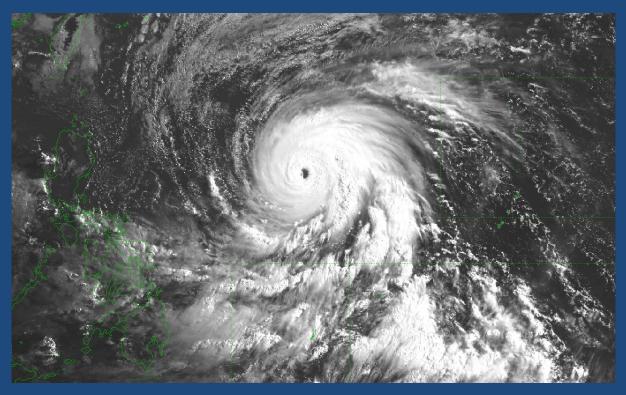
# Annual Report on the Activities of the RSMC Tokyo - Typhoon Center 2023



TY MAWAR 22 UTC, 26 May 2023

Japan Meteorological Agency

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### Japan Meteorological Agency

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#### Introduction

The RSMC Tokyo - Typhoon Center (referred to here as the Center) is a Regional Specialized Meteorological Centre (RSMC) that carries out specialized activities in analysis, tracking and forecasting of western North Pacific tropical cyclones (TCs) within the framework of the World Weather Watch (WWW) Programme of the World Meteorological Organization (WMO). The Center was established at the headquarters of the Japan Meteorological Agency (JMA) in July 1989 following a designation by the WMO Executive Council at its 40th session (Geneva, June 1988).

The Center conducts the following operations on a routine basis:

- (1) Preparation of information on the formation, movement and development of TCs and associated meteorological phenomena
- (2) Preparation of information on synoptic-scale atmospheric situations that affect the behavior of TCs
- (3) Provision of the above information to National Meteorological Services (NMSs), and in particular to United Nations Economic and Social Commission for Asia and the Pacific (ESCAP)/WMO Typhoon Committee Members, in appropriate formats for operational processing

In addition to the routine services outlined above, the Center distributes a series of reports entitled *Annual Report on the Activities of the RSMC Tokyo - Typhoon Center* as operational references for the NMSs concerned. The reports summarize the activities of the Center and review the TCs of the preceding year.

In this issue covering 2023, Chapter 1 outlines routine operations performed at the Center and its operational products, while Chapter 2 reports on its major activities in 2023. Chapter 3 describes atmospheric and oceanic conditions in the tropics and notes the highlights of TC activity in 2023. Chapter 4 presents verification statistics relating to operational forecasts (i.e., official forecasts), results from JMA's numerical weather prediction (NWP) models and other guidance models, Atmospheric Motion Vector (AMV) based Sea-surface Wind (ASWind) data, TC central pressure estimates based on satellite microwave observations and storm surge predictions. Best track data for 2023 TCs of tropical storm (TS) intensity or higher are shown in table and chart form in the appendices.

## Chapter 1 Operations at the RSMC Tokyo - Typhoon Center in 2023

The Center's area of responsibility covers the western North Pacific and the South China Sea  $(0^{\circ}-60^{\circ}\text{N}, 100^{\circ}-180^{\circ}\text{E})$  including marginal seas and adjacent land areas (Figure 1.1). The Center carries out analysis and forecasting in relation to TCs in the area and also provides the relevant NMSs with RSMC products via the Global Telecommunication System (GTS), the Aeronautical Fixed Telecommunication Network (AFTN), the Internet and other media.

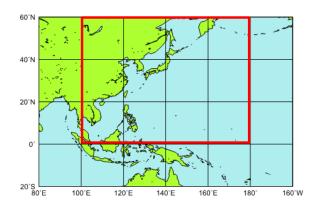


Figure 1.1

Area of responsibility of the RSMC Tokyo Typhoon Center

#### 1.1 Analysis

TC analysis is performed eight times a day at 00, 03, 06, 09, 12, 15, 18 and 21 UTC, and begins with determination of the TC's center position. Cloud imagery from Himawari-8/9 and microwave imagery from various polar orbiting satellites are the principal sources for this determination, especially for TCs migrating over data-sparse ocean areas. Information on the TC's direction and speed of movement is extracted primarily from six-hourly displacement vectors of the center position.

The maximum sustained wind speed in the vicinity of the TC's center is determined mainly from the Current Intensity (CI) number, which is derived from satellite imagery using the Dvorak method. The central pressure of the TC is then determined from the maximum sustained wind speed with the assumption of a certain pressure profile around the TC. The radii of circles representing winds with speeds exceeding 30 and 50 knots are determined mainly from surface observation, Advanced Scatterometer (ASCAT) observation and ASWind data derived from satellite images in the vicinity of the TC. The size of the central dense overcast area of the TC as observed in satellite imagery is also referenced to determine the radius of 50-knot wind speed circles.

#### 1.2 Forecast

The Center issues TC track forecasts with probability circles, as well as intensity forecasts for tropical depressions (TDs) expected to reach tropical storm (TS) intensity within 24 hours and for TCs with TS intensity or higher up to 120 hours ahead. As a primary basis for TC track forecasts, JMA implements NWP using the Global Spectral Model (GSM) and the Global Ensemble Prediction System (GEPS). The GSM (TQ959, upgraded on 14 March 2023) has a horizontal resolution of approximately 13 km and 128 vertical layers, while GEPS (TQ479; upgraded on 14 March 2023) has 51 members with a horizontal resolution of

approximately 27 km and the same number of vertical layers. GSM horizontal resolution was enhanced from 20 to 13 km in 2023. Further details and recent model improvements are detailed in Appendix 7. Since 2015 the Center has mainly employed a consensus method for TC track forecasts. This approach involves taking the mean of predicted TC positions from multiple deterministic models, including the GSM and other NWP centers' models, such as European Centre for Medium-Range Weather Forecasts (ECMWF), National Centers for Environmental Prediction (NCEP) and United Kingdom Met Office (UKMO) global models.

A probability circle shows the range into which the center of a TC is expected to move with 70% probability at each validation time. The radius for all forecast periods up to 120 hours is determined by the multiple ensemble method, which is solely according to the confidence level based on the cumulative ensemble spread calculated using multiple ensemble prediction systems (EPSs) consisting of ECMWF, NCEP and UKMO global EPSs in addition to GEPS.

In relation to TC intensity, the Center began providing TC intensity forecasts with extended lead times of up to 120 hours in March 2019, based on several tropical cyclone intensity forecast guidance products including Typhoon Intensity Forecasting scheme based on Statistical Hurricane Intensity Prediction Scheme (SHIPS), which is known as TIFS and Logistic Growth Equation Model (LGEM). These schemes were developed by JMA and Meteorological Research Institute (MRI) of JMA. The Center also refers to Hurricane Weather Research and Forecast model (HWRF) and Hurricane Analysis and Forecasting System (HAFS) in NCEP.

#### 1.3 Provision of RSMC Products

The Center prepares and distributes the RSMC bulletins listed below via the GTS or the AFTN when:

- a TC of TS intensity or higher exists in the Center's area of responsibility
- a TD is expected to reach or exceed TS intensity in the area within 24 hours

RSMC products are issued while any TC of TS intensity or higher or any TD expected to reach or exceed TS intensity within 24 hours exists in the Center's area of responsibility. Appendix 6 denotes the code forms of the bulletins.

#### (1) RSMC Tropical Cyclone Advisory (WTPQ50-55 RJTD: via GTS)

The RSMC Tropical Cyclone Advisory is issued eight times a day after observations made at 00, 03 06, 09, 12, 15, 18 and 21 UTC, and reports the following elements in analysis and in 24-, 48-, 72-, 96- and 120-hour forecasts for TCs:

Analysis Center position

Accuracy of center position determination

Direction and speed of movement

Central pressure

Maximum sustained wind speed (10-minute average)

Maximum gust wind speed

Radii of wind areas over 50 and 30 knots

24-, 48-, 72-, 96- and 120-hour Forecasts<sup>1</sup>

Center position and radius of probability circle

Direction and speed of movement

Central pressure

Maximum sustained wind speed (10-minute average)

Maximum gust wind speed

#### (2) RSMC Guidance for Forecast by GSM (FXPQ20-25 RJTD: via GTS)

The RSMC Guidance for Forecast by GSM reports the results of predictions made by the GSM; which is run four times a day with initial analyses at 00, 06, 12 and 18 UTC. The guidance presents six-hourly GSM predictions for TCs up to 132 hours ahead and reports the following elements:

NWP prediction (T = 006 to 132)

Center position

Central pressure\*

Maximum sustained wind speed\*

#### (3) RSMC Guidance for Forecast by GEPS (FXPQ30-35 RJTD: via GTS)

The RSMC Guidance for Forecast by GEPS reports the results of predictions made by the GEPS; which is run four times a day with initial analyses at 00, 06, 12 and 18 UTC. The guidance presents the ensemble mean of GEPS six-hourly predictions up to 132 hours ahead and reports the following elements:

NWP prediction (T = 006 to 132)

Center position

Central pressure\*

Maximum sustained wind speed\*

#### (4) SAREP (IUCC10 RJTD: via GTS)

The SAREP in BUFR format reports the results of TC analysis including intensity information (i.e., the CI number) based on the Dvorak method. It is issued shortly after observations made for TCs with TS intensity or higher at 00, 03, 06, 09, 12, 15, 18 and 21 UTC (TDs expected to reach TS intensity or higher within 24 hours at 00, 06, 12 and 18), and reports the following elements:

Himawari-8/9 imagery analysis

Center position

Accuracy of center position determination

Direction and speed of movement Mean diameter of overcast cloud

Apparent past 24-hour change in intensity\*\*

Dvorak Intensity (CI, T, DT, MET, PT number) \*\*

Cloud pattern type of the DT number\*\*

Trend of past 24-hour change\*\*

Cloud pattern type of the PT number\*\*

Type of the final T-number\*\*

BUFR/CREX templates for translation into table-driven code forms are provided on the WMO website

<sup>\*</sup> Predictions of these parameters are given as deviations from those at the initial time.

