131.9	1002 1004		2.0 2.0 2.0	TD TD
	(UTC)	Lat (N	Lon (E TS LE 147.1	pressur (hPa) EPI (2- 1012	(kt) 412)				C)	Lat (N)	Lon (E)	pressure	(kt)	d CI num	n. Grade		26/00 26/06	28.2 28.0	132.0	1002	35 - -	2.0 2.0	TD
	(UTC)	Lat (N	Lon (E TS LE 147.1 146.8	pressur (hPa) EPI (2- 1012	(kt) 412) 2 - 0 -	0.0	TD	Sep. 15	C)	Lat (N)	Lon (E)	pressure (hPa)	(kt) 2414)				26/00 26/06 26/12 26/18	28.2 28.0 28.1 28.5	132.0 131.9 132.2	1002 1004 1004	35 - - -	2.0 2.0 2.0 2.0	TD TD TD
	01/12 01/18 02/00 02/06	22.2 22.6 22.9 23.6	Den (E 147.1 146.8 146.6 146.5	pressur (hPa) EPI (2- 1012 1010 1012	(kt) 412) 2 - 0 - 2 - 0 -	0.0 0.5 0.5 0.5	TD TD TD TD	Sep. 15,	(00 (06 (12	TS 12.1 12.3 12.8	PULA 144.6 144.3 144.3	pressure (hPa) SAN (1002 1000 1000	(kt) 2414) 35		TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12	28.2 28.0 28.1 28.5 28.6 28.8 29.5	132.0 131.9 132.2 132.2 132.7 133.4	1002 1004 1004 1004 1004 1006	35 - - - -	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD TD
	01/12 01/18 02/00 02/06 02/12	22.2 22.6 22.9 23.6 24.0	Lon (E 147.1 146.8 146.6 146.5 146.8	pressur (hPa) 1012 1010 1012 1010 1012	(kt) 412) 2 - 0 - 2 - 0 - 2 - 0 - 0 - 0 -	0.0 0.5 0.5 0.5 0.5	TD TD TD TD	Sep. 15, 15, 15, 15,	(00 (06 (12 (18	TS 12.1 12.3 12.8 13.9	PULA 144.6 144.3 144.3 144.2	1002 1000 1000 998	(kt) 2414) 35 35	- - 0.0 0.5	TD TD TS TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0	132.0 131.9 132.2 132.2 132.7 133.4 133.5	1002 1004 1004 1004 1004 1006 1008	35 - - - - - -	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD TD TD TD
	01/12 01/18 02/00 02/06 02/12 02/18	22.2 22.6 22.9 23.6 24.0 24.6	147.1 146.8 146.6 146.8 146.8 146.8	pressur (hPa) (2- 1012 1010 1012 1010 1012	(kt) 412) 2 - 0 - 2 - 0 - 2 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0	0.0 0.5 0.5 0.5 0.5	TD TD TD TD TD TD TD	Sep. 15, 15, 15, 15, 16,	(00 (06 (12 (18	TS 12.1 12.3 12.8 13.9 15.8	PULA 144.6 144.3 144.3 144.2 143.7	1002 1000 1000 1000 998 998	(kt) 2414) - 35 35 35	- 0.0 0.5 1.0	TD TD TS TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0	1002 1004 1004 1004 1004 1006 1008	35 - - - -	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD TD TD L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00	22.2 22.6 22.9 23.6 24.0 24.6 24.8	147.1 146.8 146.5 146.8 146.5 146.8 147.3	Pressur (hPa) (hPa) 1012 1010 1012 1010 1010 1010	(kt) 412) 2 - 0 - 2 - 0 - 2 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0	0.0 0.5 0.5 0.5 0.5 0.5	TD TD TD TD TD TD TD TD	Sep. 15, 15, 15, 15, 16,	(00 (06 (12 (18 (00 (06	TS 12.1 12.3 12.8 13.9 15.8 16.1	PULA 144.6 144.3 144.3 144.2 143.7 142.0	1002 1000 1000 1000 998 998 998	(kt) 2414) 35 35 35 35	- 0.0 0.5 1.0	TD TD TS TS TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2	1002 1004 1004 1004 1006 1008 1010	35 - - - - - -	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD TD L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06	22.2 22.6 22.9 23.6 24.0 24.8 25.0	147.1 146.8 146.6 146.5 146.8 147.3 147.3	1012 1012 1012 1010 1012 1010 1010 1010	(kt) 412) 2 - 0 - 2 - 0 - 2 - 0 - 2 - 0 - 3 -	0.0 0.5 0.5 0.5 0.5 0.5 0.5	TD TD TD TD TD TD TD TD TD	Sep. 15, 15, 15, 15, 16, 16,	(00 (06 (12 (18 (00 (06 (12	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4	PULA 144.6 144.3 144.3 144.2 143.7 142.0 140.8	(hPa) (SAN (1002 1000 1000 998 998 998 996	(kt) 2414) 35 35 35 35 40	- 0.0 0.5 1.0 1.5	TD TD TS TS TS TS TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0	1002 1004 1004 1004 1004 1006 1008	35 - - - - - -	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD TD TD L
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	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12	22.2 22.6 22.9 23.6 24.0 24.6 24.8 25.0 25.7	147.1 146.8 146.6 146.5 146.8 147.3 147.1 147.6 147.1	pressur (hPa) (hPa) (2012 1010 1012 1010 1010 1010 1008 1008	(kt) 412) 2 - 0 - 2 - 0 - 2 - 0 - 2 - 0 - 3 - 3 - 3 -	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5	TD	Sep. 15, 15, 15, 16, 16, 16, 16, 17,	(00 (06 (12 (18 (00 (06 (12 (18	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7	PULA 144.6 144.3 144.3 144.2 143.7 142.0 140.8 140.1	1002 1000 1000 1000 998 998 998 996	(kt) 2414) 35 35 35 35 40 40	- 0.0 0.5 1.0 1.5 1.5	TD TD TS TS TS TS TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012	35 - - - - - -	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18	22.2 22.6 22.9 23.6 24.0 24.6 25.0 25.7 26.6	147.1 146.8 146.6 146.5 146.8 147.3 147.3 147.1 147.6 147.1	pressur (hPa) (hPa) EPI (2: 1012 1010 1012 1010 1010 1008 1008	(kt) 412) 2 - 0 - 2 - 0 - 2 - 0 - 2 - 0 - 3 - 3 - 3 - 6 - 6 -	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	TD T	Sep. 15, 15, 15, 15, 16, 16, 16, 17, 17,	(00 (06 (12 (18 (00 (06 (12 (18 (00	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0	PULA 144.6 144.3 144.3 144.2 143.7 142.0 140.8 140.1 140.1	\$\frac{(hPa)}{sAN (} 1002 1000 1000 998 998 996 996 992	(kt) 2414)	- 0.0 0.5 1.0 1.5 1.5 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/06 28/12 28/18 29/00 29/06 29/12	28.2 28.0 28.1 28.5 28.6 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014	35 - - - - - -	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/00 04/06	22.2 22.6 22.9 23.6 24.0 24.6 25.0 25.7 26.6 27.8 29.2 30.2	146.8 146.5 146.5 146.5 146.5 146.3 147.3 147.1 147.6 147.1 147.0 146.9	pressur (hPa) (hPa) EPI (2: 1012 1010 1012 1010 1010 1008 1008 1008 1008	(kt) (kt) 412) 2 2 2 2 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3 3 3 3 3 3 3 3 3 3 3 - 3	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.0 0.5 1.0 1.5	TD T	(UT Sep. 15, 15, 15, 16, 16, 16, 17, 17,	(00 (06 (12 (18 (00 (12 (18 (12 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6	Lon (E) PULA 144.6 144.3 144.2 143.7 142.0 140.8 140.1 140.1 137.4 134.5 133.7	Pressure (hPa) SAN (1002 1000 1000 998 998 998 996 996 992 992 992	(kt) 2414) - 35 35 35 35 40 40 45 45 45 45	- 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.7 32.7 32.7 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD TL L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/00 04/06 04/12 04/18	22.2 22.6 22.9 23.6 24.0 24.6 25.0 25.7 26.6 27.8 29.2 30.2 31.3	147.1 146.8 146.6 146.5 146.8 147.3 147.1 147.6 147.1 147.0 146.9	Pressur (hPa) (hPa) EPI (2- 1012 1010 1012 1010 1010 1008 1008 1006 1004	(kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.0 0.5 1.0 1.5 1.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 17, 17, 17, 17, 18,	(00 (06 (12 (18 (00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (10 (18 (00 (10 (18 (00 (10 (18 (10 (10 (10 (10 (10 (10 (10 (10 (10 (10	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 23.4	Lon (E) PULA 144.6 144.3 144.2 143.7 142.0 140.8 140.1 140.1 137.4 134.5 133.7 131.9	Pressure (hPa) SAN (1002 1000 1000 998 998 998 996 996 992 992 992	(kt) 2414) - 35 35 35 35 40 40 45 45 45 45	- 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/00 04/06 04/12 04/18 05/00	22.2 22.6 22.9 23.6 24.0 24.6 25.0 25.7 26.6 27.8 29.2 30.2 31.3 32.2	146.6 147.1 146.6 146.5 146.8 147.3 147.1 147.6 147.1 147.0 146.9 147.2 146.2	Pressur (hPa) (hPa) EPI (2 1012 1010 1012 1010 1010 1008 1008 100	(kt) (kt) (412) (2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	0.0 0.5 0.5 0.5 0.5 0.5 0.0 0.5 1.0 1.5 1.5 2.0	TD T	Sep. 15. 15. 15. 16. 16. 16. 17. 17. 17.	(00) (06) (12) (18) (00) (06) (12) (18) (00) (12) (18) (00) (06) (12) (18) (00) (06) (19) (19) (19) (19) (19) (19) (19) (19	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 23.4 24.5	PULA 144.6 144.3 144.3 144.2 143.7 142.0 140.8 140.1 140.1 137.4 134.5 133.7 131.9 130.6	Pressure (hPa) SAN (1002 1000 1000 998 998 998 996 996 992 992 992 992 992	(kt) 2414) - 35 35 35 35 40 40 45 45 45 45 45	- 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/00 04/12 04/18 05/00	22.2 22.6 22.9 23.6 24.0 24.8 25.0 25.7 26.6 27.8 29.2 30.2 31.3 32.2 33.2	D Lon (E TS LE 147.1 146.8 146.5 146.8 147.3 147.1 147.6 147.1 147.0 146.2 145.9 145.9	pressur (hPa) EPI (22 1012 1010 1012 1010 1012 1010 1006 1006 1006 1004 1004 1004 1006 1006	(kt) (412) (412) (0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.0 0.5 1.0 1.5 1.5 1.5 2.0	TD T	Sep. 15, 15, 15, 16, 16, 16, 17, 17, 17, 18, 18, 18, 18,	(00) (06) (12) (18) (00) (06) (12) (18) (00) (06) (12) (18) (00) (06) (12) (13)	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1	PULA 144.6 144.3 144.3 144.2 143.7 142.0 140.8 140.1 140.1 137.4 134.5 133.7 131.9 130.6	Pressure (hPa) SAN (1002 1000 1000 998 998 998 996 996 992 992 992	(kt) 2414) - 35 35 35 35 40 40 45 45 45 45	- 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/00 04/06 04/12 04/18 05/00	22.2.2.6.6.2.9.2.4.6.2.5.0.2.5.7.2.6.6.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.3.2.2.2.3.2	146.6 147.1 146.6 146.5 146.8 147.3 147.1 147.6 147.1 147.0 146.9 147.2 146.2	Pressur (hPa) EPI (22 1012 1010 1012 1010 1012 1010 1008	(kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.0 0.5 1.0 1.5 1.5 2.0	TD T	Sep. 15, 15, 15, 16, 16, 16, 17, 17, 17, 18, 18, 18, 18,	(00) (06) (12) (18) (00) (06) (12) (18) (00) (06) (12) (18) (00) (06) (12) (13)	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1	PULA 144.6 144.3 144.2 143.7 142.0 140.1 140.1 137.4 134.5 133.7 131.9 128.8 127.2	Pressure (hPa) SAN (1002 1000 1000 998 998 998 996 996 992 992 992 992 992 992	(kt) 2414) - 35 35 35 35 40 40 45 45 45 45 45 45	- 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/00 04/16 04/12 04/18 05/00 05/06	22.2 22.6 22.9 23.6 24.0 24.6 25.0 25.7 25.7 29.2 30.2 31.3 32.2 33.9 34.9 35.8	TS LE 147.1 146.8 146.6 146.5 147.3 147.3 147.1 147.6 147.2 146.2 145.9 145.8 145.9 146.9 148.2	Pressur (hPa) (hPa) 1012 1016 1012 1016 1016 1016 1006 1	(kt) 412) 2 2	0.0 0.5 0.5 0.5 0.5 0.5 0.0 0.5 1.0 1.5 1.5 2.0 2.0	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 18, 18, 18, 19, 19,	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	TS 12.1 12.3 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 24.5 26.1 27.3 30.1	PULA 144.6 144.3 144.3 144.2 143.7 142.0 140.8 140.1 137.4 131.9 130.6 128.8 127.2 125.6 123.5	pressure (hPa) SAN (1002 1000 1000 998 998 996 996 992 992 992 992 992 992 992 992	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 40 40 40 40	- 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/12 03/18 04/00 04/12 04/18 05/00 05/06 05/12 05/18 06/00 06/06	22.2 22.6 22.9 23.6 24.0 24.6 25.0 25.7 25.7 30.2 31.3 32.2 33.9 34.9 35.8 36.9	TS LE 147.1 146.8 146.6 146.5 147.3 147.3 147.1 147.0 146.9 147.2 146.9 148.9 148.9 148.9 148.9	Pressur (hPa) EPI (2: 1012 1010 1012 1010 1010 1010 1006 1006 1006 1004 1002 1002 1004	(kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.5 2.5 2.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 17, 17, 17, 18, 18, 18, 19, 19, 19, 19, 19,	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (12 (12 (12 (12 (12 (12 (12 (12 (12	TS 12.1 12.3 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1 27.3 30.1 30.7	PULA 144.6 144.3 144.2 143.7 142.0 140.8 140.1 140.1 137.4 134.5 133.7 131.9 130.6 128.8 127.2 125.6 123.5 122.0	Pressure (hPa) SAN (1002 1000 1000 998 998 996 996 992 992 992 992 992 992 998 998 1000	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 40 40 40 35	- 0.0 0.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/06 04/12 04/12 05/06 05/06 05/12 05/18 06/00 06/06 06/06	22.2.2.6.6.6.27.8.29.2.33.2.233.2.233.2.33.9.33.9.35.8.36.9.37.8	147.1.1 146.8.4 146.6.4 146.5.4 146.5.4 147.3.1 147.3.1 147.1 147.0.1 146.9.9 145.9 145.9 145.9 145.9 145.9 149.7 151.1	Pressur (hPa) (hPa) 1012 1010 1012 1010 1010 1010 1006 1	(kt) (412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 1.0 1.5 1.5 2.0 2.5 2.5 2.5 2.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19.	(000 (066 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (18 (18 (000 (18 (18 (18 (18 (18 (18 (18 (18 (18 (18	TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 22.6 23.4 24.5 26.1 27.3 30.1 30.7 31.3	PULA 144.6 144.3 144.3 144.2 143.7 142.0 140.8 140.1 137.4 134.5 133.7 131.9 130.6 128.8 127.2 125.6 123.5 122.0 120.9	pressure (hPa) SAN (1002 1000 1000 998 998 996 996 992 992 992 992 992 992 992 992	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 45 45 45 40 40 40 40 40 35 35	- - 0.0 0.5 1.0 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 03/18 04/00 04/12 04/18 05/00 05/12 05/18 06/06 06/12	22.2.2.6.6.6.27.8.29.2.33.9.33.9.35.88.39.0.29.37.8.39.0.29.27.27.27.27.27.27.27.27.27.27.27.27.27.	TS LE 147.1.1 146.8 146.8 147.1.1 146.8 146.8 147.3 146.8 147.3 147.3 147.3 147.3 147.3 147.3 147.3 146.9 148.2 149.7 146.9 148.2 149.7 153.1 153.1 153.1	Pressur Pressu	(kt) (412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 18, 18, 18, 19, 19, 19, 20, 20,	(000 (066 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (12 (18 (000 (18 (18 (000 (18 (18 (18 (18 (18 (18 (18 (18 (18 (18	Lat (N) TS 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1 27.3 30.1 30.1 31.3 31.8	PULA 144.6 144.3 144.3 144.3 144.2 143.7 142.0 140.8 140.1 137.4 134.5 133.7 131.9 130.6 128.8 127.2 125.6 123.5 122.0 120.9 120.4	pressure (hPa) SAN (1002 1000 1000 998 998 996 996 992 992 992 992 992 992 992 991 992 992	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 45 45 45 35 35 35 35 35		TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/06 02/12 02/18 03/10 03/06 03/12 04/06 04/12 04/8 05/00 05/06 06/06 06/18 07/00	22.22.6. 22.9. 23.6. 24.0. 24.6. 24.8. 25.0. 25.7. 26.6. 30.2. 31.3. 32.2. 33.9. 34.9. 35.8. 36.9. 37.8. 39.0. 40.6.	TS LE 147.1.1 146.8 147.1.1 146.8 147.1 146.8 147.3 147.3 147.3 147.3 147.1 147.0 147.1 147.0 146.9 145.9 145.9 145.9 145.9 145.9 155.1 155.6 15	pressure (hep-a) (20 pressure	(kt) (kt) (412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 18, 18, 18, 19, 19, 19, 20, 20, 20,	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (14 (18 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	Lat (N) TS 12.1 12.3 12.8 13.9 15.8 16.1 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1 27.3 28.3 30.1 30.7 30.7 31.3 31.8 32.0	PULA 144.6 144.3 144.3 144.3 144.3 142.0 140.8 140.1 137.4 134.5 131.9 130.6 128.8 127.6 122.0 120.9 120.9 120.4	pressure (hPa) (hP	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 45 40 40 40 35 35 35 35		TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/00 03/00 04/02 04/18 05/00 05/18 06/00 06/12 06/18 07/00	22.2.2.6.6.6.24.0.25.7.26.6.6.27.8.33.2.2.33.2.2.33.2.33.2.33.2.2.33.2.4.9.4.0.6.42.3.39.0.0.42.3	146.8 Len (E46.8 Len (Pressure	(kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 18, 18, 18, 19, 19, 19, 200, 20, 20, 20, 20,	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (14 (18 (00 (14 (18 (00 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	T\$ 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 22.6 23.4 24.5 26.1 27.3 28.3 30.1 30.7 31.3 32.0 32.7	PULA 144.6 144.3 144.2 143.7 142.0 140.1 140.1 137.4 130.9 130.9 120.8 122.0 120.9 120.4 120.4 121.2	pressure (hPa) SAN (1002 1000 1000 998 998 996 992 992 992 992 992 996 998 998 998 1000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 45 45 45 35 35 35 35 35		TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/13 02/00 02/06 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/01 06/06 06/01 06/06 07/00 07/06 07/06	22.2.2.6. 22.9.2.6. 24.0. 24.0. 24.6. 25.0. 25.7. 29.2. 30.2. 33.2. 33.9. 34.9. 37.8. 39.0. 40.6. 42.3. 44.1.	TS LE	Pressure	(kt) (kt) (kt) (kt) (kt) (kt) (kt) (kt)	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.0 0.5 1.5 1.5 1.5 2.0 2.0 2.5 2.5 2.5 2.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 20.	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (14 (18 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	T\$ 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 22.6 23.4 24.5 26.1 30.7 31.3 31.8 32.7 33.2 32.7 33.2	PULA 144.6 144.3 144.3 144.3 144.3 142.0 140.8 140.1 137.4 134.5 131.9 130.6 128.8 127.6 122.0 120.9 120.9 120.4	pressure (hPa) (hP	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 40 40 40 40 40 40 35 35 35 35		TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/00 03/00 04/02 04/18 05/00 05/18 06/00 06/12 06/18 07/00 07/06	22.2 (2.9. (146.8 Len (E46.8 Len (pressure	(kt) (kt) (412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 17, 18, 18, 18, 19, 19, 19, 20, 20, 20, 20, 21, 21, 21	(00) (00) (06) (12) (18) (00) (12) (18) (00) (12) (18) (00) (12) (18) (00) (12) (18) (00) (12) (18) (10) (10) (11) (11) (11) (11) (11) (11	T\$ 12.1 12.3 12.8 13.9 15.8 16.1 16.4 17.7 20.0 21.2 22.6 23.4 24.5 26.1 30.7 31.3 31.8 32.7 33.2 32.7 33.2	PULA 144.6 144.3 144.2 143.7 142.0 140.1 140.1 134.5 133.7 131.9 122.0 122.0 120.4 121.2 122.3 122.3	Pressure (hPa) SAN (1002 1000 1000 998 998 996 992 992 992 992 992 992 991 1000 1000 1	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 40 40 40 40 35 35 35 35 35 35		TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/06 02/12 02/18 03/00 03/06 03/12 04/06 04/12 05/06 05/18 06/00 06/06 06/06 07/00 07/06 07/12	22.2 22.6 22.9 23.6 24.0 24.6 25.7 26.6 27.8 29.2 31.3 32.2 33.2 34.9 35.8 36.9 37.8 40.6 42.3 44.1 44.5 47.7	TS LEE 147.1.1 Lon (E	pressure	(kt) (kt) (412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.0 0.5 1.5 1.5 2.0 2.5 2.5 2.5 2.5 2.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 20. 21. 21.	(00 (06 (12 (18 (00 (12 (18 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	TS 12.1 12.3 12.8 16.1 16.4 16.1 16.1 16.1 16.1 16.1 16.1	PULA 144.6 144.3 144.2 143.7 144.0 140.8 140.1 137.4 133.7 133.7 133.6 128.8 123.5 122.0 120.4 1	pressure (hPa) SAN (1002 1000 1000 998 996 992 992 992 992 992 996 998 998 1000 1000 1000 1000 1000 1000 1	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 01/18 02/00 02/00 02/06 02/12 02/18 03/10 03/06 03/12 04/06 04/12 05/00 05/06 05/12 06/06 06/18 07/00 07/16 08/00	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.0 0.5 1.5 1.5 2.0 2.5 2.5 2.5 2.5 2.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 20. 21. 21. 21.	(00) (06) (12) (18) (00) (06) (12) (18) (00) (06) (12) (18) (00) (06) (12) (18) (00) (06) (12) (18) (00) (12) (18) (00) (12) (18) (18) (18) (18) (18) (18) (18) (18	TS 12.1 12.3 12.8 16.1 12.3 12.8 16.1 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1 27.3 30.1 33.8 32.0 33.6 33.9 33.6 33.9 36.0 36.0	PULA 144.6 144.3 144.2 143.7 144.2 140.1 140.1 134.5 133.7 133.6 128.8 127.2 122.0 120.4 121.2 122.3 123.7 125.3 1	pressure (hPa) (hP	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 45 40 40 40 35 35 35 35 35 40 40 40 -	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/06 02/12 03/06 03/12 04/00 04/06 05/06 05/06 06/06 06/12 06/06 07/12 07/18	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LE LE 147.1.146.8.2 Len (E47.1.146.8.2 Len (E47.1.146.8.2 Len (E47.1.147.1.147.0.146.9.2 Len (E47.1.147.1.147.0.147	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.0 0.5 1.5 1.5 2.0 2.5 2.5 2.5 2.5 2.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 18, 18, 18, 19, 19, 20, 20, 20, 20, 21, 21, 21, 21, 22,	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (14 (18 (00 (14 (18 (00 (14 (18 (00 (14 (18 (00 (14 (18 (00 (14 (18 (00 (14 (18 (00 (14 (18 (00 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	TS 12.1 12.3 12.8 12.8 16.1 16.4 16.4 17.7 20.0 21.2 21.7 22.3 28.3 30.1 31.8 32.0 32.7 33.3 31.8 32.0 33.9 33.6 33.9 34.2 33.6 37.4	PULA 144.6 144.3 144.2 143.7 142.0 140.8 140.1 134.5 133.7 131.9 132.0 122.0 120.9 120.4 121.2 122.3 122.0 120.4 121.2 122.3 122.3 122.3 122.4 122.3 123.7 125.3 127.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1	pressure (hPa) (hP	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 20. 21. 21. 21. 22.	(00 (06 (12 (18 (00 (14 (18 (00 (14 (18 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	TS 12.1 12.3 13.9 15.8 16.1 17.7 20.0 21.2 21.7 22.6 23.4 30.1 30.7 31.3 32.7 33.2 33.9 34.2 36.0 38.8	Lon (E) PULA 144.6 144.3 144.2 143.7 142.0 140.8 140.1 137.4 134.5 133.7 132.6 122.0 120.9 120.4 120.4 120.4 120.4 120.3 122.3 123.7 124.6 125.6 126.6 127.7 132.6 128.8 127.7 132.6 128.8 127.7 132.6 128.8 128.7 129.9 120.4	Pressure (hPa) SAN (1002 1000 1000 998 998 996 992 992 992 992 996 998 1000 1000 1000 1000 1000 1000 1000	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 20. 21. 21. 21. 22. 22.	(00 (06 (12 (18 (00 (12 (18 (18 (18 (18 (18 (18 (18 (18 (18 (18	Lat (N) 12.1 12.3 13.9 15.8 16.1 16.4 17.7 20.0 21.7 22.6 24.5 26.1 27.3 30.1 30.7 31.8 32.0 33.6 33.9 33.9 33.9 33.9 33.9 33.9 33.9	PULA 144.6 144.3 144.2 143.7 144.0 140.8 140.1 134.5 133.7 133.6 128.8 122.6 123.5 122.0 120.4 120.4 120.4 120.3 121.2 122.3 123.7 125.3 125.3 125.3 125.3 125.3 126.3 127.3 128.8 129.3 1	pressure (hPa) (hPa) (SAN (1002) 1000 1000 998 998 998 996 996 992 992 992 992 996 998 998 1000 1000 1000 1000 1000 1000 1	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 17, 18, 18, 18, 19, 19, 20, 20, 20, 20, 21, 21, 21, 21, 22, 22, 22, 22, 22, 22	(00 (06 (12 (18 (00 (14 (18 (00 (14 (18 (18 (14 (18 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	TS 12.1 12.3 13.9 15.8 16.1 16.4 17.7 20.0 23.4 52.6 1.3 27.3 33.6 33.9 33.6 33.9 37.4 38.8 39.9 7	PULA 144.6 144.3 144.2 143.7 142.0 140.1 134.5 133.7 131.9 122.0 122.0 122.0 122.0 122.0 122.3 122.3 122.3 122.3 122.3 122.3 122.3 123.5 124.3 125.3 127.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1	Pressure (hPa) SAN (1002 1000 1000 998 998 996 992 992 992 992 996 998 1000 1000 1000 1000 1000 1000 1000	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15, 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 17, 18, 18, 18, 19, 19, 19, 20, 20, 20, 21, 21, 21, 21, 22, 22, 22, 22, 23, 23,	(00 (06 (12 (18 (00 (12 (18 (18 (18 (18 (18 (18 (18 (18 (18 (18	Lat (N) TS 12.1 12.3 13.9 15.8 16.1 16.1 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1 27.3 30.7 31.3 31.3 32.0 32.7 33.2 33.9 34.2 33.9 34.2 38.8 39.0 39.7 40.0	PULA 144.6 144.3 144.2 143.7 144.0 140.8 140.1 134.5 133.7 133.6 128.8 122.6 123.5 122.0 120.4 120.4 120.4 120.3 121.2 122.3 123.7 125.3 125.3 125.3 125.3 125.3 126.3 127.3 128.8 129.3 1	Pressure (hPa)	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 21. 21. 21. 22. 22. 22. 22. 22.	(00 (06 (12 (18 (18 (18 (18 (18 (18 (18 (18 (18 (18	Lat (N) TS 12.1 12.3 13.9 15.8 16.1 16.1 17.7 20.0 21.2 21.7 22.6 23.4 24.5 26.1 27.3 30.7 31.3 31.3 32.0 32.7 33.2 33.9 34.2 33.9 34.2 38.8 39.0 39.7 40.0	PULA 144.6 144.3 144.2 143.7 144.0 140.1 140.1 137.4 137.4 137.4 138.8 122.6 123.5 122.0 120.4 120.4 120.4 120.4 120.4 120.3 121.7 121.7 132.6 133.7 121.7 121.7 122.3 123.7 124.7 125.6 126.7 126.7 127.7 132.6 149.7 1	Pressure (hPa)	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 17, 17, 17, 17, 18, 18, 18, 19, 19, 19, 20, 20, 20, 20, 21, 21, 21, 21, 22, 22, 22, 23, 23, 23, 23, 23, 23, 23	(00) (00) (06) (12) (18) (00) (12) (18) (00) (12) (18) (00) (12) (18) (00) (12) (18) (00) (12) (18) (00) (12) (18) (10) (12) (18) (18) (18) (18) (18) (18) (18) (18	Lat (N) TS 12.1 12.3 13.9 15.8 16.1 16.4 17.7 20.0 21.2 21.7 22.6 23.4 23.4 27.3 28.1 30.7 31.3 30.1 30.7 31.3 33.6 33.9 34.2 33.6 33.9 34.2 33.6 37.4 38.8 39.7 40.0 41.2 43.6	PULA 144.6 144.3 144.2 143.7 142.0 140.1 134.5 133.7 131.9 132.5 122.0 120.9 120.4 121.2 122.3 123.7 125.3 127.7 125.3 127.7 125.3 127.7 125.3 127.7 125.3 127.7 125.4 136.5 1	Pressure (hPa) (hP	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 40 40 40 40 40 40 40 40 40 40 40 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 21. 21. 21. 21. 22. 22. 22. 22. 22. 23. 23. 23. 23.	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (12 (18 (00 (14 (18 (00 (14 (18 (00 (14 (14 (14 (14 (14 (14 (14 (14 (14 (14	Lat (N) 12.1 12.3 13.9 15.8 16.1 16.4 17.7 22.6 22.1.7 22.6 24.5 26.1 24.5 26.3 30.1 31.8 32.0 33.6 33.9 34.2 33.6 34.2 35.6 40.0 41.2 42.6 44.5	PULA 144.3 144.3 144.2 140.8 140.1 137.4 133.7 133.7 133.7 128.8 123.5 122.6 122.5 122.5 122.0 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.5 1	Pressure (hPa) SAN (1002 10000 10000 998 996 992 992 992 992 992 992 992 992 992	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 40 40 40 35 35 35 35 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (A) 22.2 (A) 22.6 (A) 22.2 (A) 22.6 (A) 24.6 (A) 25.7 (A	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15. 15. 15. 16. 16. 16. 16. 17. 17. 17. 18. 18. 18. 19. 19. 20. 20. 20. 21. 21. 21. 22. 22. 22. 22. 22. 23. 23. 23. 24.	(00 (06 (12 (18 (00 (12 (18 (00 (12 (18 (18 (19 (18 (18 (19 (18 (18 (19 (18 (18 (18 (18 (18 (18 (18 (18 (18 (18	Lat (N) 12.1 12.3 13.9 15.8 13.9 15.8 16.1 16.4 17.7 20.0 21.7 22.6 24.5 26.1 27.3 30.1 30.7 31.8 32.0 33.6 33.9 33.6 33.9 34.7 33.2 36.0 37.4 40.0 44.6 45.0	PULA 144.6 144.3 144.2 143.7 144.0 140.1 140.1 134.5 133.7 133.6 128.8 127.2 122.0 120.4 121.2 122.3 122.3 122.4 121.2 122.3 123.7 125.3 125.3 125.3 125.3 125.3 126.4 126.5 127.5 138.6 146.5 1	pressure (hPa) (hP	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 40 40 40 35 35 35 35 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L
	01/12 01/12 01/18 02/00 02/00 02/02 02/12 02/18 03/00 03/06 03/12 04/00 04/12 05/00 05/06 06/06 06/06 06/06 07/06 07/06 07/07/12 07/18 08/00 08/06 08/06	22.2 22.6 (Aug. 22.2 22.6 (Aug. 22.2 22.6 (Aug. 22.2 22.9 22.6 (Aug. 22.2 22.9 22.2 23.6 (Aug. 22.2 23.2 22.2 23.2 23.2 23.3 22.2 23.3 23.2 23.3 22.2 23.3 22.2 23.3 22.2 23.2 2	TS LEN (146.5) Lon (EC) 147.1.146.8.146.5.146.8.147.1.147.6.146.9.147.1.147.6.146.9.147.1.147.6.145.9.	Pressure (hea) (he	(kt) (kt) (kt) 412) 2	0.0 0.5 0.5 0.5 0.5 0.5 0.5 0.5 1.5 1.5 1.5 1.5 1.5 1.5 2.0 2.5 2.5 2.5 2.0 1.5	TD T	Sep. 15, 15, 15, 16, 16, 16, 16, 16, 17, 17, 17, 17, 18, 18, 18, 19, 19, 20, 20, 20, 20, 20, 21, 21, 21, 21, 22, 22, 22, 22, 23, 23, 24, 24, 24, 24, 24, 24, 24, 24, 24, 24	(00 (06 (12 (18 (00 (12 (18 (18 (12 (18 (18 (18 (18 (18 (18 (18 (18 (18 (18	TS 12.1 12.3 13.9 15.8 16.1 16.4 17.7 20.0 23.4 52.6 1.2 21.7 22.6 23.4 5.2 26.1 27.3 28.5 26.1 30.7 31.8 32.0 32.7 7 31.8 32.0 32.7 7 40.0 41.2 43.6 44.5 44.5 44.5 46.1	PULA 144.3 144.3 144.2 140.8 140.1 137.4 133.7 133.7 133.7 128.8 123.5 122.6 122.5 122.5 122.0 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.4 120.5 1	Pressure (hPa) SAN (1002 10000 10000 998 996 992 992 992 992 992 992 992 992 992	(kt) 2414) 35 35 35 35 40 40 45 45 45 45 45 40 40 40 35 35 35 35 40 40	0.0 0.5 1.0 1.5 1.5 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	TD TD TS		26/00 26/06 26/12 26/18 27/00 27/06 27/12 27/18 28/00 28/06 28/12 28/18 29/00 29/06 29/12 29/18 30/00 30/06	28.2 28.0 28.1 28.5 28.6 28.8 29.5 31.0 32.1 32.7 32.6 32.6 32.7 32.7 32.7 32.6 32.6 32.6 32.7	132.0 131.9 132.2 132.2 132.7 133.4 133.5 136.0 137.2 139.6 140.7 141.6 141.5 140.7 140.4	1002 1004 1004 1004 1006 1008 1010 1010 1012 1014 1016 1012 1014 1014	35	2.0 2.0 2.0 2.0 2.0	TD TD TD TD TD L L L L L L L L