<sup>\*</sup> Predictions of these parameters are given as deviations from those at the initial time.

<sup>\*\*</sup> Reported only at 00, 06, 12 and 18 UTC

<sup>&</sup>lt;sup>1</sup> At 03, 09, 15 and 21 UTC, 24-, 45-, 69-, 93- and 117-hour forecasts for TCs are reported.

at <a href="https://community.wmo.int/activity-areas/wis/wis-manuals">https://community.wmo.int/activity-areas/wis/wis-manuals</a>. The SAREP is provided in text format on the Numerical Typhoon Prediction (NTP) website (see 1.7).

#### (5) RSMC Prognostic Reasoning (WTPQ30-35 RJTD: via GTS)

The RSMC Prognostic Reasoning report provides brief reasoning for TC analysis and forecasts, and is issued at 00, 06, 12 and 18 UTC following the issuance of the RSMC Tropical Cyclone Advisory. The bulletin provides general comments on current positioning, intensity and related changes, synoptic situations such as those of the subtropical high and atmospheric/oceanographic fields, reasoning behind TC track and intensity forecasts (including details of methodology and guidance models), and relevant remarks in plain language.

#### (6) RSMC Tropical Cyclone Best Track (AXPQ20 RJTD: via GTS)

The RSMC Tropical Cyclone Best Track report provides post-analysis data on TCs of TS intensity or higher. It reports the center position, the central pressure and the maximum sustained wind speed. The best track for each TC is usually finalized three months after the termination of related issuance of the above RSMC bulletins.

### (7) <u>Tropical Cyclone Advisory for SIGMET</u> (FKPQ30-35 RJTD: via AFTN, and IWXXM 3.0 format: via AMHS (see 1.4))

As a Tropical Cyclone Advisory Centre (TCAC) within the framework of the International Civil Aviation Organization (ICAO), the Center provides Tropical Cyclone Advisory (TCA) for SIGMET to Meteorological Watch Offices (MWOs) in order to support their preparations of SIGMET information on TCs. These advisories include the following elements in analysis and in 6-, 12-, 18- and 24-hour forecasts:

Analysis Center position

Observed CB cloud

Direction and speed of movement

Changes in intensity
Central pressure

Maximum sustained wind speed (10-minute average)

Forecast Center position

Maximum sustained wind speed (10-minute average)

#### 1.4 Tropical Cyclone Advisory for SIGMET

The Center provides text-format and graphical TCAs in its role as the ICAO TCAC. These include the horizontal extent of cumulonimbus cloud and cloud top height associated with TCs potentially affecting aviation safety, in addition to text-format TCA information. Both text-format and graphical TCAs and related specifications are provided online for users via linkage from the NTP website (see 1.7), and graphical TCAs are also provided to World Area Forecast Centres (WAFCs).

In November 2020, TCAs in IWXXM 3.0 format were introduced and shared on the TCAC Tokyo website, followed by transmission via Air Traffic Services (ATS) Message Handling Services (AMHS) in March 2022. The IWXXM format is detailed in Guidelines for the Implementation of OPMET Data Exchange Using IWXXM, Third Edition (May 2019), ICAO.

#### 1.5 WIS Global Information System Center Tokyo Server

As designated at the Sixteenth WMO Congress in June 2011, the Center introduced Data Collection or Production Centre (DCPC) service under the Global Information System Centre (GISC) Tokyo for the WMO Information System (WIS) in August 2011. It provides NWP products such as data on predicted fields in grid-point-value (GPV) form and observational values through WIS Data Discovery, Access and Retrieval (DAR) via a GISC Tokyo server (<a href="https://www.wis-jma.go.jp/">https://www.wis-jma.go.jp/</a>). GSM products with resolution of 0.5 and 0.25 degrees (surface layer) and JMA SATAID (SATellite Animation and Interactive Diagnosis; <a href="https://www.wis-jma.go.jp/cms/sataid/">https://www.wis-jma.go.jp/cms/sataid/</a>) Service are also available from the server through WIS DAR. All products available via the server are listed in Appendix 8.

#### 1.6 RSMC Tokyo - Typhoon Center Website

The RSMC Tokyo - Typhoon Center Website provides TC advisories on a real-time basis and a wide variety of products including TC analysis archives, technical reviews and annual reports on the Center's activities at <a href="https://www.jma.go.jp/jma/jma-eng/jma-center/rsmc-hp-pub-eg/RSMC\_HP.html">https://www.jma.go.jp/jma/jma-eng/jma-center/rsmc-hp-pub-eg/RSMC\_HP.html</a>. Since November 2012, the website provides experimental TC advisory information in Common Alert Protocol (CAP) format.

#### 1.7 Numerical Typhoon Prediction Website

Since October 2004, the Center has operated the Numerical Typhoon Prediction (NTP) website to assist the NMSs of Typhoon Committee Members in improving their TC forecasting and warning services. The site provides TC track predictions and weather maps of deterministic global NWP models from nine centers (Bureau of Meteorology (BoM, Australia), China Meteorological Administration (CMA, China), Canadian Meteorological Centre (CMC, Canada), Deutscher Wetterdienst (DWD, Germany), ECMWF, Korea Meteorological Administration (KMA, Republic of Korea), NCEP (USA), UKMO (UK) and JMA), ensemble TC track predictions of global EPSs from four centers (ECMWF, NCEP, UKMO and JMA) and a wide variety of products including the results of the Center's TC analysis, upper-air analysis, ocean analysis, storm surge and ocean wave forecasting. All products available on the website are listed in Appendix 9.

#### 1.8 TC Communication platform

The Center's TC communication platform (developed and maintained since July 2019) supports enhanced interaction between operational forecasters in the NMSs of Typhoon Committee Members and the Center, as well as sharing of advance-notice updates. Full-scale operation of the platform was started during the 2021 typhoon season and related discussions have helped to clarify TC status and forecasts. All services provided on the platform are listed in Appendix 9.

## Chapter 2 Major Activities of the RSMC Tokyo - Typhoon Center in 2023

#### 2.1 Provision of RSMC Products

The Center provides operational products for TC forecasting to NMSs via the GTS, the AFTN and other networks. Monthly and annual totals of products issued in 2023 are listed in Table 2.1.

Table 2.1 Monthly and annual totals of products issued by the RSMC Tokyo - Typhoon Center in 2023

Product	Jan	Feb	Mar	Apr	Мау	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
IUCC10	0	0	0	27	96	72	138	336	108	153	4	12	946
WTPQ30-35	0	0	0	19	50	37	77	177	57	80	5	8	510
WTPQ50-55	0	0	0	37	101	76	156	359	118	164	8	17	1036
FXPQ20-25	0	0	0	18	50	37	77	177	57	80	4	8	508
FXPQ30-35	0	0	0	18	50	37	77	177	57	80	4	8	508
FKPQ30-35	0	0	0	18	51	37	77	177	57	80	4	8	509
AXPQ20	9	0	0	0	0	0	1	1	1	3	7	0	22

#### Notes:

IUCC10 RJTD	SAREP (BUFR format)
WTPQ30-35 RJTD	RSMC Prognostic Reasoning
WTPQ50-55 RJTD	RSMC Tropical Cyclone Advisory
FXPQ20-25 RJTD	RSMC Guidance for Forecast by GSM
FXPQ30-35 RJTD	RSMC Guidance for Forecast by GEPS
FKPQ30-35 RJTD	Tropical Cyclone Advisory for SIGMET
AXPQ20 RJTD	RSMC Tropical Cyclone Best Track

#### 2.2 Publications

In May and December 2023, the Center published the 25th and 26th issues of the RSMC Technical Review with the following areas of focus:

- 1. Upgrade of JMA's Storm Surge Prediction for the WMO Storm Surge Watch Scheme (SSWS) in 2022
- 2. JMA 30-year Dvorak Reanalysis for the Western North Pacific

In January 2024, the Center published the *Annual Report on the Activities of the RSMC Tokyo - Typhoon Center 2022*. Both publications are available on the Center's website at <a href="https://www.jma.go.jp/jma/jma-eng/jma-center/rsmc-hp-pub-eg/RSMC\_HP.html">https://www.jma.go.jp/jma/jma-eng/jma-center/rsmc-hp-pub-eg/RSMC\_HP.html</a>.

#### 2.3 Typhoon Committee Attachment Training

The Center has organized ESCAP/WMO Typhoon Committee Attachment Training courses every fiscal year since 2001 with the support of the WMO Tropical Cyclone Programme and the Typhoon Committee in order to advance the TC analysis and forecasting capacity of Committee Members.

In 2023, amid the COVID-19 pandemic, the 22nd course was held online (as in March 2021 and January 2022) from 11 to 13 January 2023 with 51 attendees from eight Typhoon Committee Members (China, Hong Kong China, Macao China, Malaysia, the Philippines, the Republic of Korea, Thailand and the United States of America), along with one invited lecturer. The course was enhanced with hands-on training materials for self-study and with interactive exercises on satellite analysis techniques/Dvorak analysis. The Center highlighted the purposes of the course as set out under Category 2 Unit of the Tropical Cyclone Forecast Competency in the Typhoon Committee Region specifications of the Typhoon Committee Operational Manual (TOM).

In addition, preparations were made for the 23rd event to be held from 15 to 26 January 2024. Amid the COVID-19 pandemic, the course had been held virtually for three years, but this one was held in person with attendees from seven Typhoon Committee Members (Hong Kong China, Lao PDR, Macao China, Malaysia, the Philippines, the Republic of Korea, and Vietnam) and two from the Panel on Tropical Cyclones (PTC) (Saudi Arabia and Sri Lanka). Presentations included content from researchers and Japanese experts from the Typhoon Committee's Hydro and Disaster Risk Reduction group, and from weathercasting professionals, to give a broad perspective and contribute to the UN's EW4All initiative.

The Center is committed to improving forecasting competence, and thereby the capacity of Meteorological Services in the Typhoon Committee region, via training to meet various regional needs, including basic application, state-of-the-art tropical cyclone forecasting and monitoring techniques/methodologies.