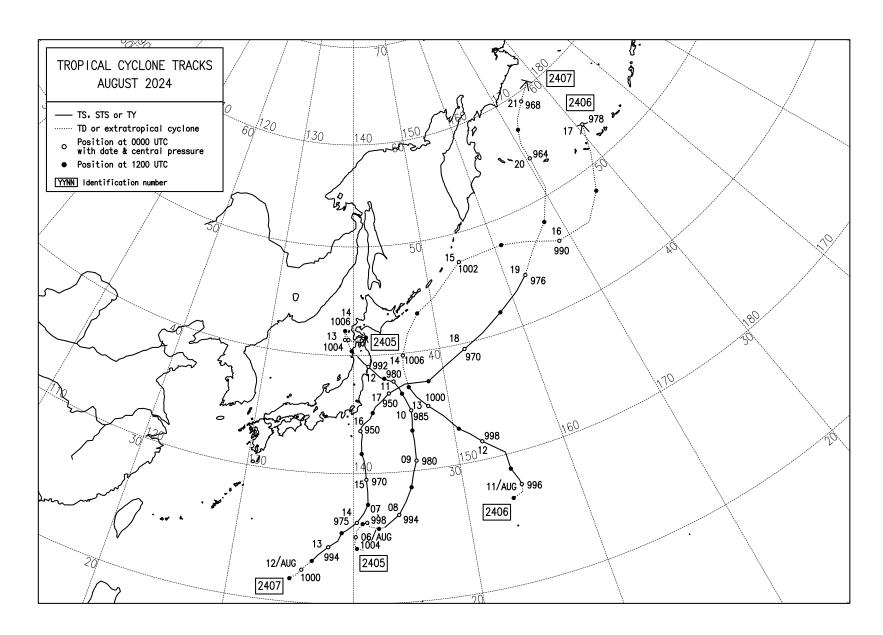
Date	e/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade	Date/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade	Date/Time	Cent	er Position	Central pressure	Max Wind	CI num.	Grade
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)			(UTC)		Lon (E)	(hPa)	(kt)			(UT		N) Lon (E)	(hPa)	(kt)		
Con	25/10	1/0	TY JE 148.9	BI (24 1006	17)	0.0	TD	O-+ 04/10			JAT (2	(419) -	1.0	TD	Oct. 18/		STS TR	1008 1008	2420)	_	TD
Sep.	25/18 26/00	15.4		1006	_	0.0 0.5	TD	Oct. 04/18 05/00		148.2	1006 1006	_	1.0 1.5	TD TD	18/			1006	_	_	TD
	26/06	16.0		1004	-	1.0	TD	05/06		147.1	1004	-	1.5	TD	19/			1008	-	-	TD
	26/12		147.0	1004	-	1.5	TD	05/12		146.7	1006	-	1.5	TD	19/			1004	_	-	TD
	26/18 27/00	16.8 17.2	146.6 146.1	1004 1002	- 35	1.5 2.0	TD TS	05/18		146.6	1006	_	1.5	TD	19/ 19/			1006 1004	_	0.0	TD TD
	27/06	17.7		1002	35	2.0	TS	06/00 06/06		145.6 145.2	1008 1004	35	1.5 2.0	TD TS	20/			1004	-	0.0	TD
	27/12	18.7	145.3	1002	35	2.0	TS	06/12		145.4	1004	35	2.0	TS	20/			1002	-	0.5	TD
	27/18	19.4	144.6	1002	35	2.0	TS	06/18		145.7	1004	35	2.0	TS	20/ 20/			1002 1000	_	1.0 1.5	TD TD
	28/00 28/06	20.1	143.3 142.8	1002 1002	35 35	2.0 2.0	TS TS	07/00		146.0	1004	35	2.0	TS	21/			1000	_	1.5	TD
	28/12	21.7	142.8	1002	35	2.0	TS	07/06 07/12	21.8 23.0	146.6 147.1	1004 1004	35 35	2.0 2.0	TS TS	21/			998	-	1.5	TD
	28/18	22.2	142.0	1002	35	2.0	TS	07/18		147.2	1002	35	1.5	TS	21/			998 994	- 35	1.5	TD
	29/00	23.0	141.9	1002	35	2.0	TS	08/00	23.9	147.0	1002	35	1.5	TS	21/ 22/			994	35 35	2.0 2.5	TS TS
	29/06 29/12	23.8 24.4		1002 1002	35 35	2.0 2.0	TS TS	08/06		147.0	1000	35	1.5	TS	22/			990	45	2.5	TS
	29/18	24.9	140.7	1002	35	2.0	TS	08/12 08/18		147.4 148.2	1000 1000	35 35	1.5 1.5	TS TS	22/			990	45	2.5	TS
	30/00	26.2		1000	40	2.5	TS	09/00		149.0	1000	35	1.5	TS	22/ 23/		2 125.6	990	45 50	2.5	TS STS
	30/06	27.9	140.8	994	45	2.5	TS	09/06		149.4	998	35	2.0	TS	23/			985 985	50	2.5 2.5	STS
	30/12 30/18		140.9 141.1	992 990	50 55	3.0 3.5	STS STS	09/12		149.2	998	35	2.0	TS	23/			985	50	3.0	STS
Oct.	01/00	32.6	141.7	980	65	4.5	TY	09/18		149.3	996	35	2.0	TS	23/			985	50	3.0	STS
	01/06	34.8	142.3	980	65	4.5	TY	10/00 10/06		150.1 150.9	996 994	40 40	2.0 2.0	TS TS	24/			985	50 50	3.0	STS
	01/12	37.2	143.4	980	65	4.5	TY	10/00		152.7	990	40	2.0	TS	24/ 24/			985 985	50 50	3.0 3.0	STS STS
	01/18 02/00	39.2 41.9		980 985	65 60	4.5 4.0	TY STS	10/18	39.2	154.2	985	45	2.0	TS	24/			985	50	3.0	STS
	02/00	45.1	153.3	990	50	3.5	STS	11/00		154.0	982	-	2.0	L	25/			985	50	3.0	STS
	02/12	49.0	157.0	992	-	3.0	L	11/06 11/12		154.0	980 976	_	_	L	25/ 25/			985 985	50 50	3.0 3.0	STS STS
	02/18	51.7	162.2	994	-	-	L	11/12		153.3 153.4	976	_	_	L L	25/ 25/			985	50 50	3.0	STS
	03/00						Dissip.	12/00		154.4	984	-	-	Ĺ	26/			975	55	3.0	STS
								12/06		155.6	988	-	-	L	26/			970	60	3.0	STS
Date	/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade	12/12		158.1	992	-	-	L	26/ 26/			975 980	55 50	3.0 3.0	STS STS
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)			12/18 13/00		160.9 162.9	996 998	_	_	L L	27/			985	45	3.0	TS
		TY	KRAT	HON (2418)			13/06		164.2	1000	_	_	L	27/			992	40	3.0	TS
Sep.	26/12	21.7	127.5	1006	-	0.0	TD		52.9	163.0	1000	-	-	L	27/			998	35	3.0	TS
	26/18		127.0	1004	-	0.5	TD	13/18		160.9	998	-	-	L	27/ 28/			1002 1004	_	2.5 2.5	TD TD
	27/00 27/06	20.7 20.0	126.6 126.3	1004 1002	_	1.0 1.5	TD TD	14/00		161.8	996	-	-	L	28/			1004	_	-	TD
	27/12	19.4	126.0	1002	_	1.5	TD	14/06 14/12		163.3 165.1	996 1000	_	_	L L	28/			1004	-	-	TD
	27/18	18.9	125.6	1000	-	2.0	TD	14/18		168.7	1000	_	_	Ĺ	28/			1004	-	-	TD
	28/00	18.5	125.3	998	35	2.0	TS	15/00	48.2	172.2	1000	-	-	L	29/ 29/			1004 1004	_	_	TD TD
	28/06 28/12	18.3 18.3	125.1 124.8	996 990	40 50	2.5 3.0	TS STS	15/06		177.4	1000	-	-	L	29/			1004	_	_	TD
	28/18	18.4	124.5	985	55	3.5	STS	15/12	48.6	180.4	1000	-	-	Out	29/						Dissip.
	29/00	18.7	124.3	980	60	3.5	STS														
	29/06	19.3	123.8	970	70	4.5	TY								Date/Time	Cont	er Position	Central	Max Wind	CLnum	Grade
	29/12	19.8	122.8	965	75 85	5.0	TY										N) Lon (E)	pressure		OI Hulli.	Grade
	29/18 30/00	19.9 20.1	122.4 122.0	950 935	95	5.5 6.0	TY TY								(01	_	/ KONG	(hPa)	(kt) (2421)		
	30/06	20.5	121.2	935	95	6.0	TY								Oct. 24/			1002	-	0.0	TD
	30/12		120.4	935	95	6.0	TY								24/	06 13.	0 148.3	1000	-	0.5	TD
Oct	30/18 01/00	20.6 20.6	120.0 119.6	935 920	100 105	7.0 7.0	TY TY								24/			1000	-	1.0	TD
OCL.	01/06		119.5	920	105	7.0	TY								24/ 25/	18 13. 00 14.		998 998	35 35	1.5 1.5	TS TS
	01/12	21.2	119.3	925	100	6.5	TY										9 142.6	998	35	1.5	TS
	01/18			935	95	6.5	TY										3 141.0	998	35	1.5	TS
	02/00 02/06			940 950	90 85	6.0 5.0	TY TY										4 139.7	996	35	2.0	TS
	02/06			950 955	80	5.0	TY									00 16. 06 16.		996 994	35 35	2.0 2.0	TS TS
	02/18	22.2	119.7	975	65	5.0	TY										2 134.6	994	35	2.0	TS
	03/00			985	55	4.5	STS								26/	18 16.	0 133.3	994	40	2.5	TS
	03/06 03/12			985 1004	50 –	4.5 4.0	STS TD									00 16.		994	40 45	3.0	TS
	03/12	22.6	120.0	1004	-	4.0	Dissip.									06 16. 12 16.	1 131.8 1 131.1	990 985	45 50	3.0 3.5	TS STS
	5																5 130.3	985	50	3.5	STS
															28/	00 16.	8 129.6	980	55	3.5	STS
																06 16.		975	60	3.5	STS
																	6 128.4 2 128.0	975 970	60 65	3.5 4.0	STS TY
																00 17.		960	75	5.0	TY
															29/	06 17.	9 126.7	950	80	5.0	TY
																12 18.		945	85	6.0	TY
																18 18. 00 19.		935 925	90 100	6.0 6.5	TY TY
																06 19. 06 19.		935	95	6.5	TY
															30/	12 20.	4 123.6	940	90	6.5	TY
																	0 122.8	940	90	6.5	TY
																21 21. 00 21.		940 950	90 85	6.0	TY TY
																	4 121.7	950	85	-	TY
																	2 121.3	960	75	6.0	TY
																12 24.		980	55	5.0	STS
															31/ Nov. 01/	18 25. າດ ຂຣ		990 994	45 40	5.0	TS TS
																00 26. 06 28.		994	40 40	4.5 4.0	TS TS
																12 30.		998	-	3.5	L
																18 31.		1000	-	-	L
																	0 128.0	1004	-	-	L
															02/	00					Dissip.

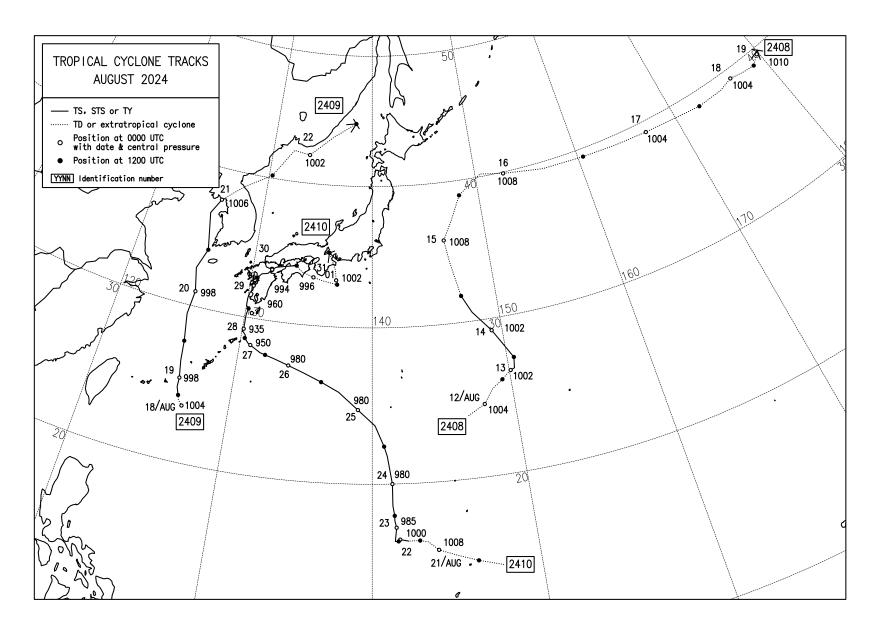
Date/Time	Center	Position	Central	Max Wind	CI num.	Grade	Dat	te/Time	Center	Position	Central	Max Wind	CI num.	Grade	Date/Tim	ne	Center	Position	Central pressure	Max Wind	CI num.	Grade
(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)				(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)			(UT	TC)	Lat (N)	Lon (E)	(hPa)	(kt)		
			(ING (2	2422)					Т	Y MAI	√YI (2	424)							AGI (24	25)		
Nov. 02/18	8.2	140.0	1006	-	0.5	TD	Nov	. 07/18	10.3	168.5	1008	-	-	TD	Nov. 09/	/00	6.7	151.4	1008	_	0.0	TD
03/00	8.9	139.0	1006	-	1.0	TD		08/00	11.0	166.4	1008	-	0.0	TD		/06	7.3	150.3	1006	-	0.0	TD
03/06	9.9	138.1	1004	_	1.5	TD		08/06	11.7	165.1	1006	-	0.0	TD		/12	7.9	149.1	1006	-	0.0	TD
03/12		136.1	1002	35	2.0	TS		08/12		163.6	1008	-	0.5	TD		/18	8.0	147.9	1006	-	0.5	TD
03/18 04/00		134.5 132.8	998	40 40	2.5	TS TS		08/18 09/00	12.2 13.5	161.9 160.4	1004 1004	35 35	1.0	TS TS		/00 /06	9.5 10.3	146.3	1006	_	0.5	TD TD
04/00		131.4	998 996	45	2.5 3.0	TS		09/00	14.5	159.3	1004	35	1.5 1.5	TS		/00 /12	10.3	144.3 142.5	1006 1006	_	0.5 1.0	TD
04/12		130.3	992	55	3.5	STS		09/12		158.7	1002	40	2.0	TS			11.3	140.8	1004	_	1.0	TD
04/18		128.9	985	65	4.0	TY		09/18	15.7	157.7	1000	45	2.0	TS			11.7	139.9	1004	-	1.0	TD
05/00	16.1	127.6	975	75	5.0	TY		10/00	15.8	156.3	1000	45	2.0	TS	11/	/06	12.2	138.5	1004	-	1.5	TD
05/06		126.4	975	75	5.0	TY		10/06	15.6	155.7	1000	45	2.0	TS	11/	/12	12.4	136.7	1004	-	2.0	TD
05/12		125.6	970	80	5.0	TY		10/12	15.6	155.3	1000	45	2.0	TS			12.6	135.0	1002	35	2.5	TS
05/18 06/00		125.0 124.8	970 970	80 80	5.0 5.0	TY TY		10/18 11/00	15.3 14.8	154.7 153.2	1000 1000	45 45	2.0 2.0	TS TS		/00	13.4	133.5	996	45	2.5	TS
06/06		124.4	965	85	5.5	TY		11/06	14.3	152.6	1000	45	2.0	TS			14.0 14.2	131.9 130.5	992 990	50 55	3.0 3.5	STS STS
06/12		124.1	960	90	6.0	TY		11/12	14.1	152.1	1000	45	2.0	TS		/18	14.6	129.0	990	55	3.5	STS
06/18		123.6	950	95	6.0	TY		11/18	13.6	151.1	1000	45	2.0	TS			15.0	127.9	980	65	4.0	TY
07/00	18.6	123.1	950	95	6.0	TY		12/00	13.8	149.3	1000	45	2.0	TS	13/	/06	15.7	126.4	970	75	4.5	TY
07/06		122.4	945	100	6.5	TY		12/06	14.2	147.5	1002	40	2.0	TS	13,	/12	16.2	125.3	960	80	5.0	TY
07/12		121.5	965	85	5.5	TY		12/12		146.3	1002	40	2.0	TS			16.6	124.0	950	90	6.0	TY
07/18 08/00		120.5 119.4	970 980	80 70	5.0 4.5	TY TY		12/18	12.9	145.0	1002	40	2.0	TS			17.2	123.1	940	95	6.0	TY
08/06		118.1	980	70	4.5	TY		13/00 13/06	12.2 12.0	144.3 143.6	1002 1002	40 40	2.0 2.0	TS TS			17.8 18.7	122.2 121.5	955 980	85 65	5.5 5.0	TY TY
08/12		116.9	975	75	4.5	TY		13/12		141.3	1002	40	2.5	TS				120.9	985	60	5.0	STS
08/18		115.9	970	80	5.0	TY		13/18	11.1	139.7	998	45	3.0	TS		/00	20.0	120.3	990	55	4.5	STS
09/00	18.9	114.9	965	85	5.5	TY		14/00	10.6	138.0	992	55	3.5	STS		/06	20.9	120.1	992	50	4.0	STS
09/06		114.1	965	85	5.5	TY		14/06	10.2	137.1	992	55	3.5	STS	15/	/12	21.4	120.1	994	45	3.5	TS
09/12		113.6	965	85	5.5	TY		14/12		135.4	992	55	3.5	STS			21.9	120.2	998	40	3.0	TS
09/18 10/00		113.3 113.2	965 975	85 75	5.5 5.0	TY TY		14/18	10.4	133.5	985	60	4.0	STS			22.3	120.4	1006	-	2.5	TD
10/06		113.2	980	70	4.5	TY		15/00 15/06	10.5 10.9	131.9 130.4	975 960	70 80	5.0 5.5	TY TY				120.5 120.5	1006 1008	_	2.0	TD TD
10/12		112.7	990	60	4.0	STS		15/12		129.0	955	85	6.0	TY		/12 /18	22.2	120.5	1008			Dissip.
10/18	17.9	112.3	994	50	3.5	STS		15/18	12.0	127.8	940	95	6.5	TY		,						Блоопр.
11/00		111.5	994	50	3.0	STS		16/00	12.6	126.7	920	105	7.0	TY								
11/06		111.0	994	50	3.0	STS		16/06	13.3	125.6	920	105	7.0	TY	Date/Tim	ne	Center	Position	Central	Max Wind	CI num.	Grade
11/12		110.6	998	40	2.5	TS		16/12	13.9	124.6	920	105	7.0	TY	(U	ITC)	Lat (N)	Lon (E)	(hPa)	(kt)		
11/18 12/00		110.0 109.7	1000 1002	35 35	2.0 2.0	TS TS		16/18	14.3	123.8	935	100	7.0	TY			Т	S PAE	3UK (2	426)		
12/06		109.4	1002	-	2.0	TD		17/00 17/06	15.0 15.8	122.9 121.9	935 935	100 100	7.0 7.0	TY TY	Dec. 21.	/18	10.1	115.3	1004	_	1.0	TD
	14.0		1008	_	2.0	TD		17/12	16.5	120.7	955	85	6.0	TY	22	/00	10.3	114.8	1006	-	1.5	TD
12/18						Dissip.		17/18	17.6	119.4	975	70	5.5	TY		/06		114.2	1002	35	2.0	TS
								18/00	18.1	118.4	980	65	5.0	TY		/12		113.7	1002	35	2.0	TS
			Central					18/06	18.5	117.3	980	65	5.0	TY		/18	10.6	113.3	1002	35	2.0	TS
Date/Time	Center	Position	pressure	Max Wind	CI num.	Grade		18/12		116.0	985	60	4.5	STS		/00 /06	11.2 11.2	112.9 112.6	1002 1002	35 35	2.0 1.5	TS TS
(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)				18/18	19.0	115.4	992	50	4.0	STS				112.6	1002	35	1.5	TS
	T	Y TOF	RAJI (2	(423)				19/00 19/06	19.0 18.7	114.7 113.3	998 1004	45 35	3.5 3.0	TS TS		/18	11.6	112.4	1002	35	1.5	TS
Nov. 08/06			1006	-	0.5	TD		19/12	18.1	112.0	1010	-	2.0	TD				112.2	1002	35	2.0	TS
08/12		136.0	1008	_	0.5	TD		19/18	17.5	111.4	1012	_	1.5	TD	24	/06	11.5	112.1	1002	35	2.0	TS
08/18		134.7 133.3	1008 1006	_	1.0	TD		20/00		110.6	1012	-	1.5	TD			11.4	111.9	1002	35	2.0	TS
09/00 09/06		131.6	1000	35	1.5 2.0	TD TS		20/06						Dissip.		/18	11.1	111.3	1006	-	2.0	TD
09/12		130.3	1000	40	2.5	TS										/00	10.6	110.7	1006	-	2.0	TD
09/18		128.3	998	45	3.0	TS										/06 /12	9.7 9.4	110.3 110.2	1006 1008	_	1.5 1.5	TD TD
10/00	15.1	126.9	996	50	3.5	STS										/18	0.4	110.2	1000		1.0	Dissip.
	15.2		990	60	3.5	STS																·
	15.5		985	65	4.0	TY																
	15.9		980 980	70 70	5.0	TY TY																
	16.3 17.1		990	55	4.5 4.5	STS																
	17.1		992	50	4.0	STS																
	18.2		992	50	3.5	STS																
12/00	18.6	118.7	992	50	3.0	STS																
	19.1		994	45	2.5	TS																
	19.5		994	45	2.5	TS																
	19.9		994	45 40	2.0	TS																
	20.2 20.7		996 996	40 40	1.5 1.5	TS TS																
	21.0		998	40	1.5	TS																
	21.1		998	40	1.5	TS																
	21.1		1000	35	1.5	TS																
14/06	21.2	113.9	1000	35	1.5	TS																
	21.2		1004	-	1.0	TD																
	21.1		1006	-	1.0	TD																
	20.9		1008	-	1.0	TD																
	20.6	113.2	1008 1008	_	1.0 1.0	TD TD																
15/12		113.7	1000		1.0	Dissip.																

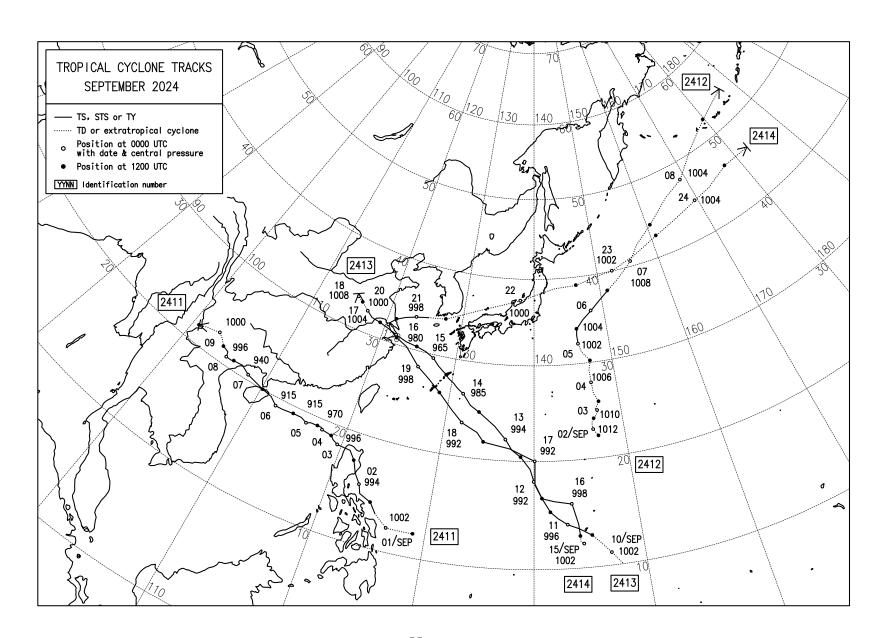
Appendix 2 Monthly Tracks of Tropical Cyclones in 2024

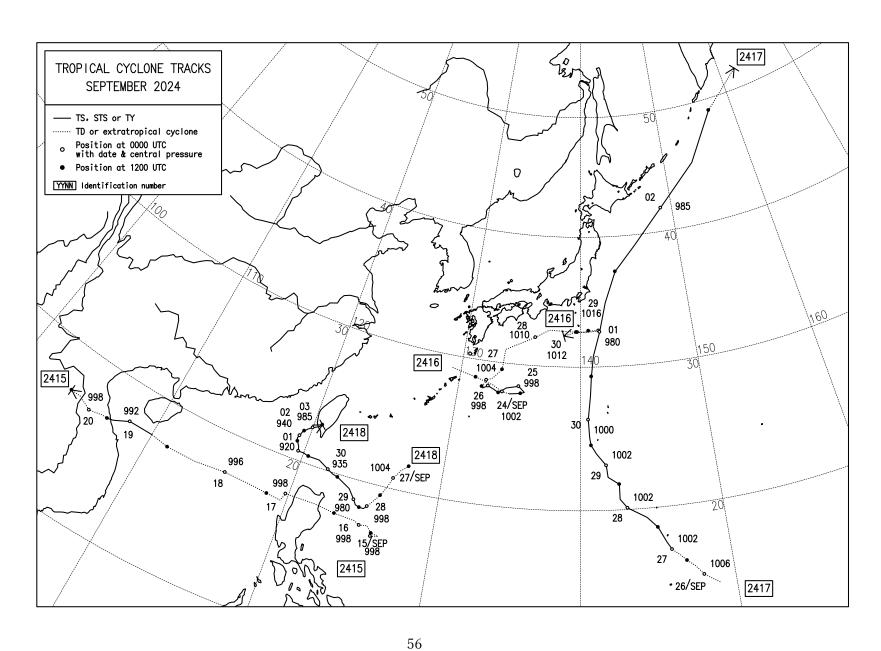


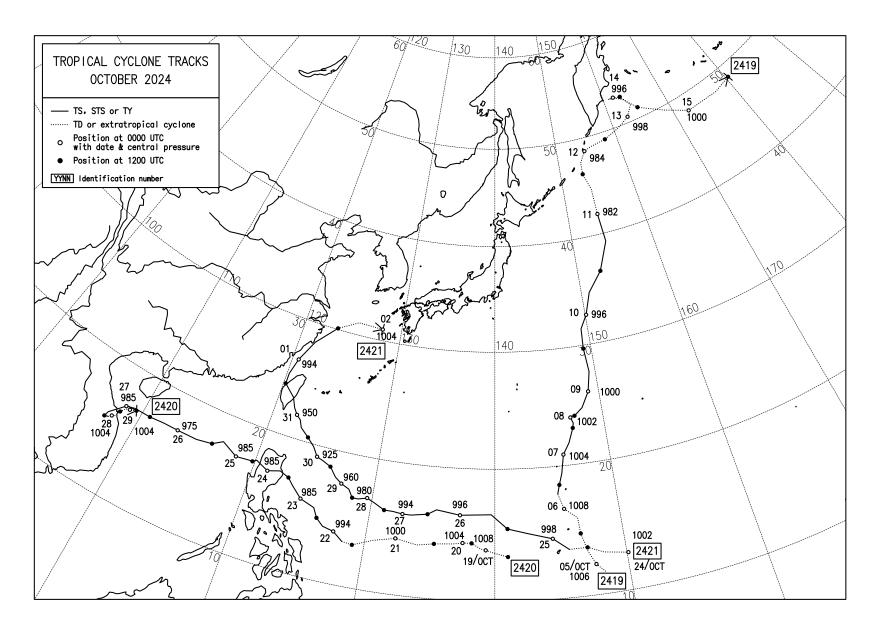


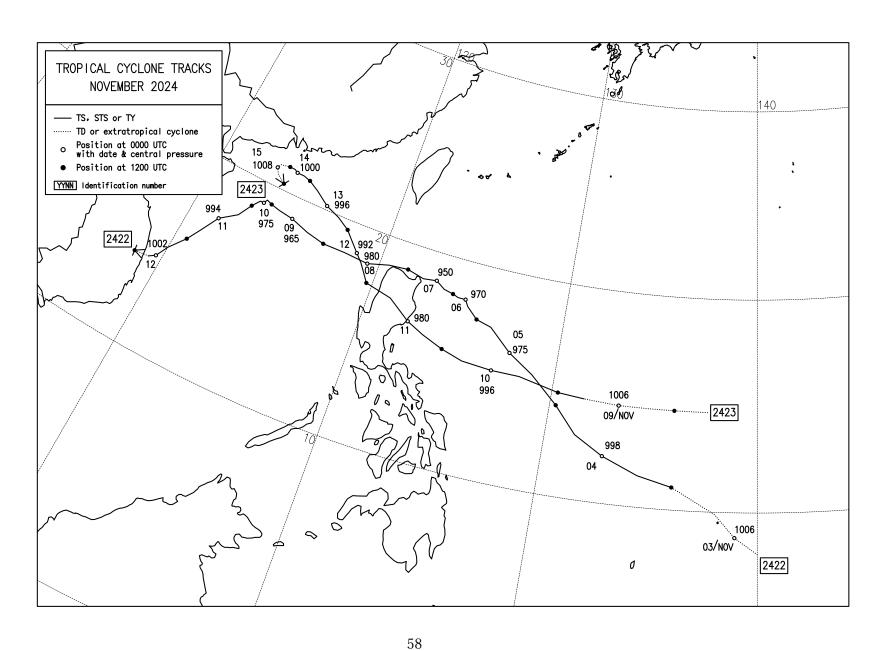


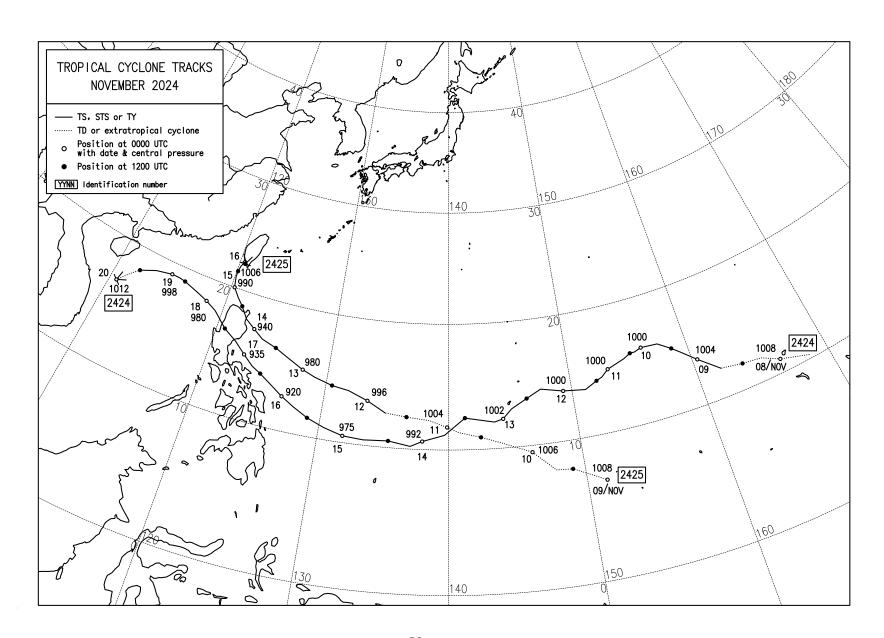


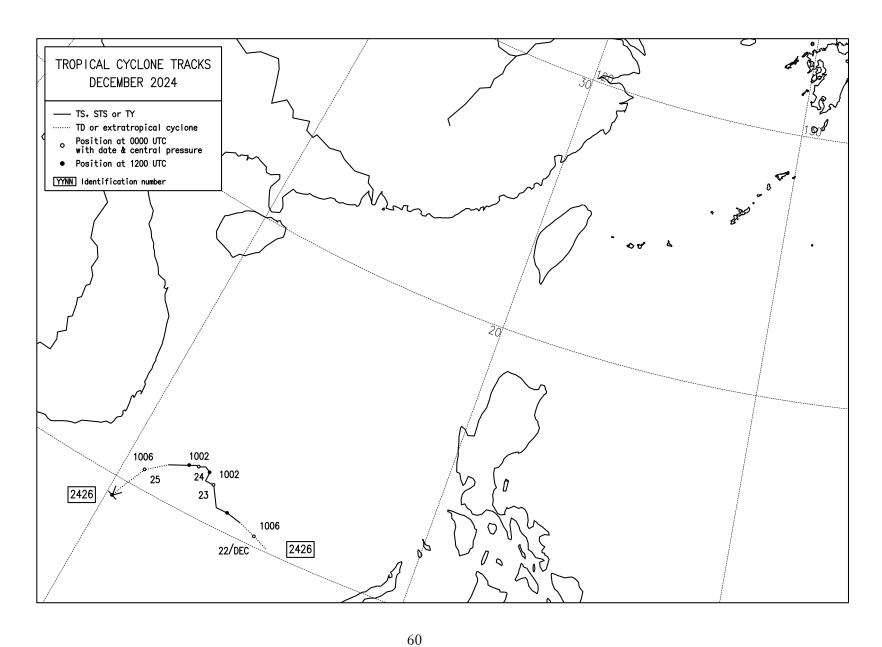












Appendix 3
Errors of Track and Intensity Forecasts for Each Tropical Cyclone in 2024

Date/	/Time	Gra	ade		Cent	er Po	sition	(km)		Cen	tral P	ressu	re (h	Pa)	Max	. Wii	nd Sp	eed (kt) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	Г=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120
		•		-					r(2401)					-					
May.	23/18	TD	TD	25	110	240	195	230	227	-4	0	15	10	5	5	-5	-20	-10	-5
	24/00	TD	TD	91	233	263	232	<i>331</i>	366	-8	0	15	0	-5	10	-5	-20	0	5
	24/06	TD	TD	112	124	179	177	338	496	-4	8	15	0	-5	5	-15	-15	0	5
	24/12	TD	TD	98	132	117	170	269	398	-2	18	15	0	-10	0	-25	-15	0	10
	24/18	TD	TD	35	117		123		493	2	19	15	0	-10		-25	-15	0	10
	25/00	TD	TD	0	124	108	222	396	1192	6	22	5	0	-2	-15	-30	-5	0	5
	25/06	TD	TD	45	44	68	113	172	234	12	22	5	0	-6	-20	-25	-5	0	10
	25/12	TS	TD	57	11	67	61	156	261	22	22	10	0	-4	-30	-25	-10	0	5
	25/18	TS	TD	69	21	92	42	119		21	20	10	0		-30	-20	-10	0	
	26/00	STS	TS	24	70	124	49	95		24	10	0	-2		-30	-10	0	5	
	26/06	STS	TS	0	56	80	139	145		22	5	0	-6		-20	-5	0	10	
	26/12	TY	TS	0	34	53	83	111		22	0	-5	-6		-20	0	5	10	
	26/18	TY	STS	0	84	89	56			20	0	-5			-15	0	5		
	27/00	TY	TY	0	54	45	85			0	-15	-7			5	15	10		
	27/06	TY	TY	35	24	73	15			-5	-10	-11			10	10	15		
	27/12	TY	TY	64	38	67	106			-5	-15	-11			10	15	15		
	27/18	TY	TY	33	69	78				-5	-15				10	15			
	28/00	TY	TY	25	73	46				-10	-12				15	15			
	28/06	TY	TY	46	35	0				-10	-16				15	20			
	28/12	TY	TY	69	37	10				-10	-11				15	15			
	28/18	TY	TY	89	82					-5					10				
	29/00	STS	TY	20	39					-2					10				
	29/06	STS	STS	0	40					-4					10				
	29/12	STS	STS	30	59					-4					5				
	29/18	STS	STS	44															
	30/00	TS	STS	59															
	30/06	TS	TS	29															
	30/12	TS	TS	29															
Initial:	TS/STS/	TY	mean	34	49	63	71	125	261	4	-3	-2	-3	-4	-2	3	3	5	5
Valid:	TS/STS/T	ΓY	sample	21	17	13	9	5	1	17	13	9	5	1	17	13	9	5	1
Initial:	TD(before				126		176		486	0	13	12	1	-5	-4	-19	-14	-1	6
	TD/TS/S7	10,	sample	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7	7
		1.C TI				1													

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date	Time	Gr	ade		Cente	er Pos	sition	(km)		Cent	ral P	ressu	re (hl	Pa)	Max.	Win	d Sp	eed (l	$\overline{(t)}^{\dagger}$
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	=120	T=24	=48	=72	=96 =	=120	T=24	=48	=72	=96 =	=120
							M	aliksi((2402	3)									
May.	30/06	TD	TD	135	91	140				0	-4				0	5			
	30/12	TD	TD	11	114	70				-2	-2				5	0			
	30/18	TD	TD	32	72	39				-2	-4				5	0			
	31/00	TS	TD	98															
	31/06	TS	TS	39															
Initial:	TS/STS/	TY	mean	69															
Valid:	TS/STS/	ГΥ	sample		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Initial:	TD(befo	re u pg.)	mean	59	93	83				-1	-3				3	2			
Valid: '	TD/TS/ST	TS/TY	sample	3	3	3	0	0	0	3	3	0	0	0	3	3	0	0	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/Ti	me	Gra	ıde		Cent	er Pos	sition	(km)		Cen	tral P	ressi	ıre (l	Pa)	Max	. Wir	nd Sp	eed (kt) [†]
J)	JTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120
							G	aemi	(2403)										
Jul.	19/12	TD	TD	62	250	183	95	159	397	0	0	5	5	-5	-5	-5	-10	-5	15
1	19/18	TD	TD	108	204	149	124	243	344	0	7	10	20	-15	-5	-15	-15	-15	20
2	20/00	TS	TD	92	193	99	57	253	353	4	12	15	30	-5	-10	-20	-20	-20	15
2	20/06	TS	TS	110	189		109		375	4	10	5	30	-25	-10	-15	-15	-20	25
2	20/12	TS	TS	63	138	119	237	447	464	-2	0	-5	-15	-30	0	-5	0	20	30
	20/18	TS	TS	63	123		153		169	5	0	10	-25	-30	-10		-10	25	35
	21/00	TS	TS	78	68		221		296	5	5		-25	-35	-10	-10	-10	25	40
2	21/06	STS	STS	92	56		181		250	0	-5		-25	-38	-5	0	-5	25	45
	21/12	STS	STS	94		103	151	178	242	-5	-10	-15		-5	0	5	20	25	10
	21/18	STS	STS	69	15	137	91	70		-5	0	-25			0	0	25	20	
	22/00	TY	TY	39	31	88	69	37		0	5	-20			-5	0	20	15	
	22/06	TY	TY	15	22	69	60	24		-5		-10	-3		0	-5	15	10	
	22/12	TY	TY	15	64		30	56		-10	-20	-5	0		5	25	10	5	
	22/18	TY	TY	11	73	10	40			0	-30	0			0	30	10		
	23/00	TY	TY	11	33	45	41			-5	-5	0			5	10	10		
	23/06	TY	TY	0	11	35	60			5	5	2			0	0	10		
	23/12	TY	TY	0	80	52	118			-10	0	4			20	5	5		
	23/18	TY	TY	10	32	87				-5	5				15	5			
	24/00	TY	TY	24	33					-5	0				10	10			
	24/06	TY	TY	0	98	45				-5	2				10	10			
	24/12	TY	TY	11	56	107				5	4				0	0			
	24/18	STS	TY	11	90					5					5				
	25/00	STS	TY	24	94					5					5				
	25/06	STS	STS	35	41					2					5				
	25/12	STS	STS	15	10					-5					10				
	25/18	TS	STS	30															
	26/00	TS	TS	59															
	26/06	TS	TS	45															
,	26/12	TS	TS	59															
Initial: TS	S/STS/	TY	mean	40	69	79	108	178	307	-1	0	-1	-8	-24	2	2	4	12	29
Valid: TS/			sample	27	23	19	15	11	7	23	19	15	11	7	23	19	15	11	7
Initial: TL	O(befor		mean		227	166	110		371	0	4	8	13	-10				-10	18
Valid: TD	/TS/ST	S/TY	sample	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/Ti	ime	Gra	ıde		Cent	er Po	sition	(km)		Cent	ral P	ressu	re (hPa)		Max	. Wir	ıd Spo	eed (k	t) [†]
()	UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	120	Γ=24	=48	=72	=96 =12	20 T	=24	=48	=72	=96 =	120
	•						Pra	piroon	(240	4)									
Jul.	20/00	TD	TD	142	130	61	93			0	8	12			0	-15	-15		
:	20/06	TD	TD	126	119	137	161			-4	7	4			0	-20	-5		
:	20/12	TD	TD	44	113	119				0	15				-5	-25			
:	20/18	TD	TD	0	67	96				4	15				-10	-25			
:	21/00	TS	TD	0	64	76				6	10				-15	-15			
:	21/06	TS	TS	0	90	104				13	8				-20	-5			
:	21/12	TS	TS	0	80					9					-20				
:	21/18	TS	TS	25	43					7					-15				
:	22/00	STS	STS	15	66					0					0				
:	22/06	STS	STS	15	0					2					0				
:	22/12	STS	STS	11															
:	22/18	STS	STS	39															
	23/00	TS	TS	35															
:	23/06	TS	TS	31															
Initial: TS	S/STS/	TY	mean	17	57	90				6	9				-12	-10			
Valid: TS	/STS/1	ſΥ	sample	10	6	2	0	0	0	6	2	0	0	0	6	2	0	0	0
Initial: TI	D(befor	re upg.)	mean	78	107	103	127			0	11	8			-4	-21	-10		
Valid: TD	/TS/ST	S/TY	sample	4	4	4	2		0	4	4	2	0	0	4	4	2	0	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date	/Time	Gra	ade		Cent	er Po	sition	(km))	Cen	tral P	ressi	ıre (h	Pa)	Max	. Wi	nd Sp	eed (kt) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					
	•			•			N	Iaria	(2405))									
Aug.	06/12	TD	TD	20	80	117	29	77	398	-2	11	16	14	10	5	-15	-20	-10	-5
	06/18	TD	TD	11	124	111	123	375	995	0	14	10	10	14	0	-15	-10	-5	-10
	07/00	TD	TD	24	134	131	178	341	699	2	14	5	10	2	-5	-15	0	-5	-5
	07/06	TD	TD	46	122	78	244	549	1062	4	10	0	5	0	-10	-15	0	-5	5
	07/12	TD	TD	0	115	78	268	655	1191	9	10	5	5	-4	-15	-15	-5	-5	5
	07/18	TS	TS	10	82	56	133	343		10	10	5	5		-15	-15	-5	-5	
	08/00	TS	TS	15	44	44	111	300		5	-5	0	-7		-10	5	0	0	
	08/06	TS	STS	11	45	100	184			0	-10	-5			0	15	10		
	08/12	STS	STS	30	0	91	164			-5	-5	0			5	10	5		
	08/18	STS	STS	0	18	46	17			-5	-10	0			5	15	5		
	09/00	STS	STS	0	56	14	38			-15	-5	-12			20	10	10		
	09/06	STS	STS	11	42	62				-15	-5				20	10			
	09/12	STS	STS	11	43	55				-10	0				15	5			
	09/18	STS	STS	11	35	62				-5	0				10	5			
	10/00	TS	STS	0	58	34				0	-7				5	5			
	10/06	TS	STS	0	62					0					5				
	10/12	STS	STS	14	52					0					5				
	10/18	STS	STS	18	14					-5					5				
	11/00	STS	STS	9	17					-12					5				
	11/06	STS	STS	11															
	11/12	STS	STS	22															
	11/18	STS	STS	0															
	12/00	TS	STS	0															
T:4:-1-	TOIGTO	TX /		10	41		100	222					-						
	TS/STS/		mean	10	41		108			-4 1.4	-4 10	-2	-1		5	7		-3	
-	TS/STS/		sample	18	14	102	160	400		<u>14</u> 3	10	<u>6</u>	2	0	14			2	0
	TD(befor	10,	mean	20			168	400	869		12		9	4		-15	-7 5	-6 5	-2 5
vana:	TD/TS/ST	S/11	sample	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	J

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ıde		Cente	er Pos	sition ((km)		Cent	ral P	ressu	re (hI	Pa)	Max.	Win	d Sp	eed (k	t) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	120	Γ=24	=48	=72	=96 =	=120	Γ=24	=48 =	=72	=96 =	120
	-						Son	-tinh((2406)									
Aug.	10/12	TD	TD	83	91	145				4	10				-5	-5			
	10/18	TD	TD	82	91	90				2	10				0	-5			
	11/00	TS	TD	0	62	112				0	8				0	-5			
	11/06	TS	TD	39	44	110				-2	6				0	-5			
	11/12	TS	TS	44	83					-4					0				
	11/18	TS	TS	0	9					-4					0				
	12/00	TS	TS	61	45					-2					0				
	12/06	TS	TS	0	11					4					-5				
	12/12	TS	TS	0															
	12/18	TS	TS	18															
	13/00	TS	TS	0															
	13/06	TS	TS	0															
Initial:	TS/STS/	TY	mean	16	43	111				-1	7				-1	-5			
Valid:	TS/STS/T	ſΥ	sample	10	6	2	0	0	0	6	2	0	0	0	6	2	0	0	0
Initial:	TD(befor	re upg.)	mean	82	91	117				3	10				-3	-5			
Valid: T	TD/TS/ST	S/TY	sample	2	2	2	0	0	0	2	2	0	0	0	2	2	0	0	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra			Cente	er Pos	sition	(km)		Cen	tral P	ressi	ıre (h	Pa)	May	Wi		eed (·kt)†
Date	(UTC)	Best	Prov.										`						
	(010)	Dest	1100.	1-0					(2407)		-10	12	70	120	1 27		12	- 70	120
Aug.	12/00	TD	TD	11	75	59	51	22	201	, 4	17	20	35	35	- 5	-15	-15	-30	-30
Aug.	12/06	TD	TD	10	94	92	<i>51</i>	67	236	6	10	10	20	20			-10		-10
	12/12	TS	TD	22	67	99		120	316	9	10	25	20	15			-25		-5
	12/18	TS	TS	33	78	76		154	281	15	0	15	20	15	-15		-15		-5
	13/00	TS	TS		110	80		181	233	10	0	10	25	15	-10		-10		-5
	13/06	TS	STS		162	109		186	88	5	5	5	20	15	0	0		-10	-5
	13/12	STS	STS	0	99		109		125	-5	0	0	15	15	5	-5	-5	-5	-5
	13/18	STS	STS	0	108		134		78	-10	0	0	15	9	10	-5	-5	-5	-5
	14/00	STS	STS	10	71	51	114	79		-10	0	10	10		10	-5	-10	0	
	14/06	STS	STS	24	29	67	99	55		-5	0	15	5		5	-5	-5	0	
	14/12	STS	STS	0	38	78	180	149		0	0	15	5		-5	-5	-5	0	
	14/18	STS	STS	0	22	85	82	261		0	0	10	10		-5	-5	0	-5	
	15/00	TY	TY	15	14	92	185			0	10	10			-5	-10	0		
	15/06	TY	TY	11	38	124	210			-5	10	10			0	0	0		
	15/12	TY	TY	15	64	188	181			-10	5	5			5	5	5		
	15/18	TY	TY	0	71	93	176			0	0	5			0	10	5		
	16/00	TY	TY	0	63	69				5	0				-5	10			
	16/06	TY	TY	0	57	44				0	0				10	10			
	16/12	TY	TY	9	118	139				-5	0				15	10			
	16/18	TY	TY	29		190				0	-5				10	5			
	17/00	TY	TY	14	53					0					5				
	17/06	TY	TY	72	48					0					5				
	17/12	TY	TY	86	92					-5					10				
	17/18	STS	TY	71	74					-5					10				
	18/00	STS	TY	44															
	18/06	STS	TY	14															
	18/12	STS	STS	8															
	18/18	STS	STS	34															
Initial	TS/STS/	TY	mean	22	69	96	129	158	187	-1	2	10	15	14	2	0	-5	-9	-5
	TS/STS/1		sample	26	22	18	14	10	6	22	18	14	10	6	22	18	14	10	6
	TD(befor		mean	11	85	76	54	44	219	5	14	15	28	28	-8	-13	-13		-20
	TD/TS/ST	10,	sample	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2

Valid: TD/TS/STS/TY sample 2 2 2 2 2 2 † Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ıde		Cente	er Pos	sition (km)		Centi	ral P	essu	re (hl	Pa)	Max.	Win	d Sp	eed (k	\overline{t}
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	=120	Γ=24 =	-48	=72 =	=96 =	=120	Γ=24 =	-48 =	=72 =	=96 =	-120
				•			Wu	kong	(2408)				•					
Aug.	13/00	TS	TD	45	152					0					0				
	13/06	TS	TS	24	124					0					0				
	13/12	TS	TS	24															
	13/18	TS	TS	78															
	14/00	TS	TS	30															
	14/06	TS	TS	95															
Initial:	TS/STS/	TY	mean	49	138					0					0				
Valid:	TS/STS/	ГΥ	sample	6	2	0	0	0	0	2	0	0	0	0	2	0	0	0	0
Initial:	TD(befor	re upg.)	mean																
Valid: T	TD/TS/ST	TS/TY	sample	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ıde		Cente	er Po	sition	(km)		Cent	ral P	ressu	re (hl	Pa)	Max.	Win	d Sp	eed (k	$(t)^{\dagger}$
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	=120	T=24	=48	=72	=96 =	=120	T=24	=48 =	=72 =	=96 =	120
	-						Jo	ngdari	i(240	9)									
Aug.	18/18	TS	TS	92	31	82				4	-4				-5	0			
	19/00	TS	TS	24	31					2					-5				
	19/06	TS	TS	0	24					0					5				
	19/12	TS	TS	20	68					-4					5				
	19/18	TS	TS	0	35					-6					5				
	20/00	TS	TS	0															
	20/06	TS	TS	15															
	20/12	TS	TD	0															
Initial:	TS/STS/	TY	mean	19	38	82				-1	-4				1	0			
Valid:	TS/STS/7	ΓY	sample	8	5	1	0	0	0	5	1	0	0	0	5	1	0	0	0
Initial:	TD(before	re upg.)	mean																
Valid: T	TD/TS/ST	TS/TY	sample	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ıde		Cente	er Pos	sition	(km)		Cen	tral F	ressi	ure (l	ıPa)	Max	Wi	nd Sr	need ((kt) [†]
	(UTC)	Best		T=0 [‡]					=120					- 1					
	()			1 0					n(241										
Aug.	21/00	TD	TD	15	65	24	33	166	478	2	9	5	5	5	-5	-15	-10	-10	-10
	21/06	TD	TD	11	64	25	81	265	623	4	9	5	5	0	-10	-15	-10	-10	-5
	21/12	TD	TD	21	102	35	68	349	623	12	9	5	5	0	-20	-15	-10	-10	-5
	21/18	TS	TS	15	109	74	59	387	627	15	7	5	0	5	-20	-10	-10	-5	-10
	22/00	TS	TS	15	91	95	88	311	636	11	5	0	-5	20	-10	-5	-5	0	-15
	22/06	TS	TS	21		109		374		5	5		-15	15	-5	-5	0	10	-10
	22/12	STS	STS		101			324		0		-10		10	0	0	5	15	-10
	22/18	STS	STS	11	88		119				-15			25	10	10	15	5	-20
	23/00	STS	STS	11	54				1065		-15		0	40	5	10	15	-5	-35
	23/06	STS	STS	0	11				1160		-25		5	40	5	15	20	-5	-35
	23/12	STS	STS	11					1204		-15		15	40	0	10		-10	-30
	23/18	STS	STS	0					1568		-15		20	40	0	10		-15	-35
	24/00	TY	TY	0					1378		-15	0	20	30	5	10		-15	-30
	24/06	TY	TY TY						1878 1774		-25	0	40	4	5 5	15		-35	-10
	24/12 24/18	TY TY		10					17/4		-30	15	40	0 -2		10	-10	-30 -25	-5
	25/00	TY	TY TY	0					1644	-15	-20 0	20 20	30 15	-2 -4	10 10		-15		0 5
	25/06	TY	TY	30					1102	-15	0	15	-5	-4 -4	10	0		-13 5	5
	25/12	TY	TY	24		127			1102	-15	10		-15		10		-10	15	3
	25/18	TY	TY	0	37		108			-5	15		-12			-10	-5	15	
	26/00	TY	TY	10	30	24		269		15	15		-19			-10	0	25	
	26/06	TY	TY	10	11		115	46		5			-19			-10	20	25	
	26/12	TY	TY	0		109	87			15		-30			-10	-5	30		
	26/18	TY	TY	0	24	91	56			25		-32			-15	0	35		
	27/00	TY	TY	0	15	104	11			0	-20	-34			0	15	40		
	27/06	TY	TY	0	51	125	72			0	-25	-14			0	25	20		
	27/12	TY	TY	0	59	62				0	-25				5	30			
	27/18	TY	TY	0	58	108				-20	-27				15	35			
	28/00	TY	TY	10	94	121				-35	-24				25	35			
	28/06	TY	TY	0	44	51				-25	-19				25	30			
	28/12	TY	TY	0	29					-40					30				
	28/18	TY	TY	10	15					-22					20				
	29/00	TY	TY	11	0					-14					15				
	29/06	STS	STS	11	51					-9					10				
	29/12	TS	STS	0															
	29/18	TS	TS	0															
	30/00	TS	TS	11															
	30/06	TS	TS	0															
Initial:	TS/STS/	TY	mean	8	63	117	213	583	1227	-6	-8	-8	2	17	5	8	6	-2	-16
	TS/STS/T		sample	35	31	27	23	19	15	31	27	23	19	15	31	27	23	19	15
Initial:	TD(befor	re upg.)	mean	16	77	28	61	260	575	6	9	5	5	2	-12	-15	-10	-10	-7
Valid: T	D/TS/ST	TS/TY .	sample	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3
†3.4		1.6 755			20			1: 1											