#### 2.4 Other Activities in 2023

#### 2.4.1 Services Introduced in 2023

Update of probability-circle radii for tropical cyclone track forecasts

On 26 June 2023, the Center updated its 70% probability-circle radii based on recent improvements in forecast accuracy. Radii for two days ahead and beyond have been reduced, with those for five days ahead now being up to 40% smaller.

## Chapter 3 Summary of the 2023 Typhoon Season

In 2023, 17 TCs of TS intensity or higher formed over the western North Pacific and the South China Sea. This total was below the climatological normal<sup>2</sup> frequency of 25.1. Among these 17 TCs, 10 reached Typhoon (TY) intensity, 2 reached severe tropical storm (STS) intensity and 5 reached TS intensity (Table 3.1).

Table 3.1 List of tropical cyclones reaching TS intensity or higher in 2023

	Tropical Cycl	lone	]	Duratio	on	(UTC)		Minim	ım Cen	tral Pres	sure	Max Wind
				(TS o	r h	igher)		(UTC)	lat(N)	long(E)	(hPa)	(kt)
TS	Sanvu	(2301)	201200	Apr	-	220000	Apr	210600	10.3	155.7	996	45
TY	Mawar	(2302)	201200	May	-	030000	Jun	251200	14.8	141.5	900	115
TY	Guchol	(2303)	061200	Jun	-	121200	Jun	091800	18.5	129.9	960	80
STS	Talim	(2304)	150600	Jul	-	181200	Jul	170000	20.1	113.0	970	60
TY	Doksuri	(2305)	210000	Jul	_	290000	Jul	241800	16.9	125.1	925	100
TY	Khanun	(2306)	280000	Jul	-	100600	Aug	010000	24.6	129.4	930	95
TY	Lan	(2307)	080000	Aug	-	170600	Aug	101800	26.4	142.9	940	90
TY	Dora	(2308)	120600	Aug	-	150000	Aug	120600	16.3	179.1	980	75
TY	Saola	(2309)	240600	Aug	-	021800	Sep	300000	20.1	121.0	920	105
STS	Damrey	(2310)	241800	Aug	-	290600	Aug	260600	26.1	152.9	985	50
TY	Haikui	(2311)	281800	Aug	-	050000	Sep	021800	22.7	123.1	945	85
TS	Kirogi	(2312)	301200	Aug	-	030000	Sep	310600	16.7	154.2	994	45
TS	Yun-yeung	(2313)	051200	Sep	-	081200	Sep	060600	26.6	134.2	998	40
TY	Koinu	(2314)	291800	Sep	-	090600	Oct	021800	20.2	125.5	940	90
TY	Bolaven	(2315)	071200	Oct	_	141200	Oct	111200	18.9	143.0	905	115
TS	Sanba	(2316)	180000	Oct	-	200000	Oct	191200	21.0	109.4	1000	40
TS	Jelawat	(2317)	170600	Dec	-	180000	Dec	170600	7.5	129.6	1002	35

#### 3.1 Atmospheric and Oceanographic Conditions in the Tropics

In association with the La Niña event that began in boreal autumn 2021 (September – November 2021) and terminated in winter 2023 (December 2022 – February 2023), significantly positive SST anomalies were observed in the western part of the equatorial Pacific and negative SST anomalies were seen from central to eastern parts from autumn 2021 to winter 2023. Tropical convection was enhanced from the eastern Indian Ocean to Southeastern Asia, and was suppressed near the date line in the equatorial Pacific.

An El Niño event occurred in boreal spring 2023 (March – May), and developed through boreal autumn. In association, SSTs in the eastern equatorial Pacific increased, and significantly positive SST anomalies emerged in the western and eastern equatorial Pacific in spring. Influences from these anomalous temperatures on atmospheric circulation were seen in the tropics. Tropical convection in spring was enhanced over the latitude bands from 10 to 20°N in the western and central tropical Pacific, and was suppressed from

 $<sup>^2</sup>$  The base period for the climatological normal is 1991 - 2020. The normal was updated in early 2021 based on 30-year data.

the Indochina Peninsula to the eastern Indian Ocean and over the equatorial central South Pacific.

In summer (June – August), positive SST anomalies over a wide area of the equatorial Pacific were observed, with significant values from central to eastern parts. In the tropical Indian Ocean, significantly positive anomalies were also seen from the Bay of Bengal to the tropical western part and negative anomalies were seen in the tropical southeastern part, indicating the positive phase of an Indian Ocean Dipole (IOD) event (Figure 3.1 (a)). Tropical convection was enhanced from seas east of the Philippines to the western equatorial Pacific and over the equatorward-shifted intertropical convergence zone in the eastern Pacific, and was suppressed in the Indian Ocean (Figure 3.1 (b)). In the lower troposphere, anti-cyclonic circulation anomalies straddling the equator were seen over the Indian Ocean, and cyclonic circulation anomalies were seen to the south of Japan (Figure 3.1 (c)). The circulation anomalies over the tropical Pacific correspond to equatorward-shifted enhanced convection over the eastern tropical Pacific, suggesting an influence from the El Niño event.

In autumn the El Niño event persisted, and positive SST anomalies were observed over a wide area of the equatorial Pacific, accompanied by significant positive anomalies from central to eastern parts. In the tropical Indian Ocean, significantly positive SST anomalies were seen in the western part and significantly negative anomalies were seen in the southeastern part, corresponding to the positive phase of the IOD event that started in boreal summer. Tropical convection was enhanced in the equatorial Pacific and the western Indian Ocean and suppressed from the eastern Indian Ocean to Indonesia. In the lower troposphere, anticyclonic circulation anomalies straddling the equator were seen over the Indian Ocean. Anti-cyclonic circulation anomalies were also seen in the subtropics from the South China Sea to the western North Pacific. Those from the Indian Ocean to the Pacific in the tropics corresponded to tropical convection, suggesting influences from the persistent El Niño event and the positive phase of the IOD.

Atmospheric and oceanographic charts (including monthly mean streamlines at 850 and 200 hPa, OLRs<sup>3</sup> with related anomalies, and monthly mean SSTs with related anomalies for the western North Pacific and the South China Sea) are provided on the Tokyo Climate Center website at

https://www.data.jma.go.jp/tcc/tcc/products/clisys/figures/db\_hist\_mon\_tcc.html and https://www.data.jma.go.jp/tcc/tcc/products/elnino/ocean/index\_tcc.html.

<sup>&</sup>lt;sup>3</sup> OLR data were calculated using information provided by the Climate Prediction Center/NOAA at https://www.cpc.ncep.noaa.gov/products/global\_precip/html/wpage.olr.html.

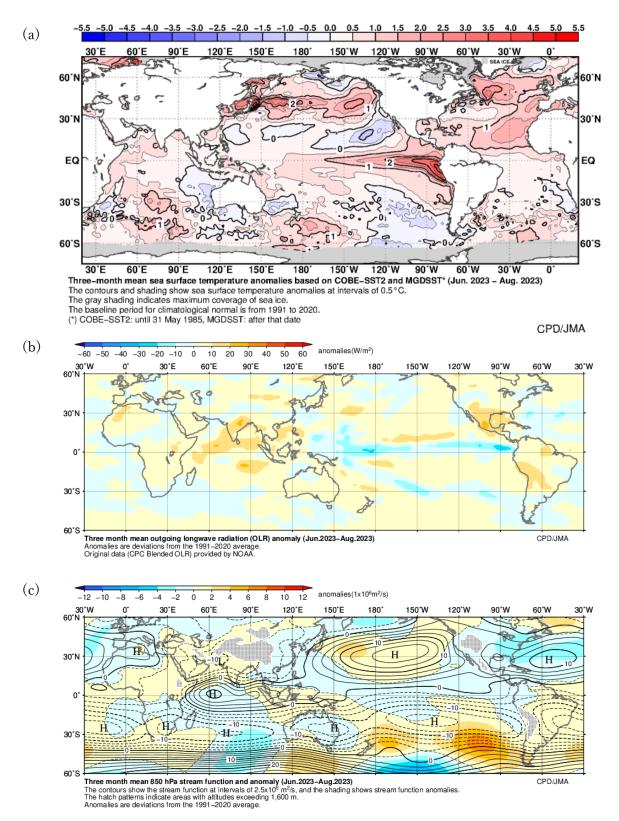


Figure 3.1 Three-month mean (a) sea surface temperature (SST) anomaly, (b) outgoing longwave radiation (OLR) anomaly, and (c) 850-hPa stream function (contours) and related anomaly (shading) in boreal summer (June – August 2023)

The base period for the normal is 1991-2020. (a) The contour interval is  $0.5^{\circ}$ C. Sea ice coverage areas are shaded in gray. (b) Negative (cold color) and positive (warm color) OLR anomalies show enhanced and suppressed convection, respectively, compared to the normal. Original data is provided by NOAA. (c) The contour interval is  $2.5 \times 10^6$  m²/s. "H" and "L" denote high- and low-pressure systems, respectively.

#### 3.2 Tropical Cyclones in 2023

A total of 17 named TCs formed over the western North Pacific and the South China Sea in 2023, which was below the climatological normal. Monthly and normal numbers of named TC formations are shown in Figure 3.2, and the tracks of the 17 TCs are shown in Figure 3.3. Figure 3.4 shows the genesis points of these TCs (dots) and related frequency distribution for past years (1951 – 2022).

The 2023 typhoon season started in April with Sanvu (2301), which formed over the sea southwest of the Marshall Islands. Only five typhoons formed from September onward, which was the lowest since records began. The lower number of formations during the peak period may have contributed to the reduced annual total. This situation may be related to the fact that the monsoon trough and the low-pressure area extending from the South China Sea to the Philippines in autumn were weaker than the climatological normal, and convective activity in this area was inactive.

The mean genesis point of named TCs was 15.1°N and 137.9°E, representing a south-eastward deviation from that of the 30-year average<sup>4</sup> (16.3°N and 135.9°E) (see Figure 3.4). The mean genesis point of named TCs formed in summer (June to August) was 17.0°N and 138.2°E, with south-eastward deviation from that of the 30-year summer average (18.5°N and 134.2°E), and that of named TCs formed in autumn (September to November) was 16.3°N and 131.8°E, with westward deviation from that of the 30-year autumn average (16.2°N and 137.0°E). The south-eastward shift of the mean genesis point in summer is presumed to be partly associated with the El Niño event that started in 2023.

The mean duration of TCs sustaining TS intensity or higher was 6.1 days, which was longer than that of the 30-year average (5.2 days). The mean duration of TCs sustaining TS intensity or higher formed in summer was 6.7 days, which was longer than that of the 30-year average (5.0 days), and the mean duration of TCs sustaining TS intensity or higher formed in autumn was 5.4 days, which was same as that of the 30-year average (5.4 days). The longer-than-average duration in summer is consistent with the results of statistical studies on the El Niño event.

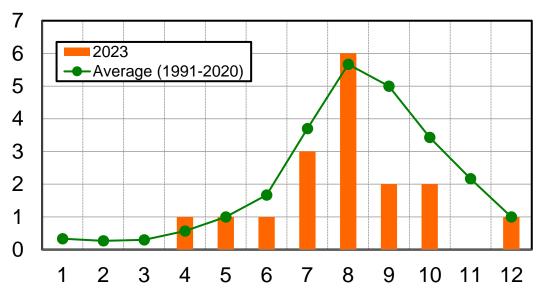


Figure 3.2 Monthly number of named TC formation for 2023 compared to the climatological normal

<sup>&</sup>lt;sup>4</sup> The 30-year averaging period is from 1991 to 2020.

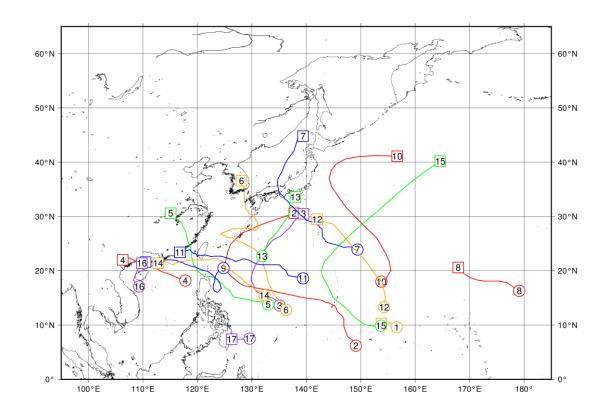


Figure 3.3 Tracks of the 17 named TCs that formed in 2023. TC tracks for those with an intensity of TS or higher are shown.

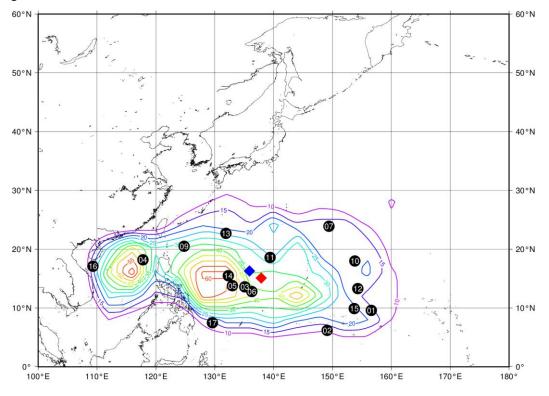


Figure 3.4 Genesis points of the 17 named TCs forming in 2023 (dots) and related frequency distribution for 1951 - 2022 (lines). Red and blue diamonds show the mean genesis points of TCs forming in 2023 and the 30-year average period (1991 - 2020), respectively.

### Chapter 4 Verification of Forecasts and Other Products in 2023

#### 4.1 Verification of Operational Forecasts

Operational forecasts for the 17 TCs of TS intensity or higher that formed in 2023 were verified using RSMC TC best track data<sup>5</sup>. The verified elements were forecasts of the center position, central pressure and maximum sustained wind speed (up to five days ahead). In addition to forecast errors, improvement ratios of forecast errors to climatological model were also evaluated to assess operational forecast skill. Forecasts issued at 00, 06, 12 and 18 UTC were included in verification for TCs classified in best track data as TS, STS or TY at both initial and forecast valid times. The position and intensity errors of such operational forecasts are shown in bold face in Appendix 3. (Those for TD before upgrading into TS intensity or higher are indicated in italic face in Appendix 3.)

#### 4.1.1 Center Position

Figure 4.1 shows annual mean errors in TC track forecasts covering periods of 24 hours (since 1982), 48 hours (since 1989), 72 hours (since 1997), 96 hours and 120 hours (since 2009). It can be seen that operational TC track forecasts have steadily improved since 1982, although year-to-year fluctuations are seen due in part to differences in TC characteristics. The improvement observed since 2015 is partially attributed to the introduction of the consensus method using four global numerical models of ECMWF, JMA, NCEP and UKMO for operational forecasts in that year. The errors in 2023 were 61, 110, 165, 249 and 356 km for 24-, 48-, 72-, 96- and 120-hour forecasts, respectively. 24-, 48- and 72-hour forecast errors in 2023 were the lowest on record.

The annual mean improvement ratios in relation to the climatology and persistence model (CLIPER)<sup>6</sup> for TC track prediction since 2011 are shown in Figure 4.2 to support evaluation of the operational forecast skill. The values are defined as

Mean Position Error (CLIPER) — Mean Position Error (Operational)

Mean Position Error (CLIPER)

and positive/negative values indicate that the operational forecasts were better/worse than the CLIPER predictions. Although there are year-to-year fluctuations, it can be seen that operational forecasts have steadily improved in the long run. The annual mean improvement ratios for 24-, 48-, 72-, 96- and 120-hour forecasts in 2023 were 59% (61% in 2022), 69% (69%), 72% (73%), 70% (77%) and 68% (74%), respectively.

The details of errors including improvement ratios to CLIPER for each named TC that formed in 2023 are summarized in Table 4.1. Forecasts for Haikui (2311) was characterized by large errors. Those in forecasts for Haikui (2311) are attributable to the fact that guidance models predict more northwest-northern tracks than reality. Meanwhile, forecasts for Lan (2307) and Koinu (2314) showed relatively small errors.

<sup>&</sup>lt;sup>5</sup> Maximum sustained wind of TD is not described in best track data or operational forecast. Therefore, maximum sustained wind of TD was treated as 30 kt for convenience in verification in 4.1.

<sup>&</sup>lt;sup>6</sup> The Center operates the CLIPER model based on Aberson (1998), Neumann (1972) and Merrill (1980). The model outputs no information on current atmospheric status, but best track data such as TC center position/central pressure/movement and dates are referenced. Multiple regression coefficients for the model were generated from best track data between 1980 and 2010.

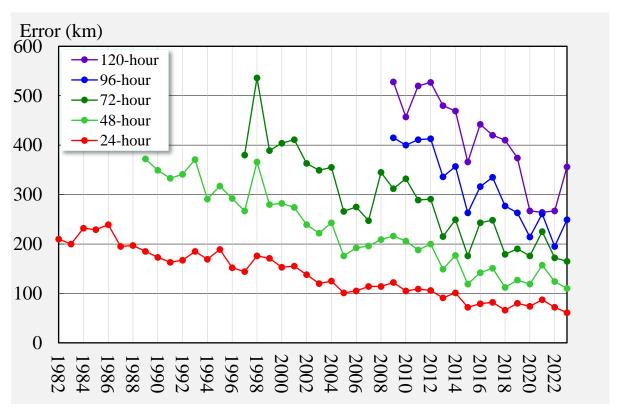


Figure 4.1 Annual mean position errors in 24-, 48-, 72-, 96- and 120-hour operational track forecasts

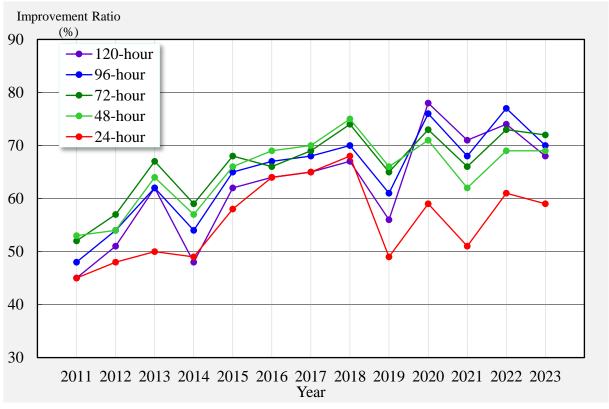


Figure 4.2 Annual mean improvement ratios in 24-, 48-, 72-, 96- and 120-hour operational track forecasts.

Table 4.1 Mean position errors of 24-, 48-, 72-, 96- and 120-hour operational forecasts for each named TC that formed in 2023. S.D., Impr. and Num. represent the standard deviation of operational forecast position errors, improvement ratio (see the equation in 4.1.1 for detail) and number of samples, respectively.