 $^{^{\}dagger}$ Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/Time	Gra	ide		Cent	er Po	sition	(km)		Cent	ral P	ressi	ıre (h	Pa)	Max	. Wir	nd Sp	eed (kt) [†]
(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					
							Yagi(2411)										
Sep. 01/00	TD	TD	0	177	476			1071	4	2	26	77	75	-10	-5	-30	-60	-55
01/06	TS	TD	49	150	446	424	578	807	4	6	41	70	60	-10	-10	-45	-55	-45
01/12	TS	TS	49	166	317	337	535	754	0	6	50	65	40	0	-10	-45	-50	-30
01/18	TS	TS	0	127	197	151	256	397	-4	12	60	60	20	5	-15	-50	-45	-15
02/00	TS	TS			217			386	-4	20	60	50	20			-45		-10
02/06	TS	TS	11	152	39		153	280	0	25	50	35	25			-35		-15
02/12	TS	TS	0	33	49	101	114	230	0	35	45	15	-20	-5	-30	-30	-10	20
02/18	TS	TS	0	44	39	81	168	183	10	50	40	0	-17	-10	-35	-25	0	20
03/00	TS	TS	0	62	33		135	161	20	55	35	5	-6		-35		0	5
03/06	TS	STS	42	25	59			115	25	40	20	35	-2			-10	-25	0
03/12	STS	STS	67	35	62	115	169		35	35	5	-10		-25	-20	0	10	
03/18	STS	STS	42	11	31	21	49		45	35	-10	-12		-30	-20	10	15	
04/00	TY	TY	0	31	74	33	254		50	20	25	2		-30	-10	-15	-5	
04/06	TY	TY	0	22	57	15	313		35	10	30	2		-20	-5	-20	-5	
04/12	TY	TY	0	15	54	74			10	-5	5			-5	5	5		
04/18	TY	TY	11	71		122			0	0	-12			0	0	0		
05/00	TY	TY	0	92		186			-10	25	0			5	-15	-5		
05/06	TY	TY	0	47		198			-10	30	2			5	-20	-5		
05/12	TY	TY	0		114				-25	-5				15	5			
05/18	TY	TY	0		112				-5	2				5	0			
06/00	TY	TY	0	66	118				0	-2				-5	-5			
06/06	TY	TY	0	52	59				20	0				-20	-5			
06/12	TY	TY	0	77					-10					5				
06/18	TY	TY	0	74					-2					0				
07/00	TY	TY	0	59					0					-5				
07/06	TY	TY	0	11					0					-5				
07/12	STS	TY	11															
07/18	TS	STS	0															
08/00	TS	TS	46															
08/06	TS	TD	35															
Initial: TS/STS/	TY	mean	13	72	111	130	243	368	7	19	26	24	13	-7	-14	-20	-18	-8
Valid: TS/STS/		sample	29	25	21	17	13	9	25	21	17	13	9	25	21	17	13	9
Initial: TD(befo		mean	0	177	476	652		1071	4	2	26	77	75	-10		-30	-60	-55
Valid: TD/TS/S7	TS/TY	sample	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/Time		Grade		Center Position (km)					Cent	ral P	ressu	re (hI	Pa)	Max. Wind Speed (kt) [†]					
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	=120	T=24	=48	=72	=96 =	=120	T=24	=48	=72	=96 =	=120
Leepi(2412)																			
Sep.	05/06	TS	TS	11	105					2					-5				
	05/12	TS	TS	9															
	05/18	TS	TS	18															
	06/00	TS	TS	0															
	06/06	TS	TS	29															
Initial:	Initial: TS/STS/TY mean		14	105					2					-5					
Valid: TS/STS/TY sample		5	1	0	0	0	0	1	0	0	0	0	1	0	0	0	0		
Initial:	Initial: TD(before upg.) mean																		
Valid: TD/TS/STS/TY sample			0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

^{*}Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/Time	Gra	Grade		Center Position (km)					Central Pressure (hPa)					Max. Wind Speed (kt) [†]				
(UTC	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					
(UTC) Best Prov. $ _{T=0}^{\ddagger} $ =24 =48 =72 =96 =120 $ _{T=24} $ =48 =72 =96 =120 $ _{T=24} $ =48 =72 =96 =120 Bebinca(2413)																		
Sep. 09/18	3 TD	TD	0	219	100		100	391	0	-2	2	5	20	0	0	0	-5	-20
10/00		TD	0	35	74	46	212	340	2	0	-9	0	20	-5	0	10	0	-25
10/06	TD	TD	16	74	54	39	170	299	2	0	-5	5	20	-5	0	5	-5	-25
10/12	TS	TS	56	101	74	46	180	153	0	0	-5	5	15	0	0	5	-5	-20
10/18	TS TS	TS	57	48	71	15	112	63	-4	-7	-5	5	5	5	10	5	-5	-10
11/00	TS	STS	33	101	61	15	88	70	-7	-19	-20	0	-5	10	20	20	-5	-5
11/06	TS	STS	24	116	61	122	107	109	-7	-15	-15	0	-5	10	15	15	-5	-5
11/12	TS.	STS	11	133	143	134	169	115	-7	-15	-10	0	2	10	15	10	-5	-10
11/18	TS TS	STS	56	63	82	164	197	87	-12	-15	-5	5	4	20	15	5	-10	-5
12/00	TS	STS	0	11	56	156	145		-14	-15	0	0		20	15	-5	-10	
12/06	TS	STS	15	56	112	249	218		-10	-15	0	5		15	15	-5	-15	
12/12	TS	STS	0	92	74	211	181		-10	-10	-5	8		15	10	0	-20	
12/18	TS	STS	25	70	119	144	35		-5	-5	5	0		5	5	-10	-5	
13/00	TS	TS	0	89	121	65			0	5	-5			0	-10	-5		
13/06	TS	TS	0	89	145	114			0	5	7			0	-10	-25		
13/12	TS	TS	33		136				0	5	2			0	-10	-15		
13/18	STS	TS	0		160	179			5	0	8			-5	-5	-5		
14/00	STS	STS	0	89	172				5	0				-10	-10			
14/06	STS	STS	0	58	70				5	9				-10	-20			
14/12		STS	0	97	119				5	12				-10				
14/18		TY	0		114				-5	4				0	-5			
15/00		TY	24	44					-15					10				
15/06		TY	0	36					-5					0				
15/12		TY	29	36					0					-5				
15/18		TY	31	35					-2					0				
16/00		TY	0															
16/06		STS	0															
16/12		STS	0															
16/18	TS TS	TS	15															
Initial: TS/STS	Initial: TS/STS/TY mean			74	105	125	143	99	-4	-4	-3	3	3	4	2	-1	-9	-9
Valid: TS/STS	Valid: TS/STS/TY sample			22	18	14	10	6	22	18	14	10	6	22	18	14	10	6
Initial: TD(before upg.) mean			5	109	76	43	161	343	1	-1	-4	3	20	-3	0	5	-3	-23
Valid: TD/TS/STS/TY sample			3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date	e/Time	Gra	ade		Cente	er Po	sition	(km)		Cen	tral P	ressu	ıre (h	Pa)	Max.	Win	d Sp	eed (l	kt) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					
	, ,						Pu	ılasaı	n(2414	•)									
Sep	. 15/06	TD	TD	55	214	101	224	190	686	0	4	4	-2	-2	0	-5	-5	0	-5
	15/12	TS	TS	89	208	197	150	334	599	0	0	0	-4	-2	0	0	0	5	-5
	15/18	TS	TS	107	94	123	257	329	680	0	0	-2	-4	0	0	0	0	5	-10
	16/00	TS	TS	74	105	226	273	365		4	0	-2	-2		-5	0	0	-5	
	16/06	TS	TS	135	91	180	263			0	4	0			0	-5	-10		
	16/12	TS	TS	156	99	207	291			0	0	-2			0	0	-5		
	16/18	TS	TS	101	70	257	342			0	-2	0			0	0	-5		
	17/00	TS	TS	181	195	230	370			4	0	0			-5	-5	-5		
	17/06	TS	TS	54	194	271	267			4	0	0			-5	-5	-5		
	17/12	TS	TS		142		426			0	-2	2			0	0	-5		
	17/18	TS	TS	47	178	211				0	0				-5	-5			
	18/00	TS	TS		206					0	2				-5	-5			
	18/06	TS	TS	54	178	140				0	2				-5	-5			
	18/12	TS	TS	39		210				-2	2				0	-5			
	18/18	TS	TS	56	88					2					-5				
	19/00	TS	TS	0	49					2					-5				
	19/06	TS	TS		123					2					-5				
	19/12	TS	TS		133					-2					0				
	19/18	TS	TS	22	65					0					-5				
	20/00	TS	TS	0	78					-2					0				
	20/06	TS	TS	11															
	20/12	TS	TS	0															
	20/18	TS	TS	0															
	21/00	TS	TS	0															
Initial	: TS/STS/	TY	mean	63	127	201	293	343	639	1	0	0	-3	-1	-3	-3	-4	2	-8
	TS/STS/		sample	23	19	13	9	3	2	19	13	9	3	2		13	9	3	2
	: TD(befo		mean		214				686	0	4	4	-2	-2	0	-5	-5	0	-5
	TD/TS/S7	10,	sample	1	1	1	1	1	1	Ī	Ī	1	1	1	Ĭ	1	1	1	1
†		1.0 701																	

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

I	Date/	Time	Gra	ade		Cent	er Po	sition	(km))	Cen	tral F	ressi	ıre (h	Pa)	Max	. Wi	nd Sp	eed (k	t) [†]
		(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24	=48	=72	=96 =	120
				•				S	oulik	(2415)					•				-
	Sep.	16/00	TD	TD	65	104	178	534	713		-2	0	2	-4		5	5	5	10	
		16/06	TD	TD	46	176	119	415	493		-2	-2	-2	-10		5	5	5	10	
		16/12	TD	TD	33	187	177	373	610		-2	-2	-6	-8		5	5	10	5	
		16/18	TD	TD	0	259	162	318			-2	2	-8			5	0	10		
		17/00	TD	TD	0	177	249	274			-2	-2	-8			5	5	10		
		17/06	TD	TD	213	116	266	260			-2	-2	-6			5	5	5		
		17/12	TD	TD	<i>301</i>	119	149	297			-2	-6	-8			5	10	5		
		17/18	TD	TD	295	123	151				2	-8				0	10			
		18/00	TD	TD	221	140	109				2	-4				0	5			
		18/06	TD	TD	82	85	160				2	-6				0	5			
		18/12	TD	TD	63	88	233				-2	-8				5	5			
		18/18	TS	TD	53															
		19/00	TS	TS	0															
		19/06	TS	TS	0															
Ini	tial· '	TS/STS/	TV	mean	18														 -	
		TS/STS/			3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
		TD(befo		sample mean	120	143	178	353	605		<u>-1</u>	-3	-5	<u>-7</u>		4	5	7	8	
		D/TS/ST		sample	11	143	11	<i>555</i>	3	0	-1 11	-3 11	-3 7	3	0	11	3 11	7	3	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date	/Time	Gra	ade		Cente	r Pos	ition	(km)		Cent	ral P	ressu	re (hl	Pa)	Max.	Win	d Sp	eed (l	$(ct)^{\dagger}$
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	-120	T=24	=48	=72	=96 =	=120	T=24	=48	=72	=96 =	=120
							Cir	naron	(241	6)									
Sep.	25/00	TS	TD	20	51					4					0				
	25/06	TS	TS	0															
	25/12	TS	TS	0															
	25/18	TS	TS	22															
	26/00	TS	TS	10															
Initial:	TS/STS/	TY	mean	10	51					4					0				
Valid:	TS/STS/	ГҮ	sample	5	1	0	0	0	0	1	0	0	0	0	1	0	0	0	0
Initial:	TD(befo	re upg.)	mean																
_Valid: '	TD/TS/S7	TS/TY	sample	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date	/Time	Gra	ıde		Cente	er Pos	sition	(km)		Cent	ral P	ressu	re (h	Pa)	Max.	Wir	nd Sp	eed (kt) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96 =	=120			_		
								Jebi(2	2417)				•					•	
Sep.	26/06	TD	TD	63	184	179	337			0	0	2			0	0	-5		
	26/12	TD	TD	39	192	272	362			0	0	2			0	0	-5		
	26/18	TD	TD	111	90	135	149			0	0	2			0	0	-5		
	27/00	TS	TD	81	38	167	91	79	191	0	0	0	18	11	0	0	0	-25	-25
	27/06	TS	TS	63	77	169	91	83	67	0	0	4	18	6	0	0	-5	-30	-15
	27/12	TS	TS	84	164	179	87	118		-2	-2	4	12		5	5	0	-15	
	27/18	TS	TS	101	136	161	65	141		-4	-6	-10	10		10	15	5	-15	
	28/00	TS	TS	79	191	131	72	238		-4	-8	5	7		10	10	-5	-10	
	28/06	TS	TS	38	97	60	11	146		-4	-4	5	4		10	10	-5	-5	
	28/12	TS	TS	101	60	19	99			-4	-2	5			10	5	-5		
	28/18	TS	TS	59	80	66	48			-4	-5	10			10	5	-10		
	29/00	TS	TS	122	15	60	112			-4	5	7			10	-5	-10		
	29/06	TS	TS	31	46	107	321			2	5	2			5	-5	0		
	29/12	TS	TS	42	10	102				4	5				0	-5			
	29/18	TS	TS	20	44	56				2	10				-5	-10			
	30/00	TS	TS	49	30	114				12	5				-15	-5			
	30/06	TS	TS	49	72	227				12	2				-15	0			
	30/12	STS	TS	11	163					12					-15				
	30/18	STS	STS	38	151					10					-10				
Oct.		TY	STS		154					-5					5				
	01/06	TY	STS		161					0					10				
	01/12	TY	STS	38															
	01/18	TY	STS	28															
	02/00	STS	STS	28															
	02/06	STS	STS	8															
Initial	TS/STS/	TV	mean	49	94	116	100	134	129	1	0	3	12	9	1	1	_4	-17	-20
	TS/STS/		sample	22	18	14	100	6	2	18	14	10	6	2	18	14	10	6	2
	TD(befo		mean	71		195				0	0	2		_ <u></u>	0	0	-5		
	TD/TS/ST	10,	sample	3	3	3	3	0	0	3	3	3	0	0	3	3	3	0	0

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ıde		Cente	er Po	sition	(km)		Cen	tral P	ressu	ıre (l	nPa)	Max	. Win	nd Sr	eed (kt) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					
		•	ı				Kı	atho	n(241	8)									
Sep.	26/18	TD	TD	0	137	107	230	551	689	0	11	42	55	45	5	-15	-40	-50	-35
	27/00	TD	TD	22	94	39	220	492	485	2	16	57	65	35	0	-20	-50	-50	-25
	27/06	TD	TD	39	74	24	153	320	582	4	26	55	55	25	-5	-30	-45	-40	-20
	27/12	TD	TD	15	49	109	230	332	496	8	20	40	50	25	-15	-20	-30	-35	-25
	27/18	TD	TD	0	46	114	260	333	522	15	35	35	30	0	-20	-30	-30	-25	-5
	28/00	TS	TS	32	39	117	286	342	577	12	35	35	25	-10	-10	-25	-25	-20	5
	28/06	TS	TS	34	22		233		535	15	30	35	15	-10	-15	-20	-25	-15	10
	28/12	STS	TS	11		167				15	30	30	15			-20		-15	
	28/18	STS	STS	21	53		188			25	20	30	-5			-20		0	
	29/00	STS	STS	35		115				35	35		-15			-25		10	
	29/06	TY	TY	21		122		506		20	30		-15			-20		15	
	29/12	TY	TY	21	96		266			20	15	15				-10			
	29/18	TY	TY	10	42		241			5	5	0			-10	-5	-5		
	30/00	TY	TY	15	33		258			5	-15	-5			-5	10	0		
	30/06	TY	TY	0	33		273			5	-15	-5			-5	10	5		
	30/12	TY	TY	0		137				0	-5				0	5			
	30/18	TY	TY	11		175					-20				5	15			
Oct.	01/00	TY	TY	0		129					-20				10	20			
	01/06	TY	TY	0		112					-15				10	20			
	01/12	TY	TY	15	22					-20					15				
	01/18	TY	TY	11	64					-25					20				
	02/00	TY	TY	11	80					-20					20				
	02/06	TY	TY	11	46					-10					15				
	02/12	TY	TY	0															
	02/18	TY	TY	0															
	03/00	STS	TY	15															
	03/06	STS	STS	0															
Initial:	TS/STS/	TY	mean	12	51	116	237	360	556	2	8	18	3	-10	-2	-5	-14	-4	8
	rs/sts/1		sample	22	18	14	10	6	2	18	14	10	6	2	18	14	10	6	2
Initial:	TD(befor	re upg.)	mean	15	80	79	219	406	555	6	22	46	51	26	-7	-23	-39	-40	-22
_Valid: T	TD/TS/ST	S/TY	sample	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ade		Cente	er Po	sition	(km)		Cent	ral P	ressu	re (hF	Pa)	Max.	Win	d Sp	eed (k	ct) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	=120	Γ=24 =	=48 =	=72 =	=96 =	-120					
							B	arijat(2419)						•				
Oct.	07/00	TS	TD	0	35	146	64			0	0	0			0	0	0		
	07/06	TS	TD	0	44	73	191			2	2	2			0	0	0		
	07/12	TS	TD	61	94	56	146			-2	-4	0			0	5	5		
	07/18	TS	TD	46	150	128	225			-2	-2	5			0	5	0		
	08/00	TS	TD	0	132	101				-4	0				0	-5			
	08/06	TS	TD	0	99	195				-2	2				0	-5			
	08/12	TS	TD	10	189	98				-2	6				0	-5			
	08/18	TS	TD	0	125	334				0	9				0	-5			
	09/00	TS	TD	11	67					2					-5				
	09/06	TS	TS	0	58					2					0				
	09/12	TS	TS	0	106					6					0				
	09/18	TS	TS	15	164					5					0				
	10/00	TS	TS	11															
	10/06	TS	TS	11															
	10/12	TS	TS	22															
	10/18	TS	TS	38															
Initial:	TS/STS/	TY	mean	14	105	141	157			0	2	2			0	-1	1		_
Valid: 7	TS/STS/T	ΓY	sample	16	12	8	4	0	0	12	8	4	0	0	12	8	4	0	
Initial:	TD(befor	re upg.)	mean																-
Valid: T	TD/TS/ST	S/TY	sample	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
†Max. w	ind spee	d for TI	Os are tr	eated	as 30	kt in	this v	alidati	on										
4	n error o																		

Date/	Time	Gra	ade		Cent	er Pos	sition	(km)	, [Cent	ral P	ressu	ıre (l	Pa)	Max	Wir	nd Sp	eed (l	kt) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					
	, ,			1 0					(2420)							 -	·	·	
Oct.	20/06	TD	TD	11	89	263			639	0	4	5	0	0	5	-5	-5	0	0
	20/12	TD	TD	0	253	270	330	427	672	0	4	5	0	0	5	-5	-5	0	0
	20/18	TD	TD	0	161	157	244	311	679	2	0	0	-5	-5	0	-5	-5	0	0
	21/00	TD	TD	101	184	240	280	238	602	2	5	0	0	5	0	-10	-5	-5	-5
	21/06	TD	TD	152	145	145	152	139	293	0	-5	-5	-5	5	-5	0	0	0	-5
	21/12	TD	TD	113	112	101	67	131	346	0	-5	-5	-5	0	-5	0	0	0	0
	21/18	TS	TS	11	82	79	60	184	328	-5	-5	-5	-10	0	0	0	0	5	0
	22/00	TS	TS	44	154	79	55	109	186	0	-5	-10	0	-5	-5	0	5	0	5
	22/06	TS	TS	57	62	0	22	116	283	0	-5	-10	5	-12	-5	0	5	-5	10
	22/12	TS	TS	0	46	24	24	105	351	-5	0	-15	0	-18	0	-5	10	0	15
	22/18	TS	TS	0	81	75	79	187		0	-5	-15	-5		-5	0	10	5	
	23/00	STS	TS	11	132	81	85	166		0	-5	-5	-10		-5	0	5	10	
	23/06	STS	STS	46	112		132			5	-5	5	-12		-5	5	0	15	
	23/12	STS	STS	11	11		152	363		5	-5	0	-18		-5	5	5	20	
	23/18	STS	STS	22	32		317			5	-5	-5			-5	5	10		
	24/00	STS	STS	0	84					0	0	-5			0	5	10		
	24/06	STS	STS	0		120				-5		-12			5	0	15		
	24/12	STS	TS	0		111	276			-10	5	-18			10	0	20		
	24/18	STS	STS	0		152				-10	0				10	5			
	25/00	STS	STS	11		132				0	0				5	5			
	25/06	STS	STS	0		170				5	-7				0	10			
	25/12	STS	STS	0		123				0	-8				5	10			
	25/18	STS	STS	11	85					-5					10				
	26/00	STS	STS	0	53					-10					15				
	26/06	STS	STS	0	85					0					5				
	26/12	STS	STS	43	140					-2					5				
	26/18	STS	STS	0															
	27/00	TS	STS	0															
	27/06	TS	TS	0															
	27/12	TS	TS	24															
Initial	TS/STS/	TV	mean	12	76	01	147	109	287	-2	-3	-8	-6	-9	2	3	8	6	8
	13/313/ TS/STS/7		sample	24	20	16	147	190	4	20	-3 16	-o 12	-o 8	-9 4	20	16	12	8	4
	TD(before		mean		157		236		538	1	10	0	-3	<u> </u>	0	-4	-3	<u>-1</u>	-2
	TD/TS/ST		sample	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6
, ana. I	10/11/01	S/ 1 1	sample							J				- 0			U	U	

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	-30 -30 -35 -35 -35 -30 -20 -20 -15
Kong-rey(2421) Oct. 24/00 TD TD 104 103 269 358 272 262 2 4 2 16 32 0 0 0 -15 24/06 TD TD 134 144 270 280 288 248 0 0 4 15 35 0 5 -5 -15 24/12 TD TD 203 109 246 235 237 153 0 0 9 15 40 0 5 -10 -15 24/18 TS TD 224 143 308 139 144 246 0 0 5 15 45 0 0 -5 -15 25/00 TS TS 230 288 254 163 163 337 -2 -4 0 15 45 5 5 0 -15 25/06	-30 -30 -35 -35 -35 -30 -20 -15
Oct. 24/00 TD TD 104 103 269 358 272 262 2 4 2 16 32 0 0 0 -15 24/06 TD TD 134 144 270 280 288 248 0 0 4 15 35 0 5 -5 -15 24/12 TD TD 203 109 246 235 237 153 0 0 9 15 40 0 5 -10 -15 24/18 TS TD 224 143 308 139 144 246 0 0 5 15 45 0 0 -5 -15 25/00 TS TS 230 288 254 163 163 337 -2 -4 0 15 45 5 5 0 -15 25/06 TS TS 257	-30 -35 -35 -35 -30 -20 -20 -15
24/06 TD TD 134 144 270 280 288 248 0 0 4 15 35 0 5 -5 -15 24/12 TD TD 203 109 246 235 237 153 0 0 9 15 40 0 5 -10 -15 24/18 TS TD 224 143 308 139 144 246 0 0 5 15 45 0 0 -5 -15 25/00 TS TS 230 288 254 163 163 337 -2 -4 0 15 45 5 5 0 -15 25/06 TS TS 257 267 222 210 225 401 0 0 10 25 35 5 0 -10 -20 25/12 TS TS 58 162 169 169 191 423 0 5 10 30 25 5	-30 -35 -35 -35 -30 -20 -20 -15
24/18 TS TD 224 143 308 139 144 246 0 0 5 15 45 0 0 -5 -15 25/00 TS TS 230 288 254 163 163 337 -2 -4 0 15 45 5 5 0 -15 25/06 TS TS 257 267 222 210 225 401 0 0 10 25 35 5 0 -10 -20 25/12 TS TS 58 162 169 169 191 423 0 5 10 30 25 5 -5 -10 -25 25/18 TS TS 24 208 109 109 191 328 0 5 10 35 25 0 -5 -10 -25 26/00 TS TS 0 177 48 100 214 303 0 10 20 45 15 0	-35 -35 -30 -20 -20 -15 10
25/00 TS TS 230 288 254 163 163 337 -2 -4 0 15 45 5 5 0 -15 25/06 TS TS 257 267 222 210 225 401 0 0 10 25 35 5 0 -10 -20 25/12 TS TS 58 162 169 169 191 423 0 5 10 30 25 5 -5 -10 -25 25/18 TS TS 24 208 109 109 191 328 0 5 10 35 25 0 -5 -10 -25 26/00 TS TS 0 177 48 100 214 303 0 10 20 45 15 0 -10 -20 -35 26/06 TS TS 0 178 108 153 236 360 4 5 10 10 -15 -5 -5 -5 -10	-35 -30 -20 -20 -15 10
25/06 TS TS 257 267 222 210 225 401 0 0 10 25 35 5 0 -10 -20 25/12 TS TS 58 162 169 169 191 423 0 5 10 30 25 5 -5 -10 -25 25/18 TS TS 24 208 109 109 191 328 0 5 10 35 25 0 -5 -10 -25 26/00 TS TS 0 177 48 100 214 303 0 10 20 45 15 0 -10 -20 -35 26/06 TS TS 0 178 108 153 236 360 4 5 10 10 -15 -5 -5 -5 -10	-30 -20 -20 -15 10
25/12 TS TS 58 162 169 169 191 423 0 5 10 30 25 5 -5 -10 -25 25/18 TS TS 24 208 109 109 191 328 0 5 10 35 25 0 -5 -10 -25 26/00 TS TS 0 177 48 100 214 303 0 10 20 45 15 0 -10 -20 -35 26/06 TS TS 0 178 108 153 236 360 4 5 10 10 -15 -5 -5 -5 -10	-20 -20 -15 10
25/18 TS TS 24 208 109 109 191 328 0 5 10 35 25 0 -5 -10 -25 26/00 TS TS 0 177 48 100 214 303 0 10 20 45 15 0 -10 -20 -35 26/06 TS TS 0 178 108 153 236 360 4 5 10 10 -15 -5 -5 -5 -10	-20 -15 10
26/00 TS TS 0 177 48 100 214 303 0 10 20 45 15 0 -10 -20 -35 26/06 TS TS 0 178 108 153 236 360 4 5 10 10 -15 -5 -5 -5 -10	-15 10
26/06 TS TS 0 178 108 153 236 360 4 5 10 10 -15 -5 -5 -5 -10	10
ACUA MA MA AL 188 118 188 400 180 8 0 18 5	20
26/12 TS TS 31 155 115 157 293 478 5 0 15 5 -35 -10 -5 -10 -5	30
26/18 TS TS 57 102 72 144 241 302 0 5 25 5 -45 -5 -10 -15 -5	40
27/00 TS TS 57 48 94 148 238 238 5 10 25 -15 -49 -10 -15 -20 5	45
27/06 TS TS 123 44 64 84 196 270 5 10 10 -25 -51 -10 -15 -10 15	45
27/12 STS TS 93 74 31 117 259 5 20 5 -45 -10 -15 -5 35	
27/18 STS TS 0 44 25 94 117 5 25 -5 -40 -10 -15 5 40	
28/00 STS STS 46 33 39 68 175 15 25 -15 -4 -15 -20 10 10	
28/06 STS STS 49 64 15 91 297 15 0 -25 -4 -10 -5 20 5	
28/12 STS STS 31 34 30 142 15 -5 -30 -10 0 30	
28/18 TY STS 15 32 25 73 15 -15 -10 -10 5 15	
29/00 TY TY 33 15 0 109 20 -25 -4 -15 10 10	
29/06 TY TY 0 10 39 238 -10 -20 -4 0 15 5	
29/12 TY TY 22 22 54 -15 -10 5 10	
29/18 TY TY 11 11 24 -15 -10 5 10	
30/00 TY TY 0 25 46 -35 -9 20 10	
30/06 TY TY 0 47 172 -35 -6 25 10	
30/12 TY TY 15 23 5 5	
30/18 TY TY 10 23 0 10 31/00 TY TY 10 45 -2 10	
31/00 TY TY 10 45 -2 10 31/06 TY TY 0 81 2 0	
31/12 STS TY 15	
31/12 S1S 11 13 31/18 TS STS 0	
Nov. 01/00 TS TS 20	
01/06 TS TS 15	
01/00 15 15 15	
Initial: TS/STS/TY mean 47 87 90 132 212 335 0 1 3 3 0 -1 -2 -1 -3	1
Valid: TS/STS/TY sample 31 27 23 19 15 11 27 23 19 15 11 27 23 19 15	11
Initial: TD(before upg.) mean 147 119 262 291 266 221 1 1 5 15 36 0 3 -5 -15	-32
Valid: TD/TS/STS/TY sample 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	

[†]Max. wind speed for TDs are treated as 30 kt in this validation †Position error of provisional analysis