			24	4-hour l	Forecas	st	48	3-hour I	Forecas	st	7	2-hour I	Forecas	t	9	6-hour I	Forecas	t	12	0-hour	Forecas	st
7	Tropical Cy	clone	Mean	S.D.	Num.	Impr.	Mean	S.D.	Num.	Impr.												
			(km)	(km)		(%)	(km)	(km)		(%)												
TS	Sanvu	(2301)	67	21	2	27	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TY	Mawar	(2302)	43	29	50	66	98	43	46	71	158	91	42	75	210	156	38	80	240	237	34	83
TY	Guchol	(2303)	38	23	20	68	90	64	16	71	174	107	12	65	250	86	8	63	406	31	4	9
STS	Talim	(2304)	38	16	9	69	72	24	5	80	170	0	1	81	-	-	0	-	-	-	0	
TY	Doksuri	(2305)	46	29	28	66	79	41	24	69	144	48	20	43	232	102	16	15	323	133	12	17
TY	Khanun	(2306)	53	42	49	61	101	85	45	73	161	133	41	75	271	158	37	68	419	193	33	59
TY	Lan	(2307)	33	28	33	71	44	26	29	85	68	33	25	85	121	49	21	78	192	74	17	69
TY	Dora	(2308)	76	43	7	57	128	35	3	44	-	-	0	-	-	-	0	-	-	-	0	
TY	Saola	(2309)	59	26	34	62	100	40	30	73	141	38	26	76	210	69	22	71	307	82	18	63
STS	Damrey	(2310)	52	27	14	85	70	62	10	91	109	30	6	90	320	137	2	75	-	-	0	
TY	Haikui	(2311)	119	90	25	26	251	144	21	8	385	180	17	12	626	195	13	15	1046	176	9	10
TS	Kirogi	(2312)	139	30	10	46	216	48	6	67	314	45	2	72	-	-	0	-	-	-	0	
TS	Yun-yeun	ıg (2313)	128	42	8	52	256	81	4	56	-	-	0	-	-	-	0	-	-	-	0	
TY	Koinu	(2314)	64	34	34	47	107	65	30	68	134	78	26	79	178	78	21	84	215	115	17	86
TY	Bolaven	(2315)	73	59	24	43	148	138	20	61	218	194	16	73	331	247	12	76	597	199	8	72
TS	Sanba	(2316)	98	41	4	53	_	-	0	-	-	-	0	-	-	-	0	-	-	-	0	
TS	Jelawat	(2317)	_	_	0	_		_	0		_		0	_	_		0	_	_	_	0	
Ar	nual Mean	(Total)	61	49	351	59	110	91	289	69	165	128	234	72	249	179	190	70	356	264	152	68

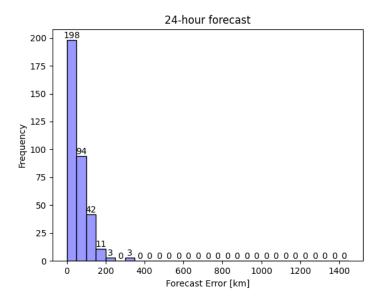


Figure 4.3 Histogram of 24-hour forecast position errors in 2023 (Histograms for 48-, 72-, 96- and 120-hour forecasts are available in the Appendix 5)

Figure 4.3 shows a histogram of 24-hour forecast position errors (histograms for 48-, 72-, 96- and 120-hour forecasts are available in Appendix 5). About 95% (91% in 2022) of 24-hour forecasts, 95% (94%) of 48-hour forecasts, 97% (95%) of 72-hour forecasts, 89% (96%) of 96-hour forecasts and 82% (96%) of 120-hour forecasts had errors of less than 150, 300, 450, 500 and 600 km, respectively.

Figure 4.4 shows frequency distributions of 48-hour forecast position errors in longitudinal/latitudinal direction and cross-track/along-track direction (Scatter diagrams of 24-, 72-, 96- and 120-hour forecasts are available in Appendix 5). While mean position biases are relatively small, a clear slow bias for Bolaven (2315) after recurvature is seen.

Table 4.2 presents the mean hitting ratios and radii of 70% probability circles<sup>7</sup> provided in operational forecasts for each named TC that formed in 2023. The term hitting ratio here is used to describe the ratio of the number of 70% probability circles within which the actual TC center fell to the total number of circles. The annual mean radius of circles provided in 24-hour position forecasts was 86 km (89 km in 2022), and their hitting ratio was 80% (73%). The corresponding values for 48-hour forecasts were 148 km (159 km in 2022) and 76% (72%), those for 72-hour forecasts were 217 km (258 km in 2022) and 75% (85%), those for 96-hour forecasts were 284 km (385 km in 2022) and 68% (95%), and those for 120-hour forecasts were 370 km (564 km in 2022) and 61% (94%).

<sup>&</sup>lt;sup>7</sup> Probability circle: a circular range in which a TC is expected to be located with a probability of 70% at each forecast period

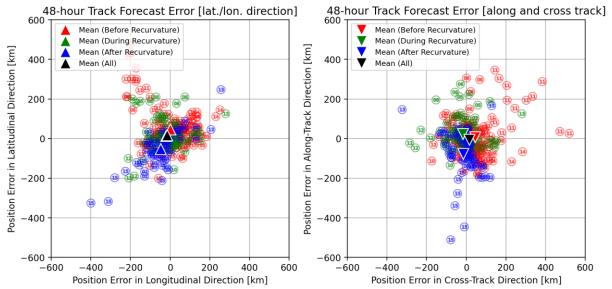


Figure 4.4 Scatter diagrams of 48-hour forecast position errors in longitudinal/latitudinal direction (left) and cross-/along-track direction (right) in 2023. (Scatter diagrams of 24-, 72-, 96- and 120-hour forecasts are available in Appendix 5.) Red, green and blue circles with TC numbers denote biases for each initial time in the stages before, during and after recurvature, respectively. Red, green and blue triangles indicate mean biases in the stages before, during and after recurvature, respectively. The definition of the stages is based on the direction of movement of each TC at individual prediction times (Figure 4.5). Black triangles indicate mean bias for all initial time.

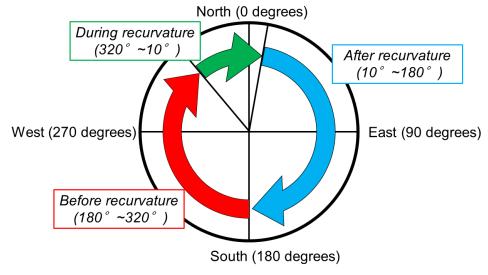


Figure 4.5 Definition of the stages before, during and after recurvature based on TC direction as calculated from positions at individual prediction times and those observed six hours prior.

Table 4.2 Mean hitting ratios (%) and radii (km) of 70% probability circles provided in 24-, 48-, 72-, 96- and 120-hour operational forecasts for each named TC that formed in 2023. Num. represents the number of samples.

			24-h	our Fo	recast	48-h	our Fo	recast	72-h	our Fo	recast	96-h	our Fo	recast	120-1	hour Fo	orecast
	Tropical C	yclone	Ratio	Num.	Radius	Ratio	Num.	Radius	Ratio	Num.	Radius	Ratio	Num.	Radius	Ratio	Num.	Radius
			(%)		(km)	(%)		(km)	(%)		(km)	(%)		(km)	(%)		(km)
TS	Sanvu	(2301)	100	2	106	-	0	- -	-	0	<del>-</del>	-	0	<del>-</del>	-	0	<del>-</del>
TY	Mawar	(2302)	84	50	70	78	46	124	76	42	199	76	38	281	82	34	407
TY	Guchol	(2303)	95	20	68	63	16	118	58	12	194	50	8	280	50	4	426
STS	Talim	(2304)	89	9	80	100	5	148	100	1	222	-	0	-	-	0	-
TY	Doksuri	(2305)	93	28	87	92	24	142	90	20	204	63	16	258	50	12	315
TY	Khanun	(2306)	84	49	76	71	45	123	66	41	182	46	37	244	30	33	312
TY	Lan	(2307)	91	33	70	93	29	126	100	25	203	100	21	282	100	17	360
TY	Dora	(2308)	57	7	104	100	3	167	-	0	-	-	0	-	-	0	-
TY	Saola	(2309)	82	34	81	80	30	145	88	26	218	91	22	276	67	18	342
STS	Damrey	(2310)	100	14	109	100	10	210	100	6	296	50	2	370	-	0	
TY	Haikui	(2311)	60	25	115	48	21	210	29	17	296	15	13	370	0	9	463
TS	Kirogi	(2312)	10	10	120	50	6	213	50	2	296	-	0	-	-	0	-
TS	Yun-yeun	ıg (2313)	38	8	120	50	4	213	-	0	=	-	0	-	-	0	=
TY	Koinu	(2314)	79	34	93	73	30	160	81	26	231	86	21	295	88	17	383
TY	Bolaven	(2315)	75	24	95	70	20	177	63	16	259	58	12	343	25	8	455
TS	Sanba	(2316)	50	4	96	-	0	-	-	0	-	-	0	-	-	0	-
TS	Jelawat	(2317)		0		_	0	=	_	0	=	_	0	=	-	0	
A	nnual Mea	n (Total)	80	351	86	76	289	148	75	234	217	68	190	284	61	152	370

#### 4.1.2 Central Pressure and Maximum Wind Speed

Figure 4.6 shows annual means of root mean square errors (RMSEs) for TC central pressure and maximum wind speed forecasts covering periods of 24 hours, 48 hours (since 2001), 72 hours (since 2003) 96 hours and 120 hours (since 2019). The values for maximum wind speed forecasts for individual TCs are available in Appendix 5.

Operational TC intensity forecasts have improved recently after a long period with no notable enhancement, although year-to-year fluctuations exist. The annual RMSEs of central pressure for 24-, 48-, 72- 96- and 120-hour forecasts were 12.8 hPa (13.7 hPa in 2022), 16.9 hPa (19.4 hPa), 18.0 hPa (21.3 hPa), 20.6 hPa (19.4 hPa) and 22.2 hPa (15.5 hPa), respectively. The corresponding values for maximum wind speed were 5.1 m/s (6.3 m/s in 2022), 7.2 m/s (8.7 m/s), 7.9 m/s (8.7 m/s), 9.2 m/s (7.7 m/s) and 10.4 m/s (6.0 m/s), respectively.

Figure 4.7 shows annual mean improvement ratios for central pressure and maximum wind speed forecasts in relation to a guidance model based on climatology and persistence (Statistical Hurricane Intensity Forecast; SHIFOR<sup>8</sup>) to highlight operational forecast skill. The values are defined as

### $\frac{\text{RMSE}(\text{SHIFOR}) - \text{RMSE}(\text{Operational})}{\text{RMSE}(\text{SHIFOR})}$

with positive/negative values indicating better/worse operational forecasts than SHIFOR predictions. The values for maximum wind speed forecasts are available in Appendix 5. It can be seen that the operational TC intensity forecasts have improved recently, with minimal year-to-year fluctuations. The annual mean improvement ratios of central pressure for 24-, 48-, 72-, 96- and 120-hour forecasts were 13% (7% in 2022), 18% (7%), 12% (9%), -6% (12%) and -9% (25%), respectively. The corresponding values of maximum wind were 17% (-3% in 2022), 26% (6%), 30% (19%), 22% (35%) and 14% (50%), respectively.

The details of errors in operational central pressure forecasts, including improvement ratios to SHIFOR for each named TC that formed in 2023, are summarized in Table 4.3. The data for maximum wind speed forecasts are available in Appendix 5. Forecasts for Koinu (2314) were characterized by large errors attributed to the difficulty of estimation for rapid intensification and weaking.

Figure 4.8 shows a histogram of maximum wind speed errors for 24-hour forecasts (Histograms for 48-, 72-, 96- and 120-hour forecasts are also available in Appendix 5). Approximately 56% (58% in 2022) of 24-hour forecasts had errors of less than  $\pm 3.75$  m/s, with figures of  $\pm 6.25$  m/s for 63% (64%) of 48-hour forecasts,  $\pm 6.25$  m/s for 59% (65%) of 72-hour forecasts,  $\pm 8.75$  m/s for 66% (77%) of 96-hour forecasts and  $\pm 8.75$  m/s for 60% (91%) of 120-hour forecasts.

<sup>&</sup>lt;sup>8</sup> The Center operates the SHIFOR model based on Jarvinen and Neumann (1979). The explanatory variables include TC analysis data (center position, central pressure and maximum sustained wind, and related temporal variation from best track data) and date. Multiple regression coefficients for the model were generated from best track data for named TCs forming between 1977 and 2010.

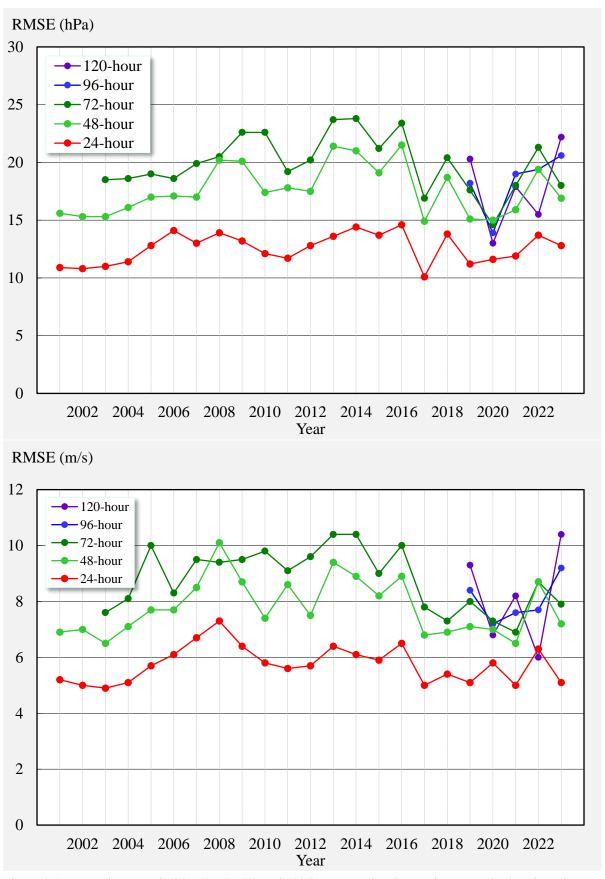


Figure 4.6 Annual RMSEs in 24-, 48, 72-, 96- and 120-hour operational central pressure (top) and maximum wind speed (bottom) forecasts

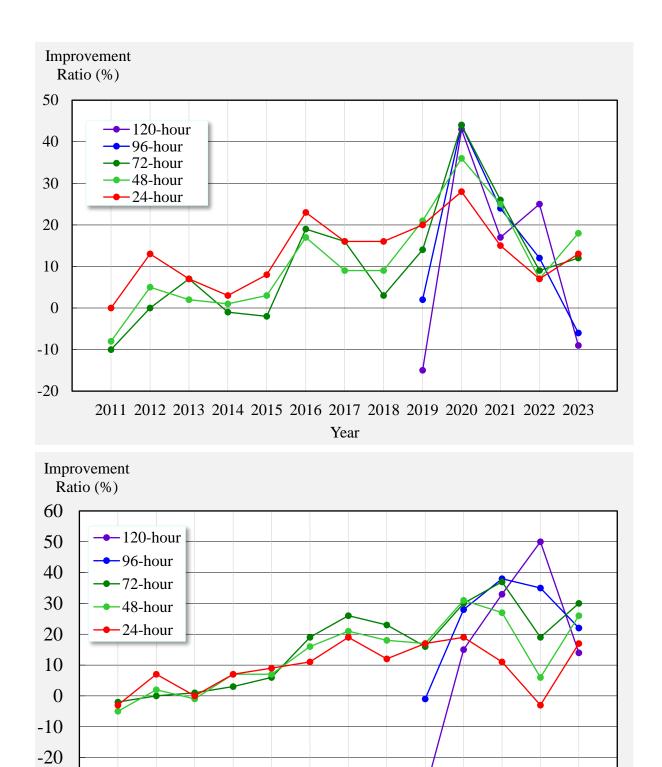


Figure 4.7 Annual mean improvement ratios in 24-, 48, 72-, 96- and 120-hour operational central pressure (top) and maximum wind speed (bottom) forecasts

2011 2012 2013 2014 2015 2016 2017 2018 2019 2020 2021 2022 2023

-30

-40

Table 4.3 Mean errors of 24-, 48-, 72-, 96- and 120-hour operational central pressure forecasts for each named TC that formed in 2023. Impr. and Num. represent improvement ratio of RMSEs (see the equation in 4.1.2 for detail) and the number of samples, respectively.

-			2	4-hour I	Forecas	st	4	8-hour F	Forecas	t	7	2-hour F	Forecas	st	9	6-hour I	Forecas	t	12	20-hour F	Forecas	st
	Tropical Cyc	lone	Error	RMSE	Num.	Impr.	Error	RMSE I	Num.	Impr.												
			(hPa)	(hPa)		(%)	(hPa)	(hPa)		(%)												
TS	Sanvu	(2301)	2.0	2.8	2	87	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	_
TY	Mawar	(2302)	3.6	17.8	50	-2	2.8	22.4	46	1	-2.7	21.2	42	-6	-5.1	21.3	38	-10	-3.4	21.6	34	5
TY	Guchol	(2303)	6.0	9.0	20	-8	2.8	7.2	16	42	-6.3	8.5	12	37	-15.6	18.8	8	-25	-21.3	21.9	4	-4
STS	Talim	(2304)	1.1	2.4	9	75	-2.0	3.2	5	70	-25.0	25.0	1	-52	-	-	0	-	-	-	0	-
TY	Doksuri	(2305)	-2.2	10.3	28	41	-0.9	12.0	24	41	0.3	13.2	20	40	4.4	14.9	16	32	0.8	13.1	12	20
TY	Khanun	(2306)	0.4	9.5	49	-6	-1.2	14.4	45	-10	-4.1	17.3	41	-6	-2.6	20.5	37	-27	0.3	24.2	33	-62
TY	Lan	(2307)	0.4	11.7	33	-17	-0.5	13.4	29	8	-4.0	11.8	25	12	-9.8	13.1	21	-55	-10.1	14.1	17	-90
TY	Dora	(2308)	-4.3	5.4	7	72	-7.3	8.4	3	78	-	-	0	-	-	-	0	-	-	-	0	-
TY	Saola	(2309)	5.1	17.9	34	-1	4.0	21.3	30	18	-2.2	19.9	26	24	5.4	22.8	22	24	17.7	26.7	18	27
STS	Damrey	(2310)	-0.6	6.4	14	14	2.4	6.2	10	61	5.7	6.5	6	77	9.5	10.1	2	68	_	-	0	
TY	Haikui	(2311)	3.2	10.9	25	21	3.6	13.7	21	19	4.8	14.8	17	-5	15.8	19.4	13	-46	15.8	18.8	9	-21
TS	Kirogi	(2312)	-3.2	3.9	10	73	-5.3	6.0	6	84	-4.0	4.0	2	92	-	-	0	-	-	-	0	-
TS	Yun-yeur	ış (2313)	-2.5	3.2	8	38	-4.5	4.6	4	69	-	-	0	-	-	-	0	-	-	-	0	-
TY	Koinu	(2314)	7.1	13.1	34	28	16.8	21.5	30	-9	19.4	24.9	26	-44	19.2	27.1	21	-90	15.8	28.7	17	-135
TY	Bolaven	(2315)	-3.3	17.1	24	12	-0.5	20.3	20	33	5.9	19.5	16	34	7.1	22.6	12	15	-0.6	15.7	8	18
TS	Sanba	(2316)	-2.0	2.4	4	73	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TS	Jelawat	(2317)	-	_	0	_	-	-	0	-	-	_	0		_	-	0	-	-	-	0	_
	Annual Mean (	Total)	1.7	12.8	351	13	2.5	16.9	289	18	0.7	18.0	234	12	1.5	20.6	190	-6	2.4	22.2	152	-9

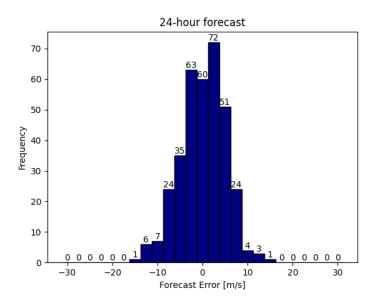


Figure 4.8 Histogram of 24-hour forecast maximum wind speed errors in 2023 (Histograms for 48-, 72-, 96- and 120-hour forecasts are also available at Appendix 5).

#### [Reference]

Aberson, S. D., 1998. Five-Day Tropical Cyclone Track Forecasts in the North Atlantic Basin, *Weather and Forecasting*, **13**, 1005-1015.

Jarvinen, B. R. and C. J. Neumann, 1979: Statistical forecasts of tropical cyclone intensity, *NOAA Tech. Memo. NWS NHC-10*, 22 pp.