Date/	/Time	Gra	ade.		Cente	er Pos	sition	(km)	I	Cent	tral P	ressi	ıre (l	Pa)	May	Wi		peed ((kt) [†]
Bute	(UTC)	Best						` /	=120				`						
	(010)	Везт	1101.	1-0		-10			(2422			- 12		120	1 27	-10	- 12		120
Nov.	03/00	TD	TD	102	90	197			489	2	21	20	35	0	- 5	-35	-30	-40	-10
1101.	03/06	TD	TD		185				649	4	21	25	40	0		-35			-10
	03/12	TS	TD	0		239			582	8	24	25	15	0		-40			-15
	03/18	TS	TS	0		206			616	11	22	35	10	5		-35			-15
	04/00	TS	TS	16	99		192		379	10	5	20	-10	5		-15		0	-15
	04/06	TS	TS		101	_	195		368	5	5	25	-10	5		-15		0	-15
	04/12	STS	TS	11	65		148		315	10	10	5	-5	5		-20		-5	-15
	04/18	TY	STS	15	48	31		221	252	5	15	0	0	10		-20	-5		-15
	05/00	TY	TY	11	25	54	163	322	316	0	10	-20	-5	0		-15	10	-5	-5
	05/06	TY	TY	40	33	39	138	218	177	-5	15	-10	10	0	-5	-20	5	-15	-5
	05/12	TY	TY	15	25	84	202	300	253	0	5	0	15	0	-10	-10	-5	-20	-5
	05/18	TY	TY	15	35	46	201	228	126	10	0	5	15	0	-15	-5	-10	-20	-5
	06/00	TY	TY	0	15	55	127	55	82	10	-10	10	5	0	-15	5	-15	-10	-5
	06/06	TY	TY	0	44	67	127	67	53	15	-10	10	0	0	-20	5	-15	-5	-5
	06/12	TY	TY	0	15	64	86	94	92	-5	0	15	2	2	-5	-5	-20	-10	-5
	06/18	TY	TY	11	24	32	33	75	87	5	10	20	6	6	-10	-15	-25	-15	-5
	07/00	TY	TY	0	11	46	24	69	200	-10	15	10	6	6	5	-20	-15	-15	-5
	07/06	TY	TY	0	11	39	33	155		-5	10	0	4		0	-15	-5	-10	
	07/12	TY	TY	15	31	35	67	147		-5	5	-5	0		0	-10	0	0	
	07/18	TY	TY	0	15	22	109	172		0	10	-2	4		-5	-15	0	-5	
	08/00	TY	TY	15	31	22	124	226		5	0	-2	4		-10	-5	0	-5	
	08/06	TY	TY	11	39		175			-5	-5	-2			-5	0	0		
	08/12	TY	TY	11	39		126			10	0	0			-15	-5	0		
	08/18	TY	TY	11	25		193			5	-2	8			-10	0	-5		
	09/00	TY	TY	15	25		132			0	-2	6			-5	0	-5		
	09/06	TY	TY	0		119				0	4				-5	-10			
	09/12	TY	TY	11		101				-5	0				0	0			
	09/18	TY	TY	0	39					-4	0				5	0			
	10/00	TY	TY	15	25	67				-4	-2				5	0			
	10/06	TY	TY	22	70					-4					5				
	10/12	STS	TY	46	49					-6					10				
	10/18	STS	STS	113	25					-2					5				
	11/00	STS	TS	32	33					2					-5				
	11/06	STS	TS	39															
	11/12	TS	TS	0															
	11/18	TS	TS	25															
	12/00	TS	TS	0															
Initial	TS/STS/	TV	mean	15	40	76	141	217	260	2	5	7	3	3		_11	_11	-10	-9
	TS/STS/7		sample	35	31	27	23	19	15	31	27	23	19	15	31	27	23		15
	TD(before		mean	69	137	207		381	569	3	21	23	38	0	-8		-33	-43	-10
	TD/TS/ST	10,	sample	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
	,,	~	~pic				<u> </u>				<u> </u>		<u> </u>					<u> </u>	

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ade		Cente	er Po	sition	(km)		Cen	tral P	ressu	re (h	Pa)	Max	. Win	d Sp	eed (kt) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96	=120	T=24	=48	=72	=96 =	=120			-		
	•						T	oraji	(2423))		•							•
Nov.	08/18	TD	TD	22	87	122	198	236	258	4	18	2	4	0	-10	-30	-5	-5	0
	09/00	TD	TD	11	85	117	178	237	290	6	12	0	-4	-8	-15	-20	0	10	15
	09/06	TS	TS	24	183	258	158	234	214	8	0	-2	-4	-2	-15	0	5	10	5
	09/12	TS	TS	15	44	106	91	178		7	6	0	-4		-10	-10	0	5	
	09/18	TS	TS	44	32	55	113	143		0	2	4	0		-5	-5	-5	0	
	10/00	STS	STS	0	54	25	91	70		-5	2	-2	-2		0	-5	5	5	
	10/06	STS	STS	11	55	69	109	100		-5	0	2	6		5	0	0	-5	
	10/12	TY	STS	25	21	100	84			0	-2	0			0	5	0		
	10/18	TY	TY	0	34	80	61			0	-2	-4			0	5	5		
	11/00	TY	TY	34	32	54	76			0	-4	-2			0	10	5		
	11/06	STS	TY	25	24	35	68			-2	-4	-2			5	10	5		
	11/12	STS	STS	33	43	79				-2	-4				5	5			
	11/18	STS	STS	15	77	100				0	0				0	0			
	12/00	STS	STS	21	38	91				-6	-2				10	5			
	12/06	TS	TS	21	44	103				-6	0				10	0			
	12/12	TS	TS	35	67					-8					10				
	12/18	TS	TS	10	33					-2					0				
	13/00	TS	TS	0	35					0					0				
	13/06	TS	TS	11	64					0					0				
	13/12	TS	TS	25															
	13/18	TS	TS	39															
	14/00	TS	TS	11															
	14/06	TS	TS	0															
Initial	TS/STS/	TV	mean	19	52	89	05	145	214	-1	-1	-1	-1	-2	1	2	2	3	5
	TS/STS/		sample	21	17	13	9	5	1	17	13	9	5	1	17	13	9	5	1
	TD(before	-	mean	16	86	120		236	274	5	15	1	0	-4	-13	-25	-3	3	8
	TD/TS/ST	10,	sample	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
	2/15/51	~, 1 1	Sample	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>		<u> </u>									

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time T	Gra	ide		Cente	er Pos	sition	(km)		Cent	ral P	ressi	ıre (h	Pa)	Mav	Wir	nd Sm	eed (kt) [†]
2 410/	(UTC)	Best	Prov.										`						
	(010)	Dest	1 100.	1=0	-24	-40			$\frac{-120}{(2424)}$		-40	-12	-90	-120	1-24	-40	-12	-90	-120
Nov.	09/00	TS	TD	11	40	316		ali-yl	(2424)	4	6	10			=	-10	15		
NOV.											2								
	09/06	TS	TS	15		302				2		4			-5		-10		
	09/12	TS	TS			312				-2	2	4			5		-10		
	09/18	TS	TS			317				-2	2	4			5		-10		
	10/00	TS	TS			259				0	4	6			0	-10			
	10/06	TS	TS			214				0	2	6			0		-10		
	10/12	TS	TS			280				0	2	6			0		-10		
	10/18	TS	TS			327				0	2	10			0		-15		
	11/00	TS	TS			358		•••		0	2	16			0		-25		
	11/06	TS	TS				338		218	-2	-2	4	30	70	5	5		-20	-45
	11/12	TS	TS				221		189	-2	-2	0	30	65	5	5		-20	-40
	11/18	TS	TS				288		336	-2	2	5	40	45	5	0		-25	-30
	12/00	TS	TS				303		400	-2	4	10	55	40	5	-5		-30	-25
	12/06	TS	TS				204		232	0	0	15	45	30	0	0		-20	-15
	12/12	TS	TS				213		267	-2	-7	15	45	10	5	10		-20	0
	12/18	TS	TS				148		216	2	-5	25	30	-5	0		-10		10
	13/00	TS	TS		159			116	101	8	5	45	30	-5	-10		-20		10
	13/06	TS	TS		112	70	54	70	145	6	20	45	30	-5		-10			10
	13/12	TS	TS	55	25	56		116	157	0	20	45	15	5		-10		-5	0
	13/18	TS	TS	16	50	31		115	94	0	25	25	10	-2		-10		-5	10
	14/00	STS	STS	33	60	34	34	57	35	5	40	15	5	-8		-15	-5	0	15
	14/06	STS	STS	16	40	54	65	39	15	15	30	15	5	-14		-10	-5	0	25
	14/12	STS	STS	45	40	66	86	110		15	30	5	0		-5	-10	5	5	
	14/18	STS	STS	11	16	11	64	81		25	15	5	0		-10	-5	0	5	
	15/00	TY	TY	11	11	40	56	70		35	5	-5	-8		-20	-5	5	10	
	15/06	TY	TY	11	22	39	25	59		30	5	-5	-6		-15	-5	5	5	
	15/12	TY	TY	0	43	54	69			20	15	0			-10	-10	0		
	15/18	TY	TY	0	0	49	44			0	15	0			0	-15	0		
	16/00	TY	TY	11	22	15	46			-15	10	-6			5	-10	5		
	16/06	TY	TY	11	74	42	46			-15	10	-10			5	-10	10		
	16/12	TY	TY	0	35	22				30	0				-30	0			
	16/18	TY	TY	0	54	44				15	-2				-15	5			
	17/00	TY	TY	0	63	118				12	0				-10	0			
	17/06	TY	TY	15	44	53				12	-6				-10	10			
	17/12	TY	TY	15	15					0					0				
	17/18	TY	TY	0	44					-7					10				
	18/00	TY	TY	11	64					-4					0				
	18/06	TY	TY	0	75					-10					10				
	18/12	STS	STS	0															
	18/18	STS	STS	15															
	19/00	TS	STS	31															
	19/06	TS	TS	34															
Initial:	TS/STS/	TY	mean	19	98	154	196	145	185	5	7	10	21	17	-2	-4	-7	-10	-6
	rs/sts/7		sample	42	38	34	30	17	13	38	34	30	17	13	38	34	30	17	13
	TD(before		mean																
	TD/TS/ST		sample	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
÷	,_,										<u> </u>	_ <u> </u>	<u> </u>				<u> </u>		

[†]Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

	- I		•		_			<i>a</i> :						D \		-			
Date/		Gra				er Po							ıre (h					peed (
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48				T=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120
							J	Jsagi	(2425)										
Nov.	10/00	TD	TD	11	86	141	170	224	207	0	0	12	50	0	5	5	-10	-35	5
	10/06	TD	TD	0	98	165	238	262	214	-2	6	22	35	2	5	-5	-20	-25	-5
	10/12	TD	TD	11	130	189	233	252	293	-2	8	32	10	0	5	-10	-25	-5	0
	10/18	TD	TD	16	107	171	193	168	263	0	8	42	5	-4	0	-10	-35	0	5
	11/00	TD	TD	0	87	120	149	122	123	6	18	52	0	-8	-10	-20	-40	5	15
	11/06	TD	TD	11	76	118	139	178	226	8	22	30	-2	-10	-10	-20	-20	10	20
	11/12	TD	TD	0	73	86	120	135	93	10	32	5	-4	-12	-15	-25	0	15	20
	11/18	TS	TS	16	43	54	47	135		6	40	0	-8		-5	-30	5	20	
	12/00	TS	TS	0	32	44	71			5	40	-5			-5	-30	5		
	12/06	STS	STS	0	21	40	43			10		-12			-15	-20	10		
	12/12	STS	STS	0	11	15	47			10	-5	-14			-10	0	15		
	12/18	STS	TY	0	24	35	98				-10	-18			-15	5	20		
	13/00	TY	TY	11	46	76				25	-15				-20	10			
	13/06	TY	TY	0	70	104				10	-17				-10	15			
	13/12	TY	TY	15	35	99					-14				20	15			
	13/18	TY	TY	11	44	89					-13				20	20			
	14/00	TY	TY	0	39					-30					25				
	14/06	TY	TY	0	33					-12					15				
	14/12	TY	TY	0	62					-4					10				
	14/18	STS	STS	0	15					0					0				
	15/00	STS	STS	0															
	15/06	STS	STS	10															
	15/12	TS	TS	46															
	15/18	TS	TS	91															
Initial	TS/STS/	TY	mean	12	37	62	61	135		-2	- 3	-10	-8		1	-2	11	20	
	rs/sts/		sample			9	5	133	0	13	9	5	-0 1	0		9	5	1	0
	TD(befo		mean	7	94		177		203	3	13	28	13	-5		-12		<u>-5</u>	9
	TD/TS/ST	10,	sample	7	7	7	7	7	7	7	7	7	7	-3 7	-3 7	7	7	-3 7	7
† 7		1.6 75																	

 $^{^{\}dagger}$ Max. wind speed for TDs are treated as 30 kt in this validation

[‡]Position error of provisional analysis

Date/	Time	Gra	ade		Cente	er Po	sition	(km)		Cent	ral P	ressu	re (hP	a)	Max.	Wine	d Spe	eed (k	t) [†]
	(UTC)	Best	Prov.	T=0 [‡]	=24	=48	=72	=96 =	=120	T=24	=48	=72	=96 =	120	T=24 =	=48 =	=72 =	=96 =	120
							P	abuk(2	2426))									
Dec.	22/00	TD	TD	137	55	73	125			-2	-2	0			0	0	0		
	22/06	TS	TD	112	40	99				-4	-4				0	0			
	22/12	TS	TD	22	69	142				-4	-4				0	0			
	22/18	TS	TD	94	99					-2					0				
	23/00	TS	TD	11	120					0					0				
	23/06	TS	TS	16	113					0					0				
	23/12	TS	TS	40	118					0					0				
	23/18	TS	TS	35															
	24/00	TS	TS	11															
	24/06	TS	TS	40															
	24/12	TS	TS	71															
Initial:	TS/STS/	TY	mean	45	93	120				-2	-4				0	0			
Valid: 7	rs/sts/t	Ϋ́	sample	10	6	2	0	0	0	6	2	0	0	0	6	2	0	0	(
Initial:	TD(befor	e upg.)	mean	137	55	73	125			-2	-2	0			0	0	0		_
Valid: 1	TD/TS/ST	S/TY	sample	1	1	1	1	0	0	1	1	1	0	0	1	1	1	0	0
†Max. w	ind spee		Os are tr		as 30	kt in	this v	alidati	on										

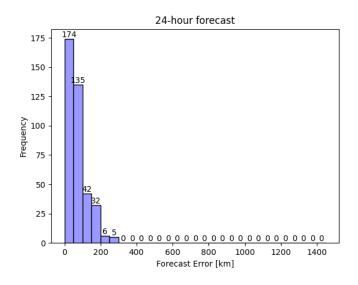
[‡]Position error of provisional analysis

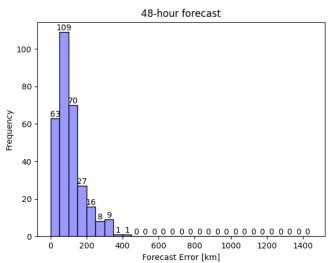
Appendix 4
Monthly and Annual Frequencies of Tropical Cyclones

Monthly and annual frequencies of tropical cyclones that attained TS intensity or higher in the western North Pacific and the South China Sea for 1951 - 2024

	INOI	rın Pa	icilic	ana t	he So	uth C		Sea 1		<u> </u>	2024		
Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
1951		1	1	2	1	1	3	3	2	4	1	2	21
1952		•	•	-	•	3	3	5	3	6	3	4	27
1953		1			1	2	1	6	3	5	3	1	23
1954			1		1		1	5	5	4	3	1	21
1955	1	1	1	1		2	7	6	4	3	1	1	28
1956			1	2		1	2	5	6	1	4	1	23
1957	2			1	1	1	1	4	5	4	3		22
1958	1			1	1	4	7	5	5	3	2	2	31
1959		1	1	1			2	5	5	4	2	2	23
1960				1	1	3	3	10	3	4	1	1	27
1961	1		1		2	3	4	6	6	4	1	1	29
1962		1		1	2		5	8	4	5	3	1	30
1963				1		4	4	3	5	4		3	24
1964					2	2	7	5	6	5	6	1	34
1965	2	1	1	1	2	3	5	6	7	2	2		32
1966				1	2	1	4	10	9	5	2	1	35
1967		1	2	1	1	1	7	9	9	4	3	1	39
1968				1	1	1	3	8	3	5	5		27
1969	1		1	1			3	4	3	3	2	1	19
1970		1				2	3	6	5	5	4		26
1971	1		1	3	4	2	8	5	6	4	2	_	36
1972	1				1	3	7	5	4	5	3	2	31
1973	_		_	_	_		7	5	2	4	3	_	21
1974	1		1	1	1	4	4	5	5	4	4	2	32
1975	1			~	~	2	2	4	5	5	3	1	21
1976	1	1	,	2	2	2	4	4	5	1	1	2	25
1977			1	,		1	3	3	5	5	1	2	21
1978 1979	1 1		1	1 1	2	3	4	8 2	5 6	4	4 2	2	30 24
	1		1		4	1	4			4			
1980 1981			1	1 2	4	1 3	4	2 8	<u>6</u>	2	3	1	24 29
1981			3	2	1	3	3	5	5	3	1	1	25
1982			3		1	1	3	5	2	5	5	2	23
1984						2	5	5	4	7	3	1	27
1985	2				1	3	1	8	5	4	1	2	27
1986	2	1		1	2	2	4	4	3	5	4	3	29
1987	1			1		2	4	4	6	2	2	1	23
1988	1				1	3	2	8	8	5	2	1	31
1989	1			1	2	2	7	5	6	4	3	1	32
1990	1			1	1	3	4	6	4	4	4	1	29
1991			2	1		1	4	5	6	3	6	<u>-</u>	29
1992	1	1	_	_	_	2	4	8	5	7	3		31
1993			1			1	4	7	6	4	2	3	28
1994				1	1	2	7	9	8	6		2	36
1995				1		1	2	6	5	6	1	1	23
1996		1		1	2		6	5	6	2	2	1	26
1997				2	3	3	4	6	4	3	2	1	28
1998							1	3	5	2	3	2	16
1999				2		1	4	6	6	2	1		22
2000					2		5	6	5	2	2	1	23
2001					1	2	5	6	5	3	1	3	26
2002	1	1			1	3	5	6	4	2	2	1	26
2003	1			1	2	2	2	5	3	3	2		21
2004				1	2	5	2	8	3	3	3	2	29
2005	1		1	1	1		5	5	5	2	2		23
2006					1	2	2	7	3	4	2	2	23
2007				1	1		3	4	5	6	4		24
2008				1	4	1	2	4	4	2	3	1	22
2009					2	2	2	5	7	3	1		22
2010			1				2	5	4	2			14
2011					2	3	4	3	7	1		1	21
2012			1		1	4	4	5	3	5	1	1	25
2013	1	1		_		4	3	6	8	6	2	~	31
2014	2	1	~	2	~	2	5	1	5	2	1	2	23
2015	1	1	2	1	2	2	3	4	5	4	1	1	27
2016				,		1	4	7	7	4	3	1	26
2017	1	1	1	1		1 4	8 5	6	3	3	3	2	27
2018	1		1					9			3	1	29
2019	1	1				1	4	5	6	4	6	1	29
2020		1		1	1	1 2	3	<u>8</u>	3	<u>6</u>	3	1	23 22
		1			1	2	2	5	7		1	1	
2022 2023				2	1	1	3	6	2	5 2	1	1	25 17
2023				1	2	1	2	6	8	3	4	1	26
								0	0	3	- 4	1	20
Normal													
1991-2020	0.3	0.3	0.3	0.6	1.0	1.7	3.7	5.7	5.0	3.4	2.2	1.0	25.1

Appendix 5 Other Verification Charts





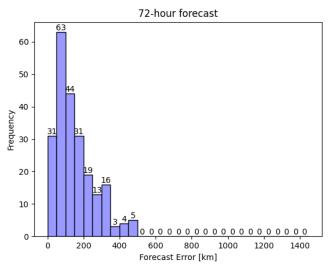


Figure A5.1 Histograms of RSMC 24-, 48- and 72-hour forecast position errors

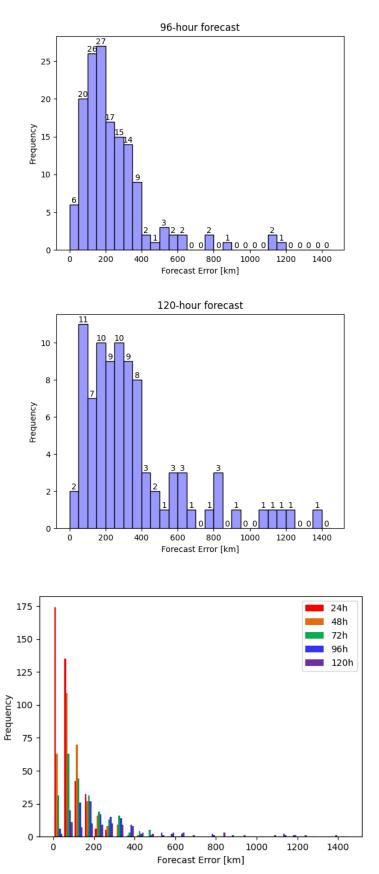


Figure A5.2 Histograms of RSMC 96-hour, 120-hour and all lead time forecast position errors

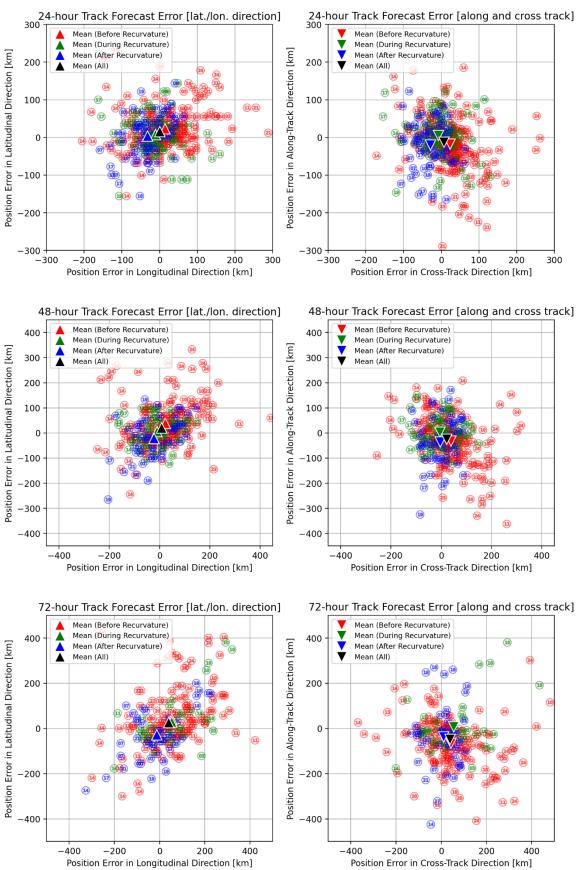


Figure A5.3 Scatter diagrams of RSMC position errors for 24-, 48- and 72-hour forecast in longitudinal/latitudinal and cross/along-track directions: Red, green and blue circles with TC number and triangles denote biases for each initial time and mean biases in the stages before, during and after recurvature, respectively. Black triangles indicate mean bias for all initial time.

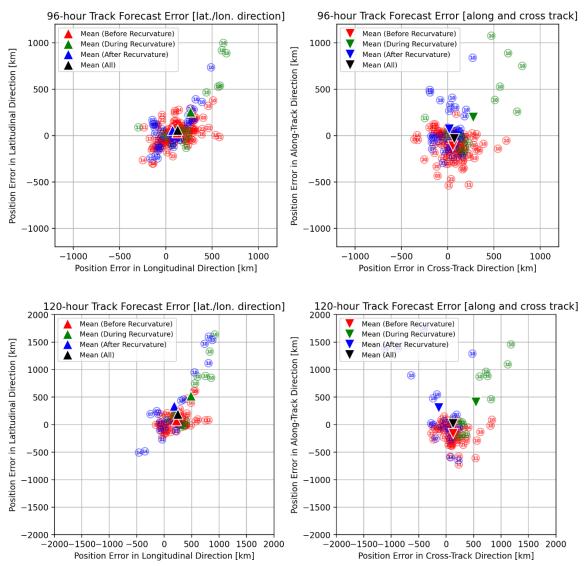


Figure A5.4 Scatter diagrams of RSMC position errors for 96- and 120-hour forecast in longitudinal/latitudinal and cross/along-track directions: Red, green and blue circles with TC number and triangles denote biases for each initial time and mean biases in the stages before, during and after recurvature, respectively. Black triangles indicate mean bias for all initial time.

Table A5.1 Annual mean errors, RMSEs and mean improvement ratios of RSMC maximum wind speed forecasts

		2	4-hour F	orecas	t	4	8-hour I	Forecas	t	7	2-hour l	orecas	t	9	6-hour l	Forecas	st	12	0-hour I	oreca	st
	Tropical Cyclone	Error	RMSE	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE 1	Num.	Impr.
		(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)
TY	Ewiniar (2401)	-0.9	8.9	17	-101	1.8	7.5	13	-79	1.7	4.9	9	-3	2.6	3.5	5	36	2.6	2.6	1	6
TS	Maliksi (2402)	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TY	Gaemi (2403)	0.9	4.2	23	25	1.1	6.1	19	16	2.2	7.2	15	24	6.1	10.3	11	-8	14.7	15.9	7	-162
STS	Prapiroon (2404)	-6.0	7.4	6	-16	-5.1	5.8	2	-35	-	-	0	-	-	-	0	-	-	-	0	-
STS	Maria (2405)	2.8	5.5	14	-30	3.3	5.3	10	-20	2.1	3.5	6	-210	-1.3	1.8	2	8	-	-	0	
TS	Son-tinh (2406)	-0.4	1.0	6	72	-2.6	2.6	2	66	_	-	0	-	-	-	0	-	-	-	0	-
TY	Ampil (2407)	0.9	4.4	22	40	0.0	3.4	18	66	-2.8	4.8	14	60	-4.6	6.5	10	39	-2.6	2.6	6	46
TS	Wukong (2408)	0.0	0.0	2	100	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TS	Jongdari (2409)	0.5	2.6	5	14	0.0	0.0	1	100	-	-	0	-	-	-	0	-	-	-	0	-
TY	Shanshan (2410)	2.4	6.4	31	10	4.2	8.3	27	22	3.2	8.9	23	19	-1.2	8.9	19	11	-8.1	10.8	15	-2
TY	Yagi (2411)	-3.4	7.1	25	32	-7.1	9.3	21	43	-10.1	14.0	17	24	-9.1	14.6	13	20	-4.0	11.2	9	17
TS	Leepi (2412)	-2.6	2.6	1	-6	-	-	0	-	_	-	0	-	-	-	0	-	-	-	0	-
TY	Bebinca (2413)	1.9	5.0	22	12	0.9	6.6	18	23	-0.4	5.9	14	24	-4.4	5.1	10	-18	-4.7	5.5	6	25
TS	Pulasan (2414)	-1.4	1.9	19	47	-1.4	1.9	13	77	-2.0	2.6	9	81	0.9	2.6	3	86	-3.9	4.1	2	76
TS	Soulik (2415)			0	-	-	_	0	-	-		0	-	-		0	-	-	-	0	_
TS	Cimaron (2416)	0.0	0.0	1	100	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TY	Jebi (2417)	0.7	4.8	18	3	0.7	3.6	14	55	-1.8	2.9	10	57	-8.6	9.6	6	-278	-10.3	10.6	2	-131
TY	Krathon (2418)	-1.1	7.3	18	8	-2.4	8.9	14	37	-7.2	8.8	10	42	-2.1	7.2	6	35	3.9	4.1	2	-103
TS	Barijat (2419)	-0.2	0.7	12	72	-0.6	2.2	8	50	0.6	1.3	4	74	-	-	0	-	-	-	0	-
STS	Trami (2420)	0.9	3.3	20	25	1.4	2.5	16	42	4.1	5.0	12	-0	3.2	5.1	8	1	3.9	4.8	4	38
TY	Kong-rey (2421)	-0.5	5.1	27	22	-1.1	5.3	23	48	-0.7	6.9	19	43	-1.5	10.9	15	21	0.7	16.3	11	-21
TY	Yinxing (2422)	-3.7	6.0	31	20	-5.4	7.8	27	18	-5.8	9.0	23	14	-5.3	6.7	19	23	-4.6	5.3	15	39
TY	Toraji (2423)	0.5	3.4	17	48	0.8	3.0	13	62	1.1	2.1	9	79	1.5	3.0	5	70	2.6	2.6	1	72
TY	Man-yi (2424)	-1.2	4.4	38	26	-2.1	4.0	34	62	-3.3	5.5	30	58	-5.0	7.9	17	47	-3.0	11.6	13	18
TY	Usagi (2425)	0.4	7.6	13	21	-0.9	9.7	9	19	5.7	6.4	5	26	10.3	10.3	1	-5	-	-	0	_
TS	Pabuk (2426)	0.0	0.0	6	100	0.0	0.0	2	100	-		0	_	-	_	0		-	-	0	
A	Annual Mean (Total)	-0.3	5.3	394	17	-0.7	6.2	304	37	-1.5	7.3	229	36	-2.5	8.6	150	24	-2.1	10.5	94	2

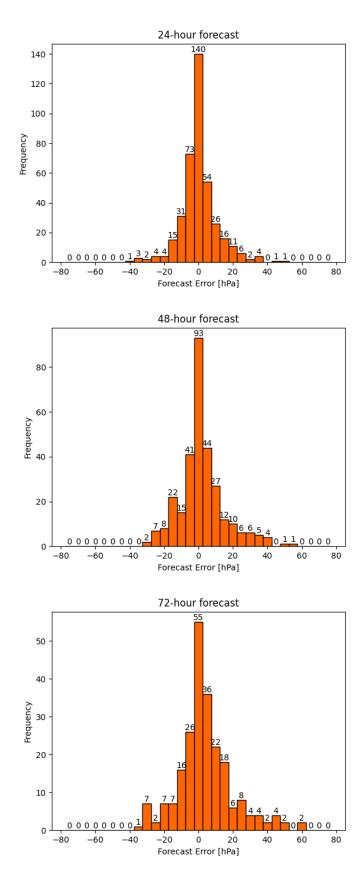


Figure A5.5 Histograms of RSMC 24-, 48- and 72-hour pressure forecast errors

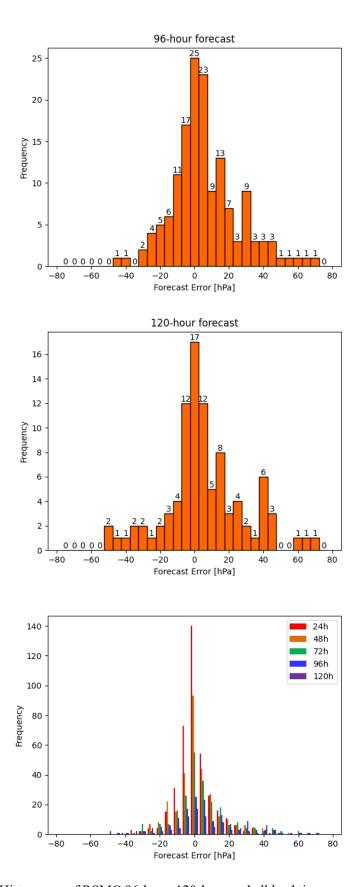


Figure A5.6 Histograms of RSMC 96-hour, 120-hour and all lead time pressure forecast errors