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Merrill, R. T., 1980: A statistical tropical cyclone motion forecasting system for the Gulf of Mexico. *NOAA Tech. Memo. NWS NHC 14*, 21 pp.

#### 4.2 Verification of Timing of First-issued Operational Forecasts

The Center issues TC track forecasts with probability circles and intensity forecasts when a TC of TS intensity or higher is present or expected within 24 hours in its area of responsibility. Accordingly, initial forecasts for individual TCs are also used as 24-hour genesis forecasts in addition to track and intensity forecasts.

Table 4.4 shows differences between initial times of first forecast and upgrade times in best track data/real-time provisional analysis data for individual named TCs. Differences are almost the ideal for 24 hours.

Table 4.4 Lead times of operational forecasting for upgrade to TS intensity or higher. "First forecast", "Upgrade (Best/Prov.)" and "Lead time (Best/Prov.)" are the initial time of the first forecast for individual named TCs, the time when the TC was upgraded to TS intensity or higher in best track data/provisional analysis, and the time difference between the two, respectively.

-					_		
	Tropical Cy	clone	First Forecast	Upgrade (Best)	Upgrade (Prov.)	Lead Time (Best) Lead Tim	e (Prov.)
TS	Sanvu	(2301)	06UTC 19 Apr	12UTC 20 Apr	06UTC 20 Apr	30 h	24 h
TY	Mawar	(2302)	12UTC 19 May	12UTC 20 May	06UTC 20 May	24 h	18 h
TY	Guchol	(2303)	18UTC 05 Jun	12UTC 06 Jun	12UTC 06 Jun	18 h	18 h
STS	Talim	(2304)	00UTC 14 Jul	06UTC 15 Jul	06UTC 15 Jul	30 h	30 h
TY	Doksuri	(2305)	18UTC 19 Jul	00UTC 21 Jul	00UTC 21 Jul	30 h	30 h
TY	Khanun	(2306)	12UTC 26 Jul	00UTC 28 Jul	18UTC 27 Jul	36 h	30 h
TY	Lan	(2307)	00UTC 07 Aug	00UTC 08 Aug	00UTC 08 Aug	24 h	24 h
TY	Dora	(2308)	00UTC 12 Aug			h	h
TY	Saola	(2309)	18UTC 23 Aug	06UTC 24 Aug	06UTC 24 Aug	12 h	12 h
STS	Damrey	(2310)	00UTC 24 Aug	18UTC 24 Aug	18UTC 24 Aug	18 h	18 h
TY	Haikui	(2311)	00UTC 27 Aug	18UTC 28 Aug	00UTC 28 Aug	42 h	24 h
TS	Kirogi	(2312)	12UTC 29 Aug	12UTC 30 Aug	12UTC 30 Aug	24 h	24 h
TS	Yun-yeung	(2313)	00UTC 04 Sep	12UTC 05 Sep	12UTC 05 Sep	36 h	36 h
TY	Koinu	(2314)	06UTC 29 Sep	18UTC 29 Sep	18UTC 29 Sep	12 h	12 h
TY	Bolaven	(2315)	12UTC 06 Oct	12UTC 07 Oct	06UTC 07 Oct	24 h	18 h
TS	Sanba	(2316)	00UTC 17 Oct	00UTC 18 Oct	06UTC 18 Oct	24 h	30 h
TS	Jelawat	(2317)	00UTC 16 Dec	06UTC 17 Dec	00UTC 17 Dec	30 h	24 h

#### 4.3 Verification of Numerical Models (GSM, GEPS)

GSM and GEPS provide primary information for use by JMA forecasters in making operational TC track and intensity forecasts. The details of GSM and GEPS and information on recent related improvements are given in Appendix 7. GSM and GEPS predictions were verified with RSMC TC best track data and predictions using the persistency (PER) method. All TC forecast verifications were conducted for both systems.

#### 4.3.1 GSM Prediction

#### 1) Center Position

GSM annual mean position errors observed since 1997 are presented in Figure 4.9. In 2023, the annual mean errors for 30-, 54-, 78-, 102- and 126-hour<sup>9</sup> predictions were 85 km (96 km in 2022), 144km (156 km), 225km (232 km), 337km (266 km) and 466km (340 km), respectively. The mean position errors of 18-, 30-, 42-, 54-, 66-, 78-, 90-, 102-, 114- and 126-hour predictions for each named TC are given in Table 4.5.

Table 4.6 shows relative GSM performance compared with results obtained using the PER method<sup>10</sup>. In this comparison, TCs were classified into the three life stages of before, during and after recurvature. The definition of the stages is based on the direction of movement of each TC at individual prediction times (Figure 4.5). The table indicates that GSM results outperformed those of the PER method throughout the forecast period beyond 18 hours from the initial time, and that the ratios of error reduction for the GSM compared to the PER method were about 52% (59% in 2022), 64% (70%), 70% (76%), 69% (77%), 65% (81%) and 62% (81%) for 18-, 30-, 54-, 78-, 102- and 126-hour predictions, respectively.

About 87% (83% in 2022) of 30-hour predictions (histograms showing the position errors of 30-, 54-, 78-, 102- and 126-hour predictions are shown in Appendix 5) had errors of less than 150 km, while 92% (91%) of 54-hour predictions had errors of less than 300 km, and 92% (89%) of 78-hour predictions had errors of less than 450 km.

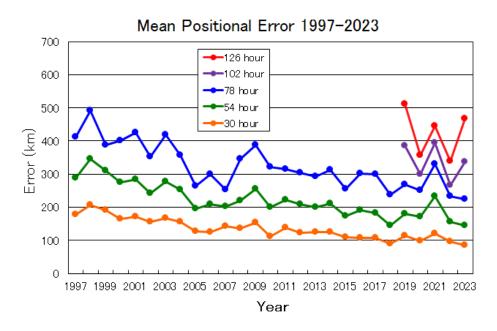


Figure 4.9 GSM annual mean position errors since 1997

<sup>&</sup>lt;sup>9</sup> 30-, 54-, 78-, 102- and 126-hour GSM predictions are used as primary information by forecasters creating 24-, 48-, 72-, 96- and 120-hour operational forecasts, respectively.

<sup>&</sup>lt;sup>10</sup> The PER method is based on the assumption that a TC holds the same movement throughout the forecast period, and linear extrapolation for the latest 12-hour track of the TC is applied to create TC track forecasts. Position errors with the PER method are used to evaluate the relative performance of operational forecasts and model predictions.

Table 4.5 GSM mean position errors (km) for each named TC that formed in 2023. The number of samples is given in parentheses.

Trop	ical Cyclo	ne	T=1	8	T=3	0	T=4	12	T=5	54	T=6	66	T=7	8	T=9	0	T=10	)2	T=11	14	T=12	6
TS	2301	SANVU	162.5	(8)	133.6	(6)	184.3	(4)	200.8	(2)	306.6	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2302	MAWAR	43.3	(54)	58.3	(52)	79.5	(50)	107.7	(48)	131.4	(46)	144.5	(44)	167.2	(42)	196.8	(40)	223.5	(38)	237.7	(36)
TY	2303	GUCHOL	48.2	(24)	53.2	(22)	77.8	(20)	130.6	(18)	199.5	(16)	271.2	(14)	346.0	(12)	433.4	(10)	537.4	(8)	681.8	(6)
STS	2304	TALIM	59.2	(14)	61.8	(12)	82.8	(10)	134.5	(8)	218.0	(6)	319.5	(4)	407.1	(2)	521.7	(1)	-	(-)	-	(-)
TY	2305	DOKSURI	45.8	(32)	65.6	(30)	86.1	(28)	113.3	(26)	142.5	(24)	190.3	(22)	248.7	(20)	311.5	(18)	352.4	(16)	375.3	(14)
TY	2306	KHANUN	68.5	(57)	91.5	(55)	119.9	(53)	162.1	(51)	193.0	(49)	230.1	(47)	281.3	(45)	337.7	(43)	398.9	(41)	482.4	(39)
TY	2307	LAN	50.9	(38)	58.2	(36)	66.9	(34)	71.3	(32)	81.5	(30)	108.0	(28)	130.2	(26)	155.7	(24)	196.5	(22)	253.2	(20)
TY	2308	DORA	84.2	(10)	107.0	(8)	139.3	(6)	178.4	(4)	162.9	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TY	2309	SAOLA	53.4	(37)	86.4	(35)	124.2	(33)	167.3	(31)	213.0	(29)	273.0	(27)	333.5	(25)	387.8	(23)	461.3	(21)	526.5	(19)
STS	2310	DAMREY	95.8	(18)	115.3	(16)	106.5	(14)	130.1	(12)	187.7	(10)	290.9	(8)	597.1	(5)	1430.8	(1)	-	(-)	-	(-)
TY	2311	HAIKUI	89.8	(32)	139.7	(30)	196.1	(28)	252.5	(26)	326.3	(24)	415.4	(22)	547.2	(20)	752.7	(18)	955.5	(16)	1270.0	(14)
TS	2312	KIROGI	82.1	(15)	127.4	(13)	156.0	(11)	189.0	(9)	256.0	(7)	294.1	(5)	290.9	(3)	192.5	(1)	-	(-)	-	(-)
TS	2313	YUN-YEUNG	112.0	(14)	137.6	(12)	157.8	(9)	180.9	(7)	161.1	(5)	270.9	(3)	623.2	(2)	-	(-)	-	(-)	-	(-)
TY	2314	KOINU	54.9	(38)	84.4	(36)	109.3	(34)	144.2	(32)	173.0	(30)	199.2	(28)	253.3	(25)	290.6	(22)	319.3	(17)	331.3	(15)
TY	2315	BOLAVEN	55.7	(29)	75.3	(27)	100.5	(25)	138.5	(23)	191.4	(21)	250.4	(19)	313.6	(17)	386.1	(15)	466.1	(13)	598.7	(11)
TS	2316	SANBA	57.4	(10)	101.4	(8)	151.9	(6)	188.8	(4)	228.9	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)
TS	2317	JELAWAT	140.3	(5)	102.8	(3)	158.9	(1)	-	(-)		(-)		(-)	-	(-)		(-)	-	(-)	-	(-)
All	Annual	Mean	64.7	(435)	85.4	(401)	110.6	(366)	144.3	(333)	181.0	(302)	224.8	(271)	283.0	(244)	337.3	(216)	393.6	(192)	466.2	(174)

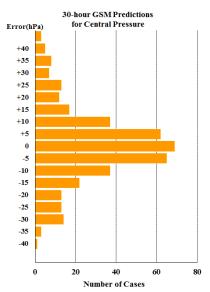
Table 4.6 Mean position errors (km) of GSM and PER method predictions for the 17 named TCs that formed in 2023 in the stages before, during and after recurvature. The number of samples is given in parentheses. IMPROV is the ratio of error reductions in GSM results to those observed using the PER method.