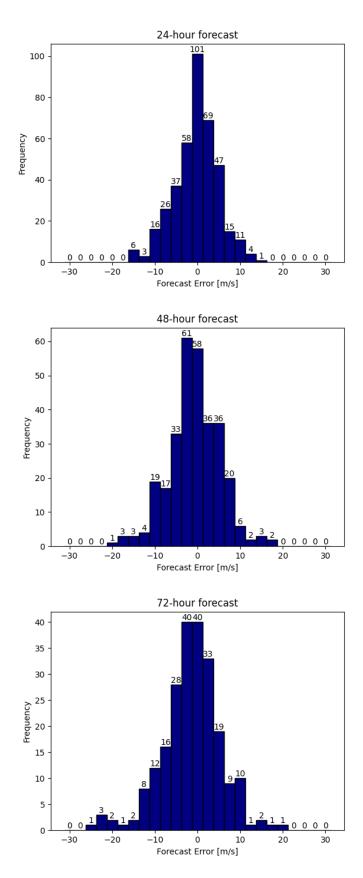


Figure A5.7 Histograms of RSMC 24-, 48- and 72-hour maximum wind speed forecast errors

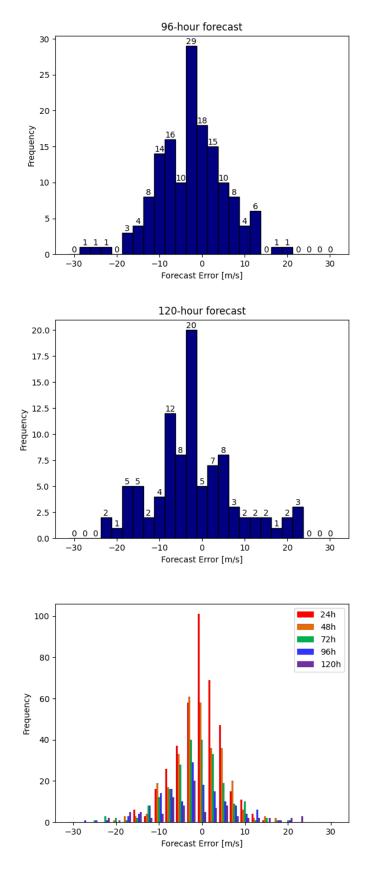


Figure A5.8 Histograms of RSMC 96-hour, 120-hour and all lead time maximum wind speed forecast errors

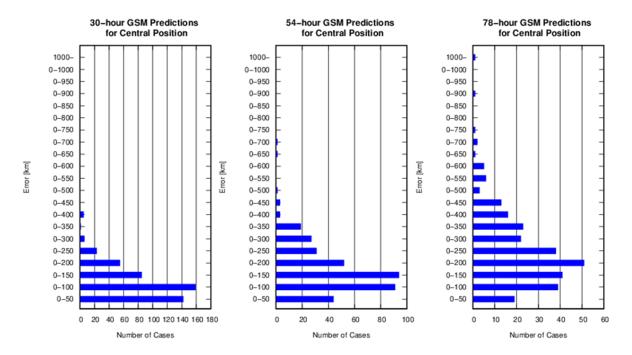


Figure A5.9 Histograms of GSM position errors for 30-, 54-, and 78-hour prediction

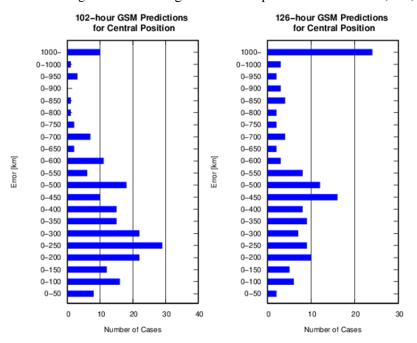


Figure A5.10 Histograms of GSM position errors for 102- and 126-hour prediction

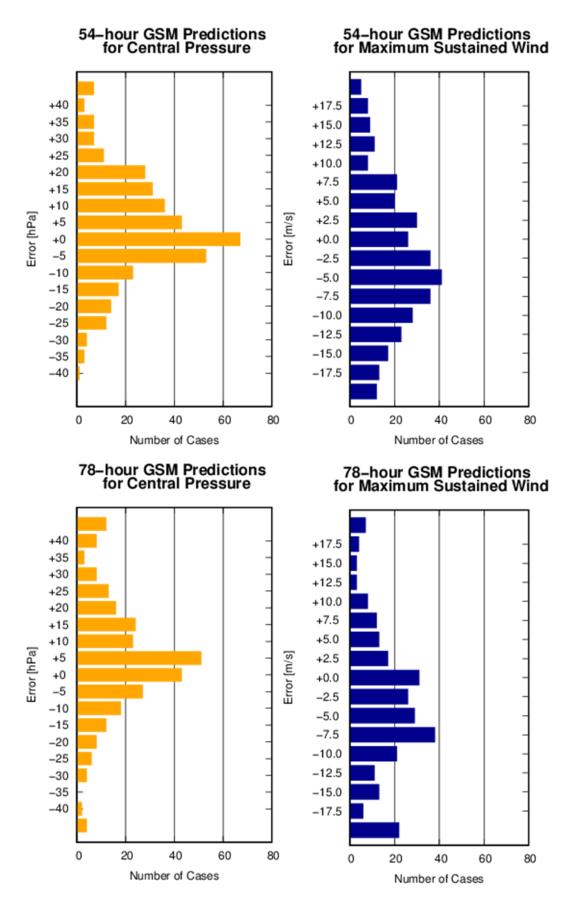


Figure A5.11 Histograms of GSM intensity errors for (top) 54- and (bottom) 78-hour prediction

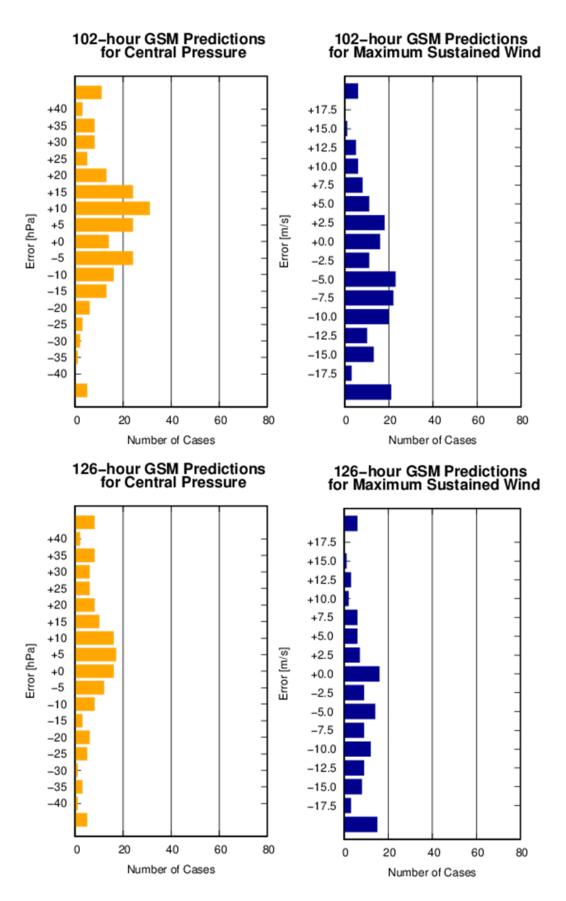


Figure A5.12 Histograms of GSM intensity errors for (top) 102- and (bottom) 126-hour prediction

Appendix 6 Code Forms of RSMC Products

(1) RSMC Tropical Cyclone Advisory (WTPQ50-55 RJTD)

WTPQii RJTD YYGGgg

RSMC TROPICAL CYCLONE ADVISORY

NAME class ty-No. name (common-No.)

ANALYSIS

PSTN YYGGgg UTC LaLa.La N LoLoLo.Lo E (or W) confidence

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

GUST VgVgVg KT

50KT RdRdRd NM (or 50KT RdRdRd NM octant RdRdRd NM octant)
30KT RdRdRd NM (or 30KT RdRdRd NM octant)
(or 30KT RdRdRd NM octant RdRdRd NM octant)

FORECAST

24HF YYGGgg_F UTC LaLa.La_F N LoLoLo.Lo_F E (or W) FrFrFr NM 70%

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

GUST VgVgVg KT

Ft1Ft1<u>HF</u> YYGGgg_F <u>UTC</u> LaLa.La_F N LoLoLo.Lo_F E (or W) FrFrFr <u>NM 70%</u>

MOVE direction SpSpSp KT

PRES PPPP HPA

GUST VgVgVg KT

MXWD VmVmVm KT

Ft2Ft2<u>HF</u> YYGGggF <u>UTC</u> LaLa.LaF N LoLoLo.LoF E (or W) FrFrFr <u>NM 70%</u>

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

GUST VgVgVg KT

Ft3Ft3<u>HF</u> YYGGgg_F <u>UTC</u> LaLa.La_F N LoLoLo.Lo_F E (or W) FrFrFr <u>NM 70%</u>

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

 $\underline{\mathrm{GUST}}\,\mathrm{VgVgVg}\,\underline{\mathrm{KT}}$

 $Ft4Ft4Ft4\underline{HF}\ YYGGgg_F\underline{UTC}\quad LaLa.La_F\ N\ LoLoLo.Lo_F\ E\ (\text{or}\ W)\ FrFrFr\ \underline{NM\ 70\%}$

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

GUST VgVgVg KT=

Notes:

a. <u>Underlined</u> parts are fixed.

b. Abbreviations

PSTN : Position

MOVE : Movement

PRES : Pressure

MXWD : Maximum wind

HF : Hour forecast

c. Symbolic letters

i i : '20', '21', '22', '23', '24' or '25'

 $YYGGgg \hspace{1.5cm} \hbox{:} \hspace{0.5cm} \hbox{Time of observation submitting the data for analysis in UTC} \\$

class : Intensity classification of the tropical cyclone 'TY', 'STS', 'TS' or 'TD'

ty-No. : Domestic identification number of the tropical cyclone adopted in Japan given in four digits (same as the

international identification number)

name : Name assigned to the tropical cyclone from the name list prepared by the Typhoon Committee

common-No. : International identification number of the tropical cyclones given in four digits

LaLa.La : Latitude of the center position in "ANALYSIS" part

LoLoLo.Lo : Longitude of the center position in "ANALYSIS" part

confidence of the center position in "ANALYSIS" part

confidence : Confidence of the center position. 'GOOD', 'FAIR' or 'POOR'

direction : Direction of movement given in 16 azimuthal direction such as 'N', 'NNE', 'NE' and 'ENE'

SpSpSp : Speed of movement
PPPP : Central pressure
VmVmVm : Maximum sustained wind
VgVgVg : Maximum gust wind

RdRdRd : Radii of 30knots and 50knots wind

octant : Eccentric distribution of wind given in 8 azimuthal direction such as 'NORTH', 'NORTHEAST' and 'EAST'

Ft1Ft1 : 48 (00, 06, 12 and 18 UTC) or 45 (03, 09, 15 and 21 UTC)
Ft2Ft2 : 72 (00, 06, 12 and 18 UTC) or 69 (03, 09, 15 and 21 UTC)
Ft3Ft3 : 96 (00, 06, 12 and 18 UTC) or 93 (03, 09, 15 and 21 UTC)
Ft4Ft4 Ft4 : 120 (00, 06, 12 and 18 UTC) or 117 (03, 09, 15 and 21 UTC)

YYGGgg_F : Time in UTC on which the forecast is valid

LaLa.La_F : Latitude of the center of 70% probability circle in "FORECAST" part LoLoLo.Lo_F : Longitude of the center of 70% probability circle in "FORECAST" part

FrFrFr : Radius of 70% probability circle

d. MOVE is optionally described as 'ALMOST STATIONARY' or '(direction) SLOWLY', depending on the speed of movement.

Example:

WTPQ50 RJTD 080000
RSMC TROPICAL CYCLONE ADVISORY
NAME TY 1919 HAGIBIS (1919)
ANALYSIS
PSTN 080000UTC 16.9N 143.8E GOOD
MOVE WNW 13KT
PRES 915HPA
MXWD 105KT
GUST 150KT
50KT 100NM
30KT 350NM EAST 240NM WEST
FORECAST
24HF 090000UTC 19.8N 140.0E 60NM 70%
MOVE NW 10KT
PRES 915HPA
MXWD 105KT
GUST 150KT
48HF 100000UTC 22.8N 138.4E 90NM 70%
MOVE NNW 08KT
PRES 915HPA
MXWD 105KT
GUST 150KT
48HF 100000UTC 26.5N 136.3E 120NM 70%
MOVE NNW 08KT
PRES 915HPA
MXWD 105KT
GUST 150KT
GUST 150KT
GUST 140KT
PRES 925HPA
MXWD 100KT
GUST 140KT
96HF 120000UTC 31.6N 135.9E 170NM 70%
MOVE N 13KT
PRES 940HPA
MXWD 090KT
GUST 130KT
120HF 130000UTC 37.5N 142.5E 240NM 70%
MOVE NE 20KT
PRES 980HPA
MXWD 060KT

(2) RSMC Guidance for Forecast by GSM (FXPQ20-25 RJTD)

FXPQ i i RJTD YYGGgg RSMC GUIDANCE FOR FORECAST

NAME -1-- 4- N- ---- (-----

<u>NAME</u> class ty-No. name (common-No.) <u>PSTN</u> YYGGgg <u>UTC</u> LaLa.La N LoLoLo.Lo E (or W)

<u>PRES</u> PPPP <u>HPA</u>

GUST 085KT =

MXWD WWW KT

FORECAST BY GLOBAL MODEL

<u>MXW</u>D PRES TIME <u>PSTN</u>

(CHANGE FROM T=0)

T=006 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=012 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=018 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

<u>T=132</u> LaLa.La N LoLoLo.Lo E (or W) appp <u>HPA</u> awww <u>KT=</u>

Notes:

Underlined parts are fixed.

Symbolic letters

'20', '21', '22', '23', '24' or '25' YYGGgg Initial time of the model in UTC

class Intensity classification of the tropical cyclone 'T', 'STS', 'TS' or 'TD'

PPPP Central pressure in hPa WWW Maximum wind speed in knots a Sign of ppp and www (+, - or blank)

Absolute value of change in central pressure from T=0, in hPa ppp Absolute value of change in maximum wind speed from T=0, in knots www

Example:

FXPQ20 RJTD 180600

RSMC GUIDANCE FOR FORECAST NAME TY 00017D 15 COUNTY (0001)

PSTN 180000UTC 15.2N 126.3E

PRES 905HPA MXWD 105KT

FORECAST BY GLOBAL MODEL

PRES MXWD (CHANGE FROM T=0) TIME PSTN

T=006 15.4N 125.8E +018HPA -008KT

T=012 15.5N 125.6E +011HPA -011KT T=018 15.8N 125.7E +027HPA -028KT

T=132 20.7N 128.8E +021HPA -022KT=

(3) RSMC Guidance for Forecast by GEPS (FXPQ30-35 RJTD)

FXPQii RJTD YYGGgg

RSMC GUIDANCE FOR FORECAST

NAME class ty-No. name (common-No.)

PSTN YYGGgg UTC LaLa.La N LoLoLo.Lo E (or W)

PRES PPPP HPA

MXWD WWW KT

FORECAST BY GLOBAL ENSEMBLE PREDICTION SYSTEM

TIME **PSTN** PRES MXWD

(CHANGE FROM T=0)

T=006 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=012 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=018 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=132 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT=

Notes:

a. <u>Underlined</u> parts are fixed.

b. Symbolic letters

'30', '31', '32', '33', '34' or '35'

YYGGgg Initial time of the model in UTC

class Intensity classification of the tropical cyclone 'T', 'STS', 'TS' or 'TD'

PPPP Central pressure in hPa WWW Maximum wind speed in knots Sign of ppp and www (+, - or blank)

Absolute value of change in central pressure from T=0, in hPa ppp www Absolute value of change in maximum wind speed from T=0, in knots

Example:

FXPQ30 RJTD 231200 RSMC GUIDANCE FOR FORECAST NAME TY 1826 YUTU (1826) PSTN 231200UTC 12.0N 149.6E

PRES 965HPA MXWD 75KT

FORECAST BY GLOBAL ENSEMBLE PREDICTION SYSTEM

PRES MXWD (CHANGE FROM T=0) **PSTN** TIME T=006 12.7N 149.1E -002HPA +001KT T=012 13.2N 148.3E -001HPA +004KT T=018 13.8N 147.6E -005HPA +004KT

T=132 18.0N 129.9E -033HPA +030KT=

(4) RSMC Prognostic Reasoning (WTPQ30-35 RJTD)

Example:

WTPQ30 RJTD 231200 RSMC TROPICAL CYCLONE PROGNOSTIC REASONING REASONING NO.10 FOR TY 1826 YUTU (1826)

1.GENERAL COMMENTS

TY YUTU IS LOCATED AT 12.0N, 149.6E. INFORMATION ON THE CURRENT POSITION IS BASED ON ANIMATED MSI. POSITIONAL ACCURACY IS GOOD. THE SYSTEM IS IN A FAVORABLE ENVIRONMENT FOR DEVELOPMENT UNDER THE INFLUENCE OF HIGH SSTS, HIGH TCHP AND WEAK VWS. THIS HAS CAUSED THE SYSTEM TO DEVELOP OVER THE LAST SIX HOURS. HOWEVER, THE INFLUENCE OF DRY AIR IS UNFAVORABLE FOR SYSTEM DEVELOPMENT. INFORMATION ON CURRENT INTENSITY IS BASED ON DVORAK INTENSITY ANALYSES.

2.SYNOPTIC SITUATION

THE SYSTEM IS MOVING WESTWARD ALONG THE SOUTHERN PERIPHERY OF A MID-LEVEL SUB-TROPICAL HIGH. ANIMATED MSI SHOWS THE APPEARANCE OF AN EYE. WATER VAPOR IMAGERY SHOWS DRY AIR IN THE DIRECTION OF THE MOVEMENT. DMSP-F18/SSMIS 89 GHZ MICROWAVE IMAGERY SHOWS THE SYSTEM HAS A BAND WITH CURVATURE INDICATING THE CSC.

3.TRACK FORECAST

THE SYSTEM WILL MOVE NORTHWESTWARD ALONG THE PERIPHERY OF A MID-LEVEL SUB-TROPICAL HIGH UNTIL FT12. THE SYSTEM WILL THEN MOVE WEST-NORTHWESTWARD ALONG THE PERIPHERY OF A MID-LEVEL SUB-TROPICAL HIGH UNTIL FT120. THE JMA TRACK FORECAST IS BASED ON GSM PREDICTIONS, AND REFERENCE TO OTHER NWP MODELS. JMA TRACK FORECAST CONFIDENCE IS FAIR UNTIL FT48 BUT LOW THEREAFTER DUE TO SIGNIFICANT DIFFERENCES AMONG NUMERICAL MODEL OUTPUTS.

4.INTENSITY FORECAST

THE SYSTEM WILL DEVELOP UNTIL FT48 DUE TO THE INFLUENCE OF INTERACTION WITH HIGH SSTS, HIGH TCHP, WEAK VWS AND GOOD UPPER LEVEL OUTFLOW. THE SYSTEM WILL THEN MAINTAIN ITS INTENSITY UNTIL FT72 DUE TO THE INFLUENCE OF INTERACTION WITH HIGH SSTS, HIGH TCHP AND DRY AIR. THE JMA INTENSITY FORECAST IS BASED ON GUIDANCE DATA. =

(5) RSMC Tropical Cyclone Best Track (AXPQ20 RJTD)

AXPQ20 RJTD YYGGgg

RSMC TROPICAL CYCLONE BEST TRACK

NAME ty-No. name (common-No.)

PERIOD FROM MMMDDTTUTC TO MMMDDTTUTC

DDTT LaLa.LaN LoLoLo.LoE PPP<u>HPA</u> WWW<u>KT</u> DDTT LaLa.LaN LoLoLo.LoE PPP<u>HPA</u> WWW<u>KT</u> DDTT LaLa.LaN LoLoLo.LoE PPP \underline{HPA} WWW \underline{KT} DDTT LaLa.LaN LoLoLo.LoE PPPHPA WWWKT

DDTT LaLa.LaN LoLoLo.LoE PPP<u>HPA</u> WWW<u>KT</u> DDTT LaLa.LaN LoLoLo.LoE PPP<u>HPA</u> WWW<u>KT</u>

REMARKS1)

TD FORMATION AT MMMDDTT<u>UTC</u> FROM TD TO TS AT MMMDDTTUTC

DISSIPATION AT MMMDDTT<u>UTC=</u>

Notes:

- Underlined parts are fixed.
- 1) REMARKS is given optionally.
- c. Symbolic letters

MMM Month in UTC given such as 'JAN' and 'FEB'

DD Date in UTC TT Hour in UTC PPP Central pressure WWW : Maximum wind speed

Example:

AXPQ20 RJTD 020600

RSMC TROPICAL CYCLONE BEST TRACK
NAME 0001 DAMREY (0001)
PERIOD FROM OCT1300UTC TO OCT2618UTC
1300 10.8N 155.5E 1008HPA //KT 1306 10.9N 153.6E 1006HPA //KT
1312 11.1N 151.5E 1004HPA //KT 1318 11.5N 149.8E 1002HPA //KT
1400 11.9N 148.5E 1000HPA //KT 1406 12.0N 146.8E 998HPA 35KT

1712 14.6N 129.5E 905HPA 105KT 1718 14.7N 128.3E 905HPA 105KT

2612 32.6N 154.0E 1000HPA //KT 2618 33.8N 157.4E 1010HPA //KT

REMARKS

TD FORMATION FROM TD TO TS FROM TS TO ST AT OCT1300UTC TO TS TO STS AT OCT1406UTC AT OCT1512UTC FROM STS TO TY FROM TY TO STS AT OCT1600UTC TO STS AT OCT2100UTC FROM STS TO TS FROM TS TO L AT OCT2112UTC AT OCT2506UTC DISSIPATION AT OCT2700UTC=

(6) Tropical Cyclone Advisory for SIGMET (FKPQ30-35 RJTD)

FKPQ i i RJTD YYGGgg

TC ADVISORY

DTG: yyyymmdd/time Z

TCAC: **TOKYO** TC: name NR: number

PSN: N LaLa.LaLa E LoLoLo.LoLo

MOV: direction SpSpSp KT

PPPP HPA <u>C:</u> MAX WIND: WWW KT

FCST PSN +6HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo*

FCST MAX WIND +6HR: WWW KT*

FCST PSN +12HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo

FCST MAX WIND +12HR: WWW KT

FCST PSN +18HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo* FCST MAX WIND +18HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo* FCST PSN +24HR: YY/GGgg Z N LaLa.LaLa E LoLoLo.LoLo

FCST MAX WIND +24HR: WWW KT RMK: NIL =

NXT MSG: yyyymmdd/time \underline{Z}

Notes:

Underlined parts are fixed.

Abbreviations

DTG Date and time

TCAC Tropical Cyclone Advisory Centre

TC Tropical Cyclone

NR Number PSN Position MOV Movement C Central pressure MAX WIND Maximum wind **FCST** Forecast RMK Remarks NXT MSG Next message

c. Symbolic letters

'30', '31', '32', '33', '34' or '35' ii

Date(YY), hour(GG) and minute(gg) in UTC (Using "Z") YYGGgg

Year(yyyy), month(mm), date(dd), hour and minute (time) in UTC (Using "Z") yyyymmdd/time Name assigned to the tropical cyclone by RSMC Tokyo-Typhoon Center name

Advisory number (starting with "01" for each cyclone) Number

LaLa.LaLa Latitude of the center position LoLoLo.LoLo Longitude of the center position

Direction of movement given in 16 azimuthal direction such as 'N', 'NNE', 'NE' and 'ENE' direction

Speed of movement. "SLW" for less than 3 kt "STNR" for less than 1 kt. SpSpSp

PPPP Central pressure

WWW Maximum sustained wind

Example:

FKPQ30 RJTD 271200

TC ADVISORY DTG: 20080927/1200Z TCAC: TC: TOKYO JANGMI NR: 15 N2120 E12425 PSN: NW 13KT MOV: 910HPA

115KT 27/1800Z N2200 E12330

C: MAX WIND: FCST PSN +6HR: FCST MAX WIND +6HR: FCST PSN +12HR: FCST MAX WIND +12HR: FCST PSN +18HR: FCST MAX WIND +18HR: FCST PSN +24HR: FCST MAX WIND +24HR: RMK: 115KT 28/0000Z N2240 E12250

115KT 28/0600Z N2340 E12205 95KT

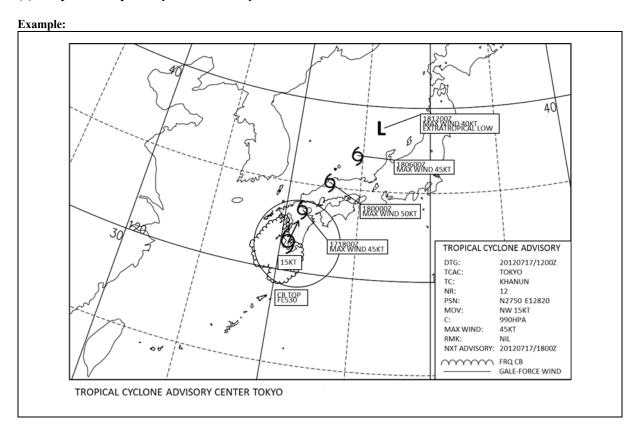
28/1200Z N2440 E12105

80KT RMK: NIL.

NXT MSG: 20080927/1800Z =

^{* 6} hour and 18 hour forecasts are added from 22 May 2008.

(7) Graphical Tropical Cyclone Advisory for SIGMET



Appendix 7 Specifications of JMA's NWP Models (GSM, GEPS)

The Global Spectral Model (GSM) and the Global Ensemble Prediction System (GEPS) are used in JMA as a primary basis for TC forecasts. The general specifications of GSM and GEPS are summarized in Table A7.1.

Table A7.1 Specifications of GSM and GEPS

NWP Models	GSM (Global Spectral Model),	GEPS (Global Ensemble			
	TQ959L128	Prediction System), TQ479L128			
Resolution	13 km, 128 layers (Top: 0.01 hPa)	27 km, 128 layers (Top: 0.01 hPa)			
Area	Global	Global			
Method for	Global Data Assimilation System	Unperturbed condition: Truncated			
initial value	(Hybrid-4DVAR)	GSM initial condition			
	Outer resolution: TQ959L128	Initial perturbation: LETKF-based			
	Inner resolution: TL319L128	perturbation and SV-based			
	Window: Init-3h to Init + 3h	perturbation			
		Ensemble size: 51 (50 perturbed			
		members and 1 control member)			
		SV target areas: Northern			
		Hemisphere (30 – 90°N), Tropics			
		$(30^{\circ}S - 30^{\circ}N)$, Southern			
		Hemisphere (90 – 30°S)			
Forecast length	264 hours (00, 12 UTC)	432 hours (12 UTC)			
(initial times)	132 hours (06, 18 UTC)	264 hours (00, UTC)			
		132 hours (06, 18 UTC)			
Operational	14 March 2022	` ' '			
Operational as	14 March 2023	14 March 2023			
from					

GSM (TQ959L128) has a horizontal resolution of approximately 13 km and 128 vertical layers. Details of the model can be found in JMA (2025) and Yonehara et al. (2023).

GEPS (TQ479L128) is an ensemble prediction system used for TC track forecasts up to five days ahead, one-week forecasts, early warning information on extreme weather, and one-month forecasts. It has 51 members and a horizontal resolution of approximately 27 km along with 128 vertical layers for the first 18 days of forecasts. Details of the system can be found in JMA (2025) and Ota et al. (2023). A combination of a Local Ensemble Transform Kalman Filter (LETKF; Hunt et al. 2007) and a singular vector (SV) method (Buizza and Palmer 1995) is employed for the initial perturbation setup. In addition, a stochastically perturbed physics tendency scheme (Buizza et al. 1999) is incorporated in consideration of model uncertainties associated with physical parameterizations, and a perturbation technique for sea surface temperature (SST) is incorporated to represent uncertainty in the prescribed SST.

[Recent upgrades to GSM, Global Data Assimilation System and GEPS] Global Data Assimilation System:

- Assimilation of the ATMS and Cross-track Infrared Sounder (CrIS) data from NOAA-21 was started (March 2024)

[References]

- Buizza, R., M. Miller, and T. N. Palmer, 1999: Stochastic representation of model uncertainties in the ECMWF Ensemble Prediction System. *Quart. J. Roy. Meteor. Soc.*, **125**, 2887–2908.
- Buizza, R. and T. N. Palmer, 1995: The singular-vector structure of the atmospheric global circulation. *J. Atmos. Sci.*, **52**, 1434 1456.
- Hunt, B. R., E. J. Kostelich and I. Szunyogh, 2007: Efficient data assimilation for spatiotemporal chaos: a local ensemble transform Kalman filter. *Physica. D.*, **230**, 112 126.
- Japan Meteorological Agency, 2025: Outline of the Operational Numerical Weather Prediction at the Japan Meteorological Agency. *Japan Meteorological Agency, Tokyo, Japan.*
- Ota, Y., J. Chiba, Y. Ichikawa, H. Oashi, T. Takakura and H. Yamaguchi, 2023: Upgrade of JMA's Global Ensemble Prediction System. *WGNE Res. Activ. Earth system Modell.*, **53**, 06.11-12.
- Yonehara, H., Y. Kuroki, M. Ujiie, C. Matsukawa, T. Kanehama, R. Nagasawa, K. Ochi, M. Higuchi, Y. Ichikawa, R. Sekiguchi and S. Hirahara, 2023: Upgrade of JMA's Operational Global Numerical Weather Prediction System. *WGNE Res. Activ. Earth system Modell.*, **53**, 06.15-16.

Appendix 8 Products on WIS GISC Tokyo Server

(Available at https://www.wis-jma.go.jp/cms/)

NWP products (GSM and GEPS with GRIB formatted data)

Model	GSM	GSM	GSM
Area and resolution	Whole globe, 1.25°×1.25°	20°S–60°N, 60°E–160°W 1.25°×1.25°	Whole globe, 2.5°×2.5°
Levels and elements	10 hPa: Z, U, V, T 20 hPa: Z, U, V, T 30 hPa: Z, U, V, T 50 hPa: Z, U, V, T 70 hPa: Z, U, V, T 100 hPa: Z, U, V, T 150 hPa: Z, U, V, T 200 hPa: Z, U, V, T 200 hPa: Z, U, V, T, Ψ, χ 250 hPa: Z, U, V, T, H, ω 400 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 700 hPa: Z, U, V, T, H, ω 700 hPa: Z, U, V, T, H, ω 850 hPa: Z, U, V, T, H, ω 925 hPa: Z, U, V, T, H, ω 1000 hPa: Z, U, V, T, H, ω Surface: P, U, V, T, H, R†	10 hPa: Z, U, V, T 20 hPa: Z, U, V, T 30 hPa: Z, U, V, T 50 hPa: Z, U, V, T 70 hPa: Z, U, V, T 100 hPa: Z, U, V, T 150 hPa: Z, U, V, T 200 hPa: Z, U, V, T 200 hPa: Z, U, V, T 300 hPa: Z, U, V, T 300 hPa: Z, U, V, T, D 400 hPa: Z, U, V, T, D 500 hPa: Z, U, V, T, D 500 hPa: Z, U, V, T, D 500 hPa: Z, U, V, T, D, ω 850 hPa: Z, U, V, T, D, ω 850 hPa: Z, U, V, T, D, ω 1000 hPa: Z, U, V, T, D, ω 1000 hPa: Z, U, V, T, D Surface: P, U, V, T, D	10 hPa: Z*, U*, V*, T* 20 hPa: Z*, U*, V*, T* 30 hPa: Z°, U°, V°, T° 50 hPa: Z°, U°, V°, T° 70 hPa: Z°, U°, V°, T° 100 hPa: Z°, U°, V°, T° 150 hPa: Z*, U*, V*, T* 200 hPa: Z, U, V, T 250 hPa: Z°, U°, V°, T° 300 hPa: Z, U, V, T, D*‡ 400 hPa: Z, U, V, T, D*‡ 700 hPa: Z, U, V, T, D*‡ 850 hPa: Z, U, V, T, D 850 hPa: Z, U, V, T, D 850 hPa: Z, U, V, T, D 1000 hPa: Z, U*, V*, T*, D*‡ Surface: P, U, V, T, D*‡
Forecast hours	0–84 every 6 hours and 96–192 every 12 hours for 12 UTC initial † Except analysis	0–84 every 6 hours § 96–192 every 24 hours for 12 UTC initial ¶ 90–192 every 6 hours for 12 UTC initial	0–72 every 24 hours and 96–192 every 24 hours for 12 UTC initial ° 0–120 for 12 UTC initial † Except analysis * Analysis only
Initial times	00, 06, 12 and 18 UTC	00, 06, 12 and 18 UTC	00 UTC and 12 UTC ‡ 00 UTC only

Model	GEPS
Area and resolution	Whole globe, 2.5°×2.5°
Levels and elements	250 hPa: μU, σU, μV, σV 500 hPa: μZ, σZ 850 hPa: μU, σU, μV, σV, μT, σT 1000 hPa: μZ, σZ Surface: μP, σP
Forecast hours	0–192 every 12 hours
Initial times	00 and 12 UTC

NWP products (GSM and GEPS with GRIB2 formatted data)

Model	GSM	GSM	GSM
Area and resolution	5S-90N and 30E-165W, Whole globe 0.25° × 0.25°	5S-90N and 30E-165W, Whole globe 0.5° × 0.5°	Whole globe 1.25° × 1.25°
Levels and elements	Surface: U, V, T, H, P, Ps, R, Cla, Clh, Clm, Cll	10 hPa: Z, U, V, T, H, ω 20 hPa: Z, U, V, T, H, ω 30 hPa: Z, U, V, T, H, ω 50 hPa: Z, U, V, T, H, ω 70 hPa: Z, U, V, T, H, ω 100 hPa: Z, U, V, T, H, ω 150 hPa: Z, U, V, T, H, ω 200 hPa: Z, U, V, T, H, ω 200 hPa: Z, U, V, T, H, ω 300 hPa: Z, U, V, T, H, ω 400 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 700 hPa: Z, U, V, T, H, ω 800 hPa: Z, U, V, T, H, ω 800 hPa: Z, U, V, T, H, ω 900 hPa: Z, U, V, T, H, ω 925 hPa: Z, U, V, T, H, ω 925 hPa: Z, U, V, T, H, ω 975 hPa: Z, U, V, T, H, ω 975 hPa: Z, U, V, T, H, ω Surface: U, V, T, H, ρ, Ps, R, Cla, Clh, Clm, Cll	10 hPa: Z, U, V, T 20 hPa: Z, U, V, T 30 hPa: Z, U, V, T 50 hPa: Z, U, V, T 70 hPa: Z, U, V, T 100 hPa: Z, U, V, T 150 hPa: Z, U, V, T 200 hPa: Z, U, V, T, Ψ, χ 250 hPa: Z, U, V, T, Ψ, χ 250 hPa: Z, U, V, T, H, ω 400 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 700 hPa: Z, U, V, T, H, ω, ζ, δ 850 hPa: Z, U, V, T, H, ω, ζ, ∇ 850 hPa: Z, U, V, T, H, ω, ζ, ∇ 925 hPa: Z, U, V, T, H, ω, ζ, ∇ 1000 hPa: Z, U, V, T, H, ω, ζ, ∇
Forecast hours	0–132 every 3 hours 138–264 every 6 hours for 00 UTC and 12 UTC initial	0–132 every 3 hours 138–264 every 6 hours for 00 UTC and 12 UTC initial	0–132 every 3 hours 138–264 every 6 hours for 00 UTC and 12 UTC initial
Initial times	00, 06, 12 and 18 UTC	00, 06, 12 and 18 UTC	00, 06, 12 and 18 UTC

Model	GEPS
Area and resolution	Whole globe, 1.25°×1.25°
Levels and elements	250 hPa: μU, σU, μV, σV 500 hPa: μZ, σZ 850 hPa: μU, σU, μV, σV, μT, σT 1000 hPa: μZ, σZ Surface: μP, σP Probability of precipitation [1,5,10,25,50,100 mm/24hour], Probability of 10m sustained wind and gusts[10,15,25 m/s], Probability of temperature anomalies [±1, ±1.5, ±2σ]
Forecast hours	0-264 every 12 hours
Initial times	00 UTC and 12 UTC

Notes:	Z: geopotential height T: temperature ω: vertical velocity χ: velocity potential Ps: pressure	U: eastward wind D: dewpoint depression ζ: vorticity ∇: divergence R: rainfall	V: northward wind H: relative humidity ψ: stream function P: sea level pressure Cla: total cloudiness
	±		
	City along the angle (layer layer)	Clm: cloudiness (middle laye	r)

Cll: cloudiness (lower layer)

The prefixes μ and σ represent the average and standard deviation of ensemble prediction results respectively. The symbols °, *, ¶, §, ‡ and † indicate limitations on forecast hours or initial time as shown in the tables.

Other products

Data	Contents / frequency (initial time)					
	High density atmospheric motion vectors (BUFR) Himawari-8/9 (VIS, IR, WVx3: every hour), 60S-60N, 90E-170W					
Satellite products	Clear Sky Radiance (CSR) data (BUFR)					
	Himawari-8/9 radiances and brightness temperatures					
	averaged over cloud-free pixels: every hour					
Tropical cyclone						
Information	• tropical cyclone analysis data (00, 06, 12 and 18 UTC)					
	Global Wave Model (GRIB2)					
	• significant wave height					
	prevailing wave period					
Wave data	wave direction					
	Forecast hours:					
	0–84 every 6 hours (00, 06 and 18UTC)					
	0–84 every 6 hours and 96-192 every 12 hours (12 UTC)					
	(a) Surface data (TAC/TDCF)					
Observational	SYNOP, SHIP, BUOY: Mostly 4 times a day					
data	(b) Upper-air data (TAC/TDCF)					
	TEMP (parts A-D), PILOT (parts A-D): Mostly twice a day					
	(a) Satellite imagery (SATAID)					
	Himawari-8/9					
	(b) Observation data (SATAID)					
SATAID service	SYNOP, SHIP, METAR, TEMP (A, B) and ASCAT sea-surface wind					
	(c) NWP products (SATAID)					
	GSM					
	(Available at https://www.wis-jma.go.jp/cms/sataid/)					

Appendix 9 Online RSMC Tokyo Products and Services

List of products provided on the Numerical Typhoon Prediction (NTP) website

Products	Frequency	Details
RSMC Advisor	ies	
RSMC TC Advisory	At least 8 times/day	The Center's TC analysis and forecasts up to 120 hours ahead (linked to the JMA website at https://www.jma.go.jp/bosai/map.html#contents=typhoon⟨=en)
Storm Wind Probability Map	4 times/day	Probabilistic forecast map for sustained wind of 50-kt or more for 1, 2, 3, 4 and 5 days ahead
Prognostic Reasoning	4 times/day	RSMC Tokyo Tropical Cyclone Prognostic Reasoning (WTPQ3X)
TC Advisory	4 times/day	TC Advisory in text, graphical and xml formats including the Center's TC analysis, track and intensity forecasts up to 24-hours and horizontal extents of cumulonimbus cloud and cloud top height associated with TCs potentially affecting aviation safety (linked to the Tropical Cyclone Advisory Center Tokyo Website)
Remote Sensing	3	
Satellite Analysis	At least 4 times/day	Results and historical logs of the Center's TC analysis conducted using satellite images (Conventional Dvorak analysis and Early-stage Dvorak analysis)
Satellite Imagery	Up to 142 times/day	Satellite imagery of Himawari-8/9 (linked to the JMA website at https://www.jma.go.jp/bosai/map.html#elem=ir⟨=en&contents=himawari)
Satellite Microwave Products		 TC snapshot images Warm-core-based TC intensity estimates Weighted consensus TC intensity estimates made using Dvorak analysis and satellite microwave warm-core-based intensity estimates
Sea-surface AMV (ASWind)	Every 10 / 30 minutes	AMV-based Sea-surface Wind in the vicinity of TC (linked to the Meteorological Satellite Center web site)
Radar Composite Imagery	Every hour	Radar composite imagery of the Typhoon Committee Regional Radar Network
Atmospheric Ci	rculation	
Weather Charts	4 times/day	Weather maps for surface analysis, 24- and 48-hour forecasts (linked to the JMA website at https://www.jma.go.jp/bosai/weather_map/#lang=en)
NWP Multi Center Weather Charts	Twice/day	 Mean sea level pressure and 500 hPa Geopotential height (up to 168 hours) of deterministic NWP models from nine centers (BoM, CMA, CMC, DWD, ECMWF, KMA, NCEP, UKMO and JMA)
JMA GSM Analysis and Forecast	4 times/day	 Upper-air analysis and forecast data based on JMA-GSM Streamlines at 850, 500 and 200 hPa Divergence at 200 hPa Velocity potential at 200 hPa Vertical Velocity in Pressure Coordinate at 500 hPa Dew Point Depression at 600 hPa Curvature Vorticity at 850 hPa Vertical wind shear between 200 and 850 hPa Sea Level Pressure Genesis Potential Index
MJO Phase Diagram	Daily	MJO phase and amplitude diagram MJO Hovmöller diagram (linked to the Tokyo Climate Center web site)

Products	Frequency	Details				
Asian Monsoon Monitoring Indices	Daily, only during Apr Oct.	• Time series of vertical wind shear, OLR and other indices associated with SW Asian Monsoon (linked to the Tokyo Climate Center web site)				
Ocean Conditi	on					
SST	Once/day	Sea surface temperature and related differences from 24 hours ago				
ТСНР	Once/day	Tropical cyclone heat potential and related differences from 24 hours ago				
Numerical TC Prediction						
Track Bulletin	4 times/day	RSMC Tokyo Tropical Cyclone Track Forecast Bulletin Track forecast by GSM (FXPQ2X) Track forecast by GEPS (FXPQ3X)				
TC intensity (TIFS monitor)	4 times/day	TC Intensity prediction of TIFS, LGEM, HAFS and GSM				
TC Track Prediction	4 times/day	 TC track prediction of deterministic NWP models from nine centers (BoM, CMA, CMC, DWD, ECMWF, KMA, NCEP, UKMO and JMA) TC track prediction of EPS models from four centers (ECMWF, NCEP, UKMO and JMA) 				
TC Activity Prediction	Twice/day	• Two- and five-day TC activity prediction maps based on EPS models from four centers (ECMWF, UKMO, NCEP and JMA) and a related consensus				
TC Verification	4 times/day	• Verification results of the Center's official forecasts as well as NWP model and guidance predictions.				
Marine Foreca	st					
Storm Surge Forecasts	4 times/day	 Distribution of storm surge for the Center TC track forecasts and probabilistic products (ensemble mean, maximum, third quartile, spread and exceeding probabilities) of storm surge EPS from GEPS ensemble members (up to 132 hours) Time-series storm surge forecast charts (plume diagrams, box plots and exceeding probabilities) for the Center TC track forecasts and 51 TC track forecasts from GEPS ensemble members (up to 132 hours) 				
Ocean Wave Forecasts	Twice/day	 Distribution maps for ensemble mean, maximum, probability of exceeding various thresholds and ensemble spread of wave height and period based on the Wave Ensemble System (WENS) (up to 264 hours) Time-series representations with box-and-whisker plots for wave height/period and probability of exceeding various wave height/period thresholds based on WENS (up to 264 hours) 				

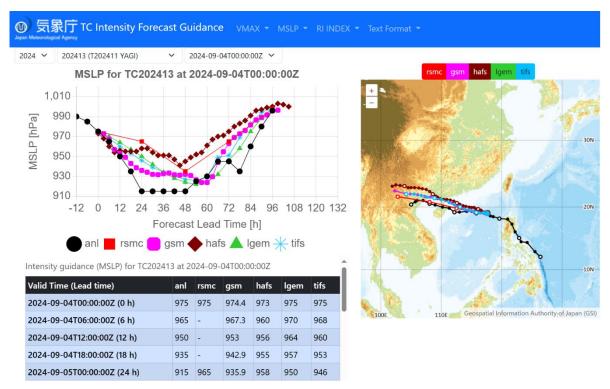
List of services provided on the TC communication platform

Services	Details
Early announcement ¹¹	Announcement of "upgrade is being consideration" prior to Advance notice from the Center *Supplemental information to RSMC advisories (It may not be provided in certain situations and should not be considered as an official RSMC advisory and/or its replacement)
Advance notice	Advance notice on TC status change from the Center *Supplemental information to RSMC advisories (It may not be provided in certain situations and should not be considered as an official RSMC advisory and/or its replacement)
Enhanced communication	A platform on which Committee Members can post inquiries or comments related to tropical cyclone analysis and forecasts

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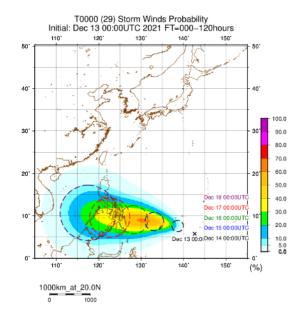
¹¹ This service started in 2025.

RSMC Tokyo - Typhoon Center product examples



Website on the TIFS (Typhoon Intensity Forecast scheme based on SHIPS) monitor

The upper figure shows TIFS, LGEM, HAFS and GSM intensity prediction values at each initial time for individual TCs with analysis data in line graphs as well as a map of tracks. The table shows intensity prediction values at each valid time with analysis data.



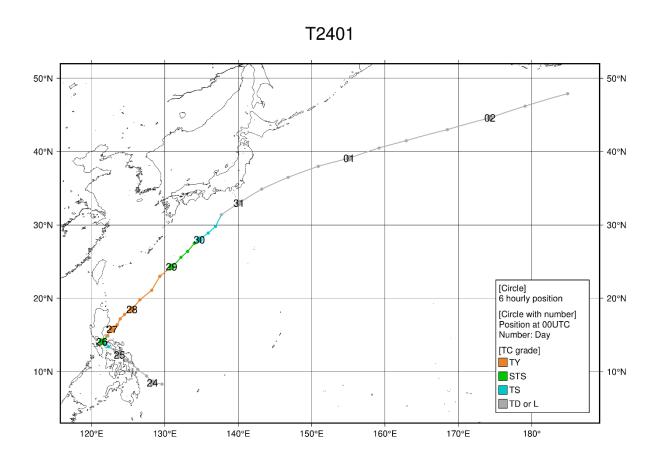
Five-day storm wind probability product (50 kt and above)

The figure shows spatial distribution of accumulated probability for the storm wind (equal to or above 50 kt) area associated with a selected TC up to a selected lead time on the calibrated levels of moderate (yellow), middle (red) and high (violet).

Appendix 10 Tropical Cyclones in 2024

EWINIAR (2401)

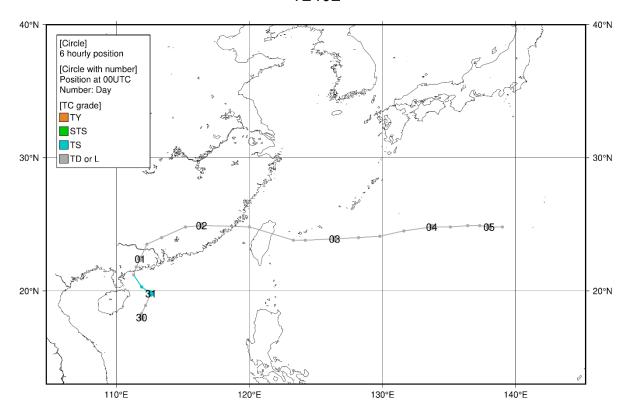
EWINIAR formed as a tropical depression (TD) over the sea east of Mindanao at 18 UTC on 23 May 2024 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the Philippines at 12 UTC on 25 May. It was further upgraded to severe tropical storm (STS) intensity in Luzon Island at 00 UTC on 26 May. After turning northeastward, it was upgraded to typhoon (TY) intensity over the Philippines 12 hours later. It reached its peak intensity with maximum sustained winds of 75 kt and a central pressure of 970 hPa over the same waters at 00 UTC on 27 May. It downgraded to STS intensity over the sea south of Japan at 00 UTC on 29 May and weakened to TS intensity at 00 UTC the next day. Keeping its northeastward track, it transitioned into an extratropical cyclone over the same waters 18 hours later. Further accelerating east-northeastward, it entered the sea south of the Aleutian Islands and crossed longitude 180 degrees east before 12 UTC on 2 June.



MALIKSI (2402)

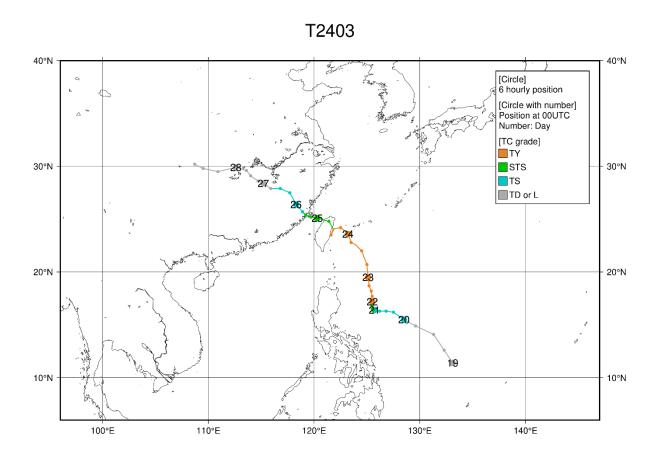
MALIKSI formed as a tropical depression (TD) over the South China Sea at 00 UTC on 30 May 2024 and moved northeastward. It was upgraded to tropical storm (TS) intensity, reached its peak intensity with maximum sustained winds of 35 kt and a central pressure of 998 hPa over the same waters at 00 UTC on 31 May and moved northwestward. It weakened to TD intensity over the same waters 12 hours later and then hit South China while moving northeastward. Moving eastward, it transitioned into an extratropical cyclone by 00 UTC on 2 June and then entered the East China Sea. Keeping its eastward track, it dissipated over the sea south of Japan at 12 UTC on 5 June.





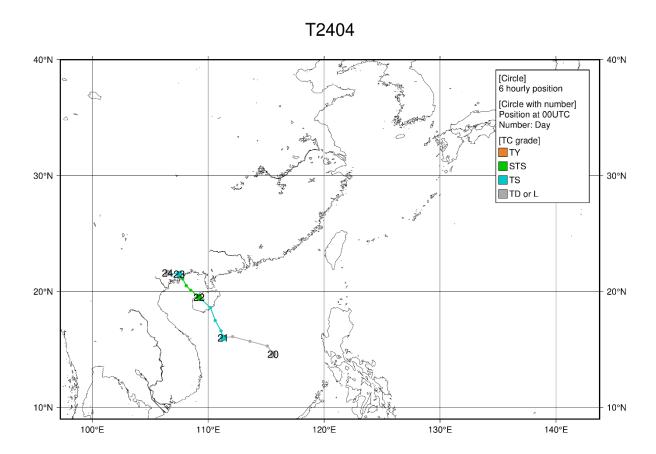
GAEMI (2403)

GAEMI formed as a tropical depression (TD) over the sea east of the Philippines at 00 UTC on 19 July 2024 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the same waters at 00 UTC the next day and moved westward. After turning northward, it was further upgraded to typhoon (TY) intensity over the same waters at 00 UTC on 22 July. It moved westward and reached its peak intensity with maximum sustained winds of 90 kt and a central pressure of 935 hPa south of Yonagunijima Island at 03 UTC on 24 July. Turning in a counterclockwise direction to circle over the sea east of Taiwan, it was downgraded to STS intensity at 15 UTC the same day. Moving westward, it hit Taiwan with STS intensity after 15UTC the same day and weakened rapidly. After passing through Taiwan Strait, it hit South China with STS intensity at 12 UTC on 25 July and downgraded to TS intensity in same area at 18 UTC the same day. Moving northwestwestward, it weakened to TD intensity in Central China at 18 UTC on 26 July and then dissipated at 00UTC on 29 July.



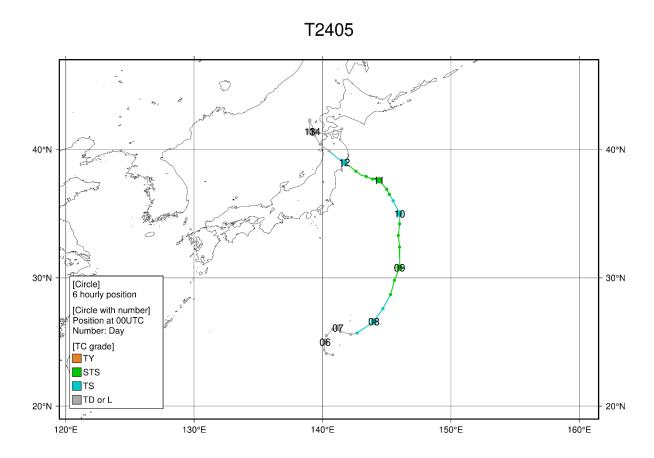
PRAPIROON (2404)

PRAPIROON formed as a tropical depression (TD) over the South China Sea at 00 UTC on 20 July 2024 and moved northwestward, then west-northwestward. It was upgraded to tropical storm (TS) intensity at 00 UTC the next day over the same waters and moved north-northwestward. It crossed Hainan Island with TS intensity around 18 UTC on 21 July and was upgraded to severe tropical storm (STS) intensity six hours later. After entering the Gulf of Tonkin, it reached its peak intensity with maximum sustained winds of 55 kt and a central pressure of 985 hPa at 06 UTC on 22 July. It hit Viet Nam before 00 UTC on 23 July, weakened to TD intensity 12 hours later and then moved westward. After turning in a clockwise direction to circle, it entered the Gulf of Tonkin by 00UTC on 25 July again and then dissipated.



MARIA (2405)

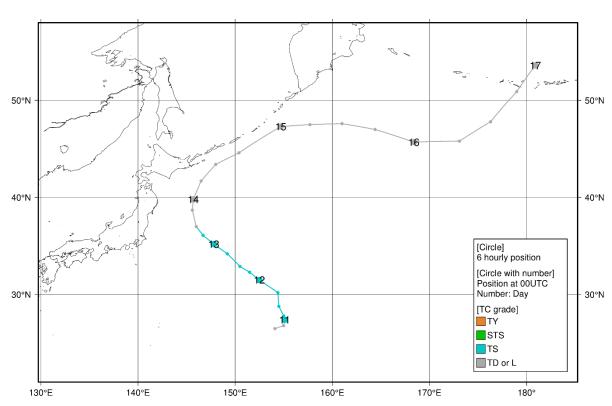
MARIA formed as a tropical depression (TD) over the sea around the Ogasawara Islands at 06 UTC on 5 August 2024 and moved northwestward. After it gradually turned eastward, it was upgraded to tropical storm (TS) intensity over the same waters at 18 UTC on 7 August and moved northeastward. It was further upgraded to severe tropical storm (STS) intensity at 12 UTC the next day and reached its peak intensity with maximum sustained winds of 55 kt and a central pressure of 980 hPa over the same waters six hours later, as moving northward. After it gradually turned northwestward, it made landfall near Ofunato city, Iwate Prefecture with STS intensity around 2330 UTC on 11 August. Crossing Honshu Island, it weakened to TD intensity at 06 UTC the next day and then entered the Sea of Japan. It slowly moved northward, passed through the Tsugaru Strait and dissipated over the waters south of Hokkaido Island at 18 UTC on 14 August.



SON-TINH (2406)

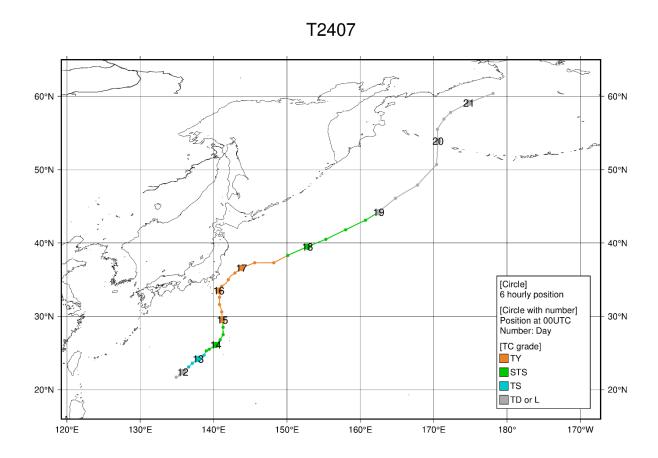
SON-TINH formed as a tropical depression (TD) over the sea north of Minamitorishima Island at 12 UTC on 10 August 2024 and moved northeastward. It was upgraded to tropical storm (TS) intensity at 00 UTC the next day and reached its peak intensity with maximum sustained winds of 40 kt and a central pressure of 994 hPa over the same waters 12 hours later, as moving northwestward. It weakened to TD intensity over the sea east of Japan at 12 UTC on 13 August and gradually accelerated northeastward. Maintaining its northeastward track, it transformed into an extratropical cyclone over the sea around the Kuril Islands by 00 UTC on 15 August and then turned eastward. After it turned northeastward toward the sea around the Aleutian Islands, it crossed longitude 180 degrees east before 00 UTC on 17 August.





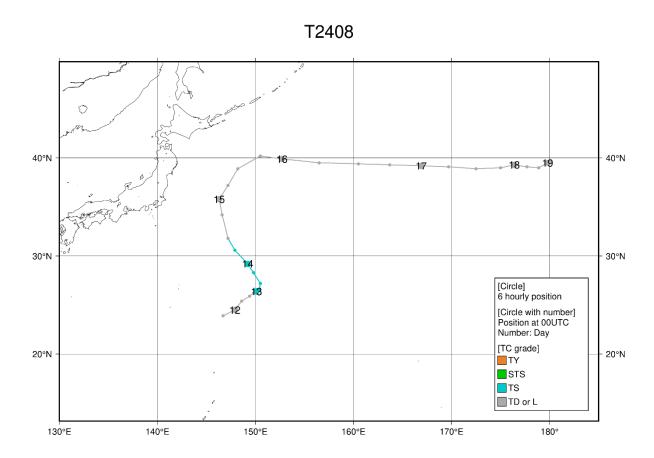
AMPIL (2407)

AMPIL formed as a tropical depression (TD) over the sea south of Japan at 12 UTC on 11 August 2024 and moved northeastward. It was upgraded to tropical storm (TS) intensity over the same waters at 12 UTC on 12 August. After turning northward, it was further upgraded to typhoon (TY) intensity over the sea around the Ogasawara Islands at 00 UTC on 15 August. Keeping its northward track, it reached its peak intensity with maximum sustained winds of 85 kt and a central pressure of 950 hPa over the sea east of Japan 12 hours later. Moving northeastward, it was downgraded to severe tropical storm (STS) intensity over the same waters at 18 UTC on 17 August and transitioned into an extratropical cyclone over the sea east of the Kuril Islands by 00 UTC on 19 August. After moving northward and entering the Bering Sea, it turned northeastward and then crossed latitude 60 degrees north before 06 UTC on 21 August.



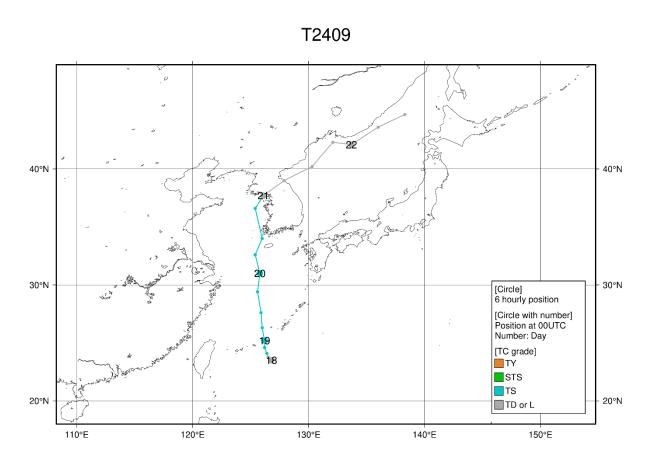
WUKONG (2408)

WUKONG formed as a tropical depression (TD) over the sea east of the Ogasawara Islands at 18 UTC on 11 August 2024 and moved northeastward. It was upgraded to tropical storm (TS) intensity and reached its peak intensity with maximum sustained winds of 35 kt and a central pressure of 1002 hPa over the sea northwest of Minamitorishima Island at 00 UTC on 13 August. After it turned northwestward, it weakened to TD intensity over the sea east of Japan at 12 UTC on 14 August and gradually turned eastward. Maintaining its eastward track, it transformed into an extratropical cyclone over the sea far off east of Japan by 12 UTC on 16 August. After entering the sea south of Aleutians, it crossed longitude 180 degrees east before 06 UTC on 19 August.



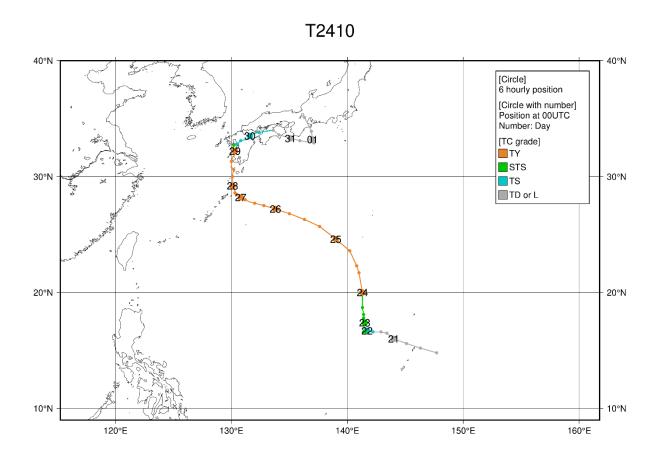
JONGDARI (2409)

JONGDARI formed as a tropical depression (TD) over the sea south of Okinawa at 00 UTC on 18 August 2024 and moved northward. It was upgraded to tropical storm (TS) intensity over the same waters 12 hours later. Keeping its northward track and moving to the East China Sea, it reached its peak intensity with maximum sustained winds of 40 kt and a central pressure of 996 hPa over the same waters at 06 UTC on 19 August. It entered the Yellow Sea, turned northeastward and then weakened to TD intensity over the waters near the western coast of the Korean Peninsula at 00 UTC on 21 August. After crossing the Korean Peninsula and entering the Sea of Japan, it transitioned into an extratropical cyclone by 00 UTC on 22 August and dissipated over the same waters 18 hours later.



SHANSHAN (2410)

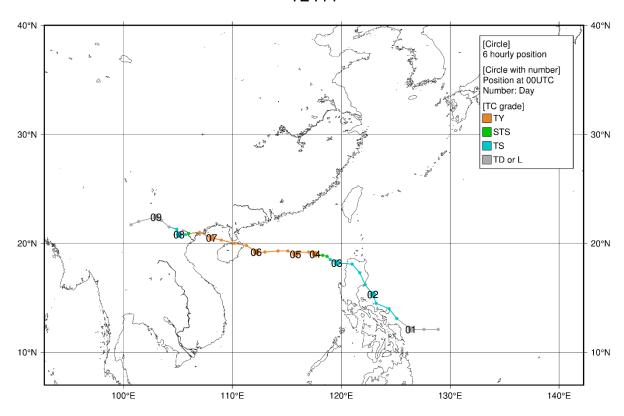
SHANSHAN formed as a tropical depression (TD) around the Mariana Islands at 06 UTC on 20 August 2024 and moved westward. It was upgraded to tropical storm (TS) intensity over the same waters at 18 UTC on 21 August. After turning sharply northward, it was further upgraded to typhoon (TY) intensity around the Ogasawara Islands at 00 UTC on 24 August. Turning northwestward, it reached its peak intensity with maximum sustained winds of 95 kt and a central pressure of 935 hPa northeast of Amami-Oshima Island at 15 UTC on 27 August. Moving northward and gradually turning northeastward, it made landfall near Satsumasendai city, Kagoshima Prefecture with TY intensity around 23 UTC on 28 August. After making landfall, it weakened rapidly and was downgraded to severe tropical storm (STS) intensity over Kyushu Island at 06 UTC on 29 August and to TS intensity six hours later. It moved eastward and then weakened to TD intensity over Shikoku Island at 12 UTC on 30 August. After moving to the sea south of Japan with its southeast track, it turned northward sharply and then dissipated in Honshu Island at 18 UTC on 1 September.



YAGI (2411)

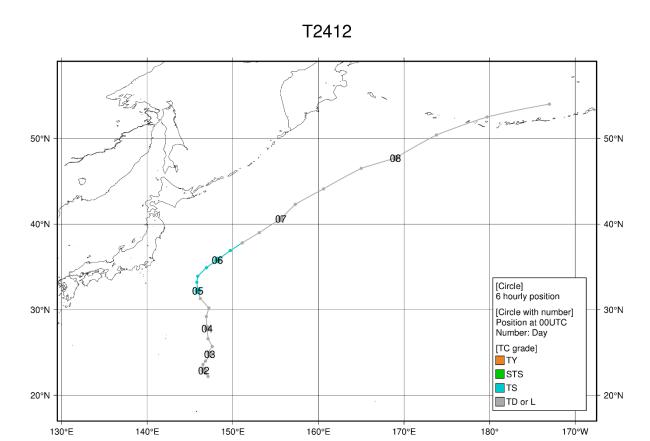
YAGI formed as a tropical depression (TD) over the sea east of the Philippines at 12 UTC on 31 August 2024 and moved westward. Turning northwestward, it was upgraded to tropical storm (TS) intensity over the same waters at 06 UTC on 1 September. After crossing north of Luzon Island and turning westward, it was further upgraded to typhoon (TY) intensity over the South China Sea at 00 UTC on 4 September. It developed rapidly and reached its peak intensity with maximum sustained winds of 105 kt and a central pressure of 915 hPa over the same waters at 00 UTC on 5 September. After crossing Hainan Island, it entered the Gulf of Tonkin and hit Northern Viet Nam with TY intensity around 06 UTC on 7 September. As it moved westward in the area, it was downgraded to TS intensity 12 hours later and weakened to TD intensity at 12 UTC on 8 September. It dissipated in Southwestern China at 18 UTC on 9 September.





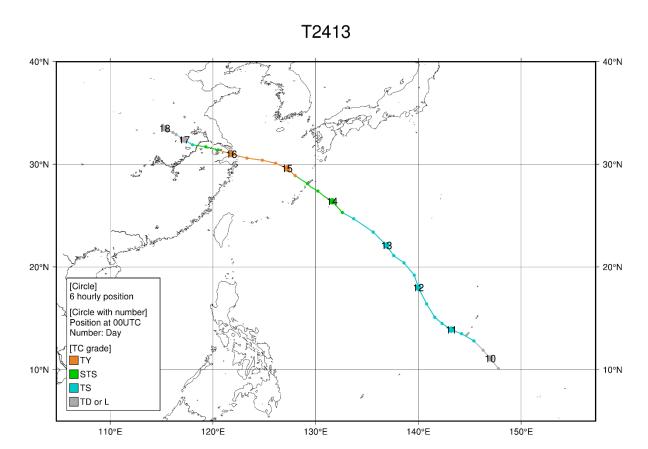
LEEPI (2412)

LEEPI formed as a tropical depression (TD) around the Ogasawara Islands at 12 UTC on 1 September 2024 and moved northwestward. While moving northward, it was upgraded to tropical storm (TS) intensity and reached its peak intensity with maximum sustained winds of 35 kt and a central pressure of 1002 hPa over the sea east of Japan at 00 UTC on 5 September. After turning northeastward, it weakened to TD intensity over the same waters at 12 UTC on 6 September and transitioned into an extratropical cyclone over the sea far off east of Japan by 00 UTC on 7 September. It kept its northeastward track and then crossed longitude 180 degrees east before 18 UTC on 8 September.



BEBINCA (2413)

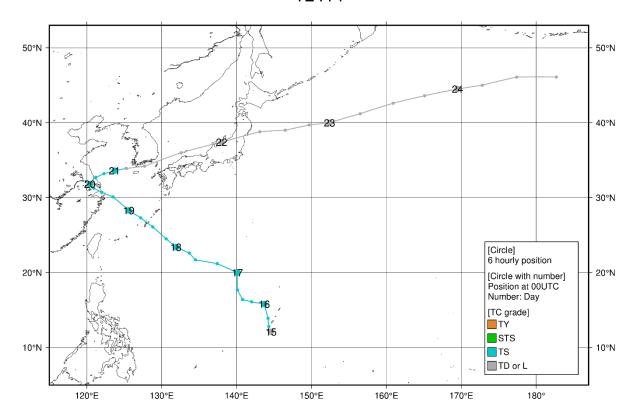
BEBINCA formed as a tropical depression (TD) over the sea around the Mariana Islands at 18 UTC on 9 September 2024 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the same waters 18 hours later and moved to the sea south of Japan while keeping its northwestward track. After passing around Amami-Oshima Island, it was upgraded to typhoon (TY) intensity over the East China Sea at 18 UTC on 14 September and reached its peak intensity with maximum sustained winds of 75 kt and a central pressure of 965 hPa over the same waters six hours later. Keeping its northwestward track, it hit Central China with TY intensity around 00 UTC on 16 September and was downgraded to TS intensity 18 hours later. It weakened to TD intensity there at 00 UTC on 17 September and dissipated in North China at 12 UTC on 18 September.



PULASAN (2414)

PULASAN formed as a tropical depression (TD) around the Mariana Islands at 00 UTC on 15 September 2024 and moved northward. It was upgraded to tropical storm (TS) intensity over the same waters 12 hours later and reached its peak intensity with maximum sustained winds of 45 kt and a central pressure of 992 hPa around the Ogasawara Islands at 00 UTC on 17 September. After turning northwestward, it crossed Okinawa Island after 12 UTC on 18 September and hit Central China around 12 UTC on 19 September. After it turned northeastward, it entered the Yellow Sea around 12 UTC on 20 September and transitioned into an extratropical cyclone by 06 UTC the next day. Keeping its northeastward track, it crossed the northern part of Honshu Island around 00 UTC on 22 September. After entering the sea south of the Aleutian Islands, it crossed longitude 180 degrees east before 18UTC on 24 September.

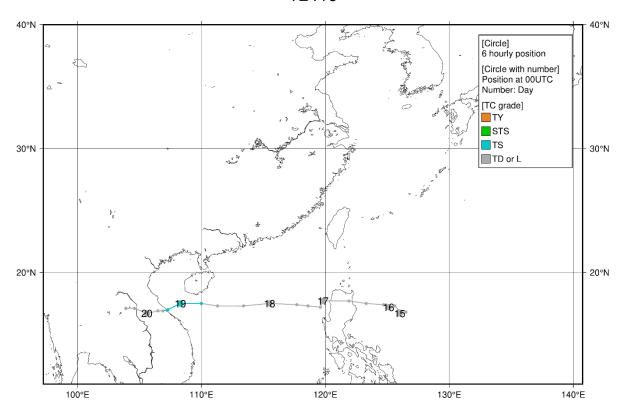




SOULIK (2415)

SOULIK formed as a tropical depression (TD) over the sea east of the Philippines at 00 UTC on 15 September 2024 and moved eastward. It turned westward sharply and crossed north of Luzon Island. After moving southward over the sea west of the island and turning westward again, it was upgraded to tropical storm (TS) intensity and reached its peak intensity with maximum sustained winds of 35 kt and a central pressure of 992 hPa over the South China Sea at 18 UTC on 18 September. Moving westward through the Gulf of Tonkin, it hit Viet Nam with TS intensity and was weakened to TD intensity at 12 UTC on 19 September. It dissipated in Northeast Thailand at 18 UTC the next day.

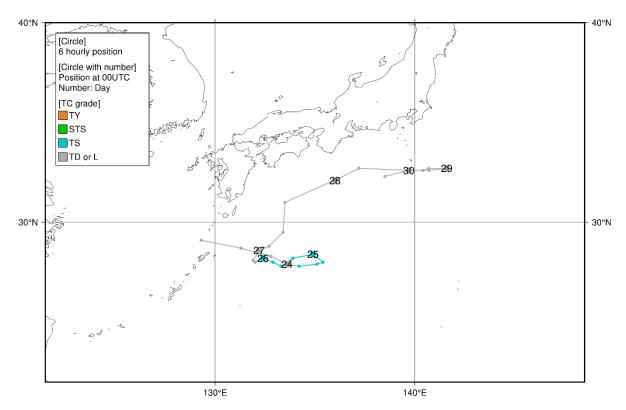




CIMARON (2416)

CIMARON formed as a tropical depression (TD) north of Amami-Oshima Island at 06 UTC on 23 September 2024 and moved southeastward. Moving eastward, it was upgraded to tropical storm (TS) intensity over the sea south of Japan at 06 UTC the next day and reached its peak intensity with maximum sustained winds of 35 kt and a central pressure of 998 hPa six hours later. After it turned in a counterclockwise direction to circle, it moved westward and weakened to TD intensity over the same waters at 06 UTC on 26 September. It turned northeastward and then transitioned into an extratropical cyclone over the same waters by 18 UTC on 27 September. After it gradually turned eastward, it moved to the sea east of Japan by 18 UTC on 28 September. After turning in a counterclockwise direction to circle over the same waters around 00 UTC on 29 September, it moved westward and dissipated over the sea south of Japan at 12 UTC on 30 September.

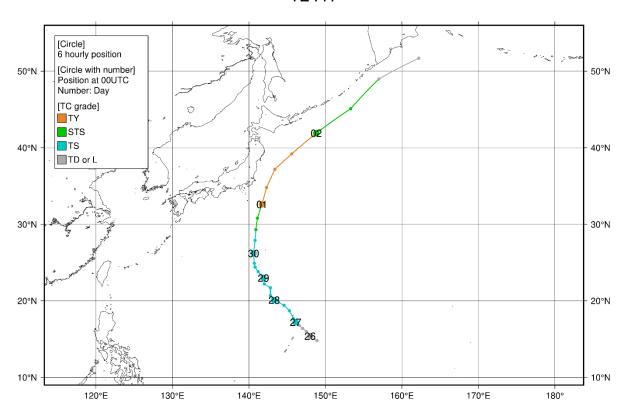




JEBI (2417)

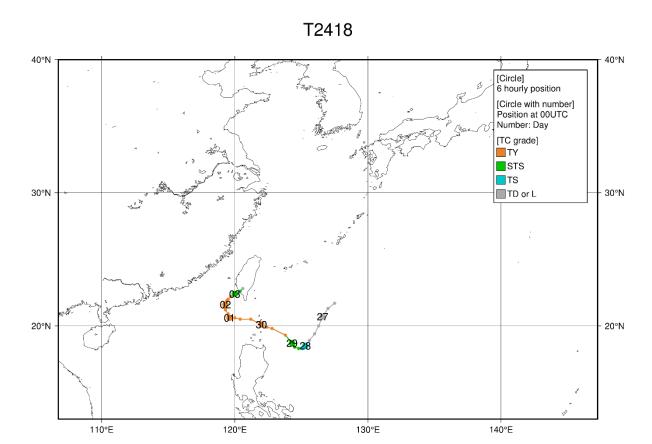
JEBI formed as a tropical depression (TD) over the sea around the Mariana Islands at 18 UTC on 25 September 2024 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the same waters at 00 UTC on 27 September. After gradually turning northward around the Ogasawara Islands, it was upgraded to severe tropical storm (STS) intensity over the same waters at 12 UTC on 30 September. It was further upgraded to typhoon (TY) intensity and reached its peak intensity with maximum sustained winds of 65 kt and a central pressure of 980 hPa over the sea east of Japan at 00 UTC on 1 October. It moved northeastward and was downgraded to STS intensity over the same waters at 00 UTC the next day. It transitioned into an extratropical cyclone over the sea around the Kuril Islands by 12 UTC on 2 October and dissipated over the sea east of the Kamchatka Peninsula 12 hours later.





KRATHON (2418)

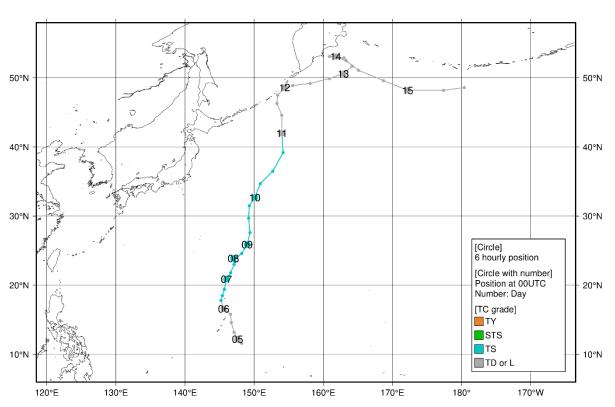
KRATHON formed as a tropical depression (TD) south of Okinawa at 12 UTC on 26 September 2024 and moved southwestward. Keeping its southwestward track, it was upgraded to tropical storm (TS) intensity east of the Philippines at 00 UTC on 28 September and then moved westward. It was upgraded to severe tropical storm (STS) intensity 12 hours later and then moved northwestward. Keeping its northwestward track, it was upgraded to typhoon (TY) intensity over the same waters at 06 UTC the next day, moved westward and reached its peak intensity with maximum sustained winds of 105 kt and a central pressure of 920 hPa over the South China Sea at 00 UTC on 1 October. After it gradually turned northward, it weakened to STS intensity rapidly over the Bashi Channel at 00 UTC on 3 October. It hit Taiwan with STS intensity before 06 UTC on 3 October. It weakened to TD intensity at 12 UTC on 3 October and then dissipated six hours later.



BARIJAT (2419)

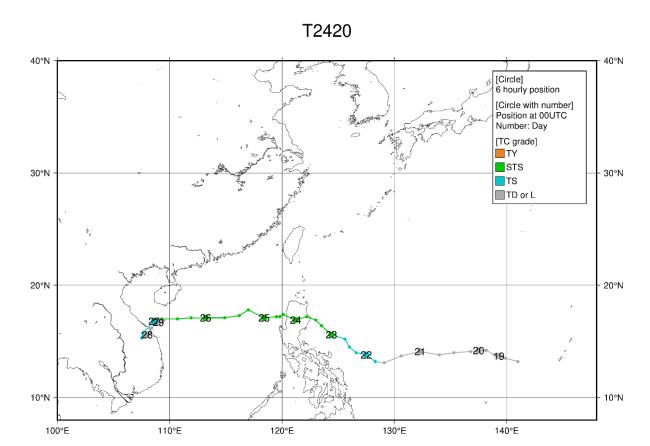
BARIJAT formed as a tropical depression (TD) around the Mariana Islands at 18 UTC on 4 October 2024 and moved northward. It was upgraded to tropical storm (TS) intensity over the same waters at 06 UTC on 6 October. Keeping its northward track, it reached its peak intensity with maximum sustained winds of 45 kt and a central pressure of 985 hPa over the far off east of Japan at 18 UTC on 10 October. It transitioned into an extratropical cyclone over the same waters by six hours later. After it moved to the sea around the Kuril Islands and turned eastward, it turned in a counterclockwise direction to circle east of the Kamchatka Peninsula. It moved eastward and crossed longitude 180 degrees east before 12 UTC on 15 October.





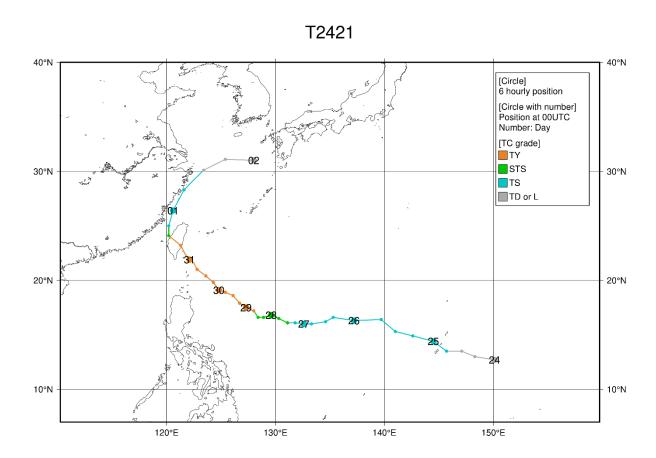
TRAMI (2420)

TRAMI formed as a tropical depression (TD) around the Mariana Islands at 12 UTC on 18 October 2024 and moved westward. It was upgraded to tropical storm (TS) intensity over the sea east of the Philippines at 18 UTC on 21 October and moved northwestward. Keeping its northwestward track, it was upgraded to severe tropical storm (STS) intensity over the same waters at 00 UTC on 23 October. It crossed north of Luzon Island with STS intensity 18 hours later and then moved westward. After entering the South China Sea, it reached its peak intensity with maximum sustained winds of 60 kt and a central pressure of 970 hPa at 06 UTC on 26 October. It was downgraded to TS intensity over the sea east of Viet Nam at 00 UTC on 27 October and then hit Viet Nam. Turning in a counterclockwise direction to circle, it weakened to TD intensity at 18 UTC on 27 October. It entered the South China Sea again and dissipated at 18 UTC on 29 October.



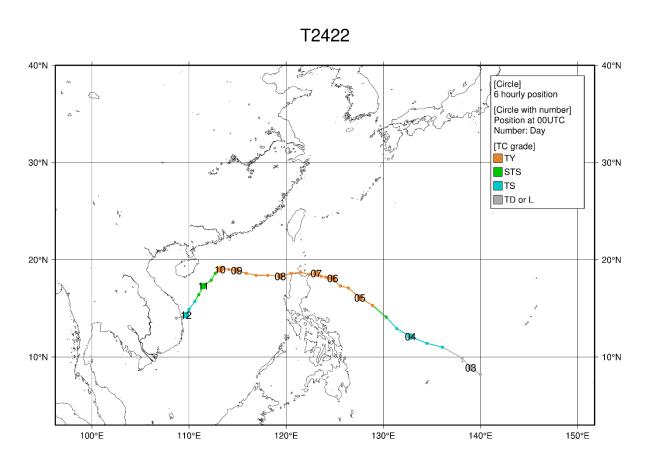
KONG-REY (2421)

KONG-REY formed as a tropical depression (TD) around the Chuuk Islands at 00 UTC on 24 October 2024 and moved westward. It was upgraded to tropical storm (TS) intensity around the Mariana Islands 18 hours later and was further upgraded to typhoon (TY) intensity over the sea east of the Philippines at 18 UTC on 28 October. After turning northwestward, it reached its peak intensity with maximum sustained winds of 100 kt and a central pressure of 925 hPa over the same waters at 00 UTC on 30 October. Keeping its northwestward track, it hit Taiwan with TY intensity around 06 UTC on 31 October and then weakened rapidly. After it entered Taiwan Strait and turned northward, it was downgraded to STS intensity at 12 UTC on 31 October and to TS intensity six hours later. Turning northeastward, it transitioned into an extratropical cyclone over the East China Sea by 12 UTC on 1 November. It moved eastward and dissipated over the same waters 18 hours later.



YINXING (2422)

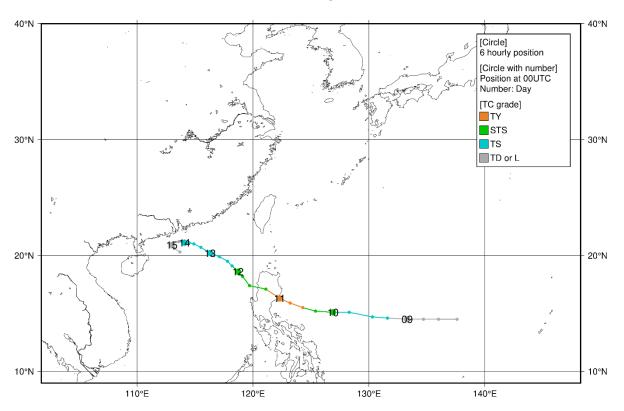
YINXING formed as a tropical depression (TD) around the Caroline Islands at 18 UTC on 2 November 2024 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the sea east of the Philippines 18 hours later. It developed rapidly and was further upgraded to typhoon (TY) intensity at 18 UTC the next day. It reached its peak intensity with maximum sustained winds of 100 kt and a central pressure of 945 hPa over the sea north of the Philippines at 06 UTC on 7 November and moved westward. After entering the South China Sea, it was downgraded to STS intensity at 12 UTC on 10 November and turned southwestward. After weakening to TD intensity over the same waters at 06 UTC on 12 November, it hit Viet Nam and dissipated 12 hours later.



TORAJI (2423)

TORAJI formed as a tropical depression (TD) over the sea east of the Philippines at 06 UTC on 8 November 2024 and moved westward. After upgraded to tropical storm (TS) intensity over the same waters at 06 UTC on 9 November, it developed rapidly and was further upgraded to typhoon (TY) intensity at 12 UTC the next day. It reached its peak intensity with maximum sustained winds of 70 kt and a central pressure of 980 hPa over the same waters at 18 UTC on 10 November. Keeping its westward track, it crossed north of Luzon Island with TY intensity after 00 UTC on 11 November and entered the South China Sea. Turning northwestward, it was downgraded to TS intensity over the same waters at 06 UTC on 12 November and weakened to TD intensity at 12 UTC on 14 November. After turning southeastward, it dissipated over the same waters at 18 UTC on 15 November.

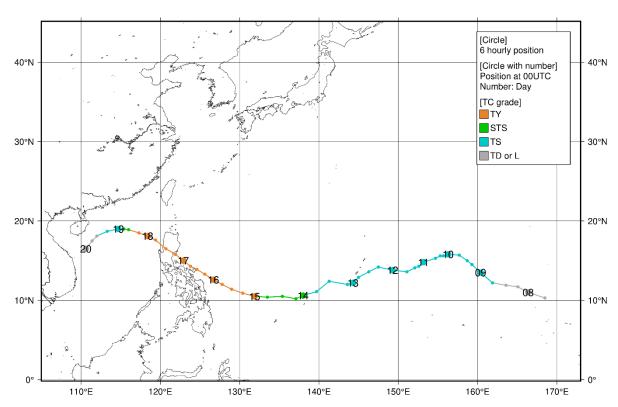




MAN-YI (2424)

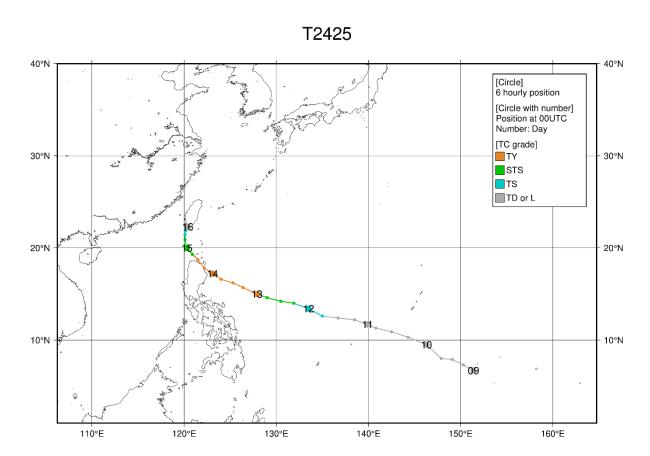
MAN-YI formed as a tropical depression (TD) around the Marshall Islands at 18 UTC on 7 November 2024 and moved westward. It was upgraded to tropical storm (TS) intensity at 18 UTC the next day and moved northwestward. Gradually turning southwestward around the Mariana Islands, it was upgraded to severe tropical storm (STS) intensity over the sea east of the Philippines at 00 UTC on 14 November and turned westward. Developing rapidly, it was further upgraded to typhoon (TY) intensity at 00 UTC on 15 November and turned northwestward. It reached its peak intensity with maximum sustained winds of 105 kt and a central pressure of 920 hPa over the same waters at 00 UTC the next day. Keeping its TY intensity and northwestward track, it crossed north of Luzon Island at 06 UTC on 17 November and then weakened rapidly. After entering the South China Sea, it was downgraded to STS intensity at 12 UTC on 18 November and turned southwestward. It further weakened to TD intensity at 12 UTC the next day. Keeping its southwestward track, it dissipated over the same waters 18 hours later.





USAGI (2425)

USAGI formed as a tropical depression (TD) around the Chuuk Islands at 00 UTC on 9 November 2024 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the sea east of the Philippines at 18 UTC on 11 November. Developing rapidly over the same waters, it was further upgraded to typhoon (TY) intensity at 00 UTC on 13 November and reached its peak intensity with maximum sustained winds of 95 kt and a central pressure of 940 hPa at 00 UTC the next day. Keeping its northwestward track, it crossed north of Luzon Island with TY intensity around 06 UTC on 14 November and weakened rapidly. After gradually turning northward, it was downgraded to TS intensity over the Bashi Channel at 12 UTC on 15 November and weakened to TD intensity over the sea south of Taiwan 12 hours later. It remained almost stationary around south of Taiwan and dissipated at 18 UTC on 16 November.



PABUK (2426)

PABUK formed as a tropical depression (TD) over the South China Sea at 18 UTC on 21 December 2024 and moved westward. It was upgraded to tropical storm (TS) intensity and reached its peak intensity with maximum sustained winds of 35 kt and a central pressure of 1002 hPa over the same waters at 06 UTC on 22 December. It moved northwestward and gradually turned southwestward around 00 UTC on 24 December. It weakened to TD intensity at 18 UTC on 24 December. Keeping its southwestward track, it dissipated over the same waters at 18 UTC on 25 December.