TIME	MODEL	Befor	e	Durin	g	After		A	11
T=18	GSM	61.2	(238)	66.8	(115)	71.5	(82)	64.7	(435)
	PER	114.0	(238)	136.8	(115)	191.8	(82)	134.7	(435)
	IMPROV	46.3	%	51.2	%	62.7	%	52.0	%
T=30	GSM	82.8	(217)	89.7	(107)	86.8	(77)	85.4	(401)
	PER	198.2	(217)	236.7	(107)	346.7	(77)	237.0	(401)
	IMPROV	58.2	%	62.1	%	75.0	%	64.0	%
T=42	GSM	112.1	(195)	110.6	(99)	106.7	(72)	110.6	(366)
	PER	300.2	(195)	349.4	(99)	518.4	(72)	356.5	(366)
	IMPROV	62.7	%	68.4	%	79.4	%	69.0	%
T=54	GSM	143.9	(171)	145.5	(94)	143.5	(68)	144.3	(333)
	PER	392.1	(171)	514.8	(94)	654.4	(68)	480.3	(333)
	IMPROV	63.3	%	71.7	%	78.1	%	70.0	%
T=66	GSM	184.2	(152)	169.7	(85)	188.0	(65)	181.0	(302)
	PER	495.0	(152)	660.8	(85)	816.8	(65)	610.9	(302)
	IMPROV	62.8	%	74.3	%	77.0	%	70.4	%
T=78	GSM	233.3	(134)	202.7	(76)	233.8	(61)	224.8	(271)
	PER	569.9	(134)	724.3	(76)	1083.	(61)	728.8	(271)
	IMPROV	59.1	%	72.0	%	78.4	%	69.2	%
T=90	GSM	293.1	(121)	240.5	(63)	307.2	(60)	283.0	(244)
	PER	674.6	(121)	776.4	(63)	1324.	(60)	860.8	(244)
	IMPROV	56.6	%	69.0	%	76.8	%	67.1	%
T=102	GSM	359.8	(111)	288.4	(52)	338.4	(53)	337.3	(216)
	PER	799.9	(111)	795.3	(52)	1440.	(53)	955.9	(216)
	IMPROV	55.0	%	63.7	%	76.5	%	64.7	%
T=114	GSM	426.5	(101)	342.8	(42)	369.2	(49)	393.6	(192)
	PER	936.4	(101)	888.1	(42)	1552.	(49)	1083.	(192)
	IMPROV	54.4	%	61.4	%	76.2	%	63.7	%
T=126	GSM	495.5	(92)	410.6	(35)	450.2	(47)	466.2	(174)
	PER	1065.	(92)	1016.	(35)	1635.	(47)	1209.	(174)
	IMPROV	53.5	%	59.6	%	72.5	%	61.5	%

#### 2) Central Pressure and Maximum Wind Speed

The mean errors of 30-, 54-, 78-, 102- and 126-hour GSM central pressure predictions in 2023 were +0.4 hPa (+6.7 hPa in 2022), -0.5 hPa (+8.8 hPa), -1.8 hPa (+9.5 hPa), -1.6 hPa (+7.3 hPa) and -2.6 hPa (+5.3 hPa), respectively. Their root mean square errors (RMSEs) were 15.3 hPa (15.7 hPa in 2022) for 30-hour predictions, 18.7 hPa (19.9 hPa) for 54-hour predictions, 23.8 hPa (22.1 hPa) for 78-hour predictions, 27.4 hPa (24.2 hPa) for 102-hour predictions and 27.5 hPa (20.4 hPa) for 126-hour predictions. The biases in 30-, 54-, 78-, 102- and 126-hour maximum wind speed predictions were -0.4 m/s (-6.0 m/s in 2022) with an RMSE of 8.1 m/s (9.8 m/s), -0.4 m/s (-7.1 m/s) with a RMSE of 10.0 m/s (12.2 m/s), -0.4 m/s (-7.2 m/s) with a RMSE of 12.2 m/s (12.7 m/s), -1.5 m/s (-5.9 m/s) with a RMSE of 13.3 m/s (13.2 m/s) and -1.9 m/s (-5.9 m/s) with a RMSE of 13.0 m/s (11.5 m/s), respectively.

Figure 4.10 shows histograms of central pressure errors and maximum wind speed errors in 30-hour GSM predictions. The GSM exhibited a small positive bias in central pressure prediction, and tended to underestimate the wind speed of TCs until 2022. However, these biases were smaller in 2023, probably in association to the GSM upgrade of March 2023, including horizontal resolution enhancement. The upgrade is detailed in Appendix 7.



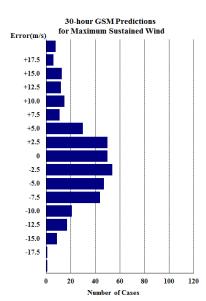


Figure 4.10 Error distribution of GSM 30-hour intensity predictions in 2023. The figure on the left shows error distribution for central pressure, while the one on the right shows that for maximum wind speed (the error distributions of 54-, 78-, 102- and 126-hour predictions are shown at the Appendix 5).

#### 4.3.2 GEPS Prediction

#### 1) Ensemble Mean Center Position

GEPS took over the role of the Typhoon Ensemble Prediction System (TEPS), and has been providing ensemble forecasts for TCs since January 2017. GEPS and TEPS annual mean position errors observed since 2008 are presented in Figure 4.11. In 2023, the mean position errors of GEPS ensemble mean forecasts for 30-, 54-, 78-, 102- and 126-hour predictions for each named TC are given in Table 4.7. The annual means of ensemble mean position errors for 30-, 54-, 78-, 102- and 126-hour predictions were 92 km (85 km with the GSM), 152 km (144 km), 230 km (225 km), 343 km (337 km) and 471 km (466 km), respectively.

#### Ensemble mean Positional Error 2008-2023

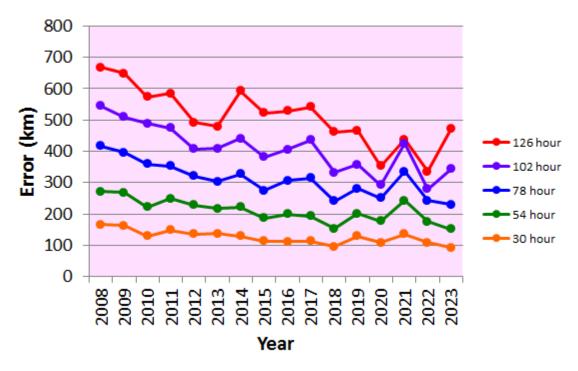


Figure 4.11 GEPS and TEPS annual mean position errors since 2008

Table 4.7 Mean position errors (km) of GEPS ensemble mean forecasts for each named TC that formed in 2023. The number of samples is given in parentheses.

Trop	ical Cycl	one	T=1	18	T=3	30	T=4	2	T=5	4	T=6	6	T=7	8	T=9	0	T=10	2	T=114	T=126
TS	2301	SANVU	138.6	(6)	198.4	(4)	265.0	(2)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	- (-)	- (-)
TY	2302	MAWAR	40.2	(55)	55.3	(53)	74.4	(51)	100.1	(49)	123.3	(47)	142.8	(45)	164.2	(43)	187.5	(41)	201.4 (39)	224.7 (37)
TY	2303	GUCHOL	56.7	(24)	68.7	(22)	95.5	(20)	154.2	(18)	225.7	(16)	293.1	(14)	360.4	(12)	438.9	(10)	527.0 (8)	634.7 (6)
STS	2304	TALIM	64.7	(15)	85.3	(13)	118.8	(11)	181.2	(9)	264.2	(7)	365.7	(5)	422.6	(3)	499.2	(1)	- (-)	- (-)
TY	2305	DOKSURI	46.0	(32)	66.9	(30)	88.7	(28)	106.5	(26)	124.7	(24)	149.2	(22)	191.1	(20)	231.4	(18)	262.5 (16)	277.1 (14)
TY	2306	KHANUN	68.0	(57)	92.3	(55)	122.1	(53)	160.2	(51)	193.2	(49)	239.4	(47)	298.6	(45)	367.2	(43)	447.0 (41)	527.0 (39)
TY	2307	LAN	53.5	(38)	64.0	(36)	80.2	(34)	87.7	(32)	101.3	(30)	128.1	(28)	159.2	(26)	188.6	(24)	207.7 (22)	217.5 (20)
TY	2308	DORA	68.7	(10)	65.7	(8)	56.9	(6)	67.5	(4)	141.1	(2)	-	(-)	-	(-)	-	(-)	- (-)	- (-)
TY	2309	SAOLA	60.3	(35)	90.2	(33)	125.9	(31)	166.4	(29)	209.6	(27)	259.2	(25)	311.3	(23)	376.4	(21)	453.2 (19)	541.0 (17)
STS	2310	DAMREY	103.2	(18)	129.3	(16)	125.0	(14)	128.5	(12)	184.8	(10)	239.5	(8)	457.6	(5)	1121.2	(1)	- (-)	- (-)
TY	2311	HAIKUI	94.4	(32)	138.6	(30)	195.0	(28)	258.2	(26)	334.7	(24)	423.3	(22)	531.3	(20)	713.2	(18)	940.7 (16)	1166.7 (14)
TS	2312	KIROGI	121.4	(15)	203.1	(13)	275.5	(11)	337.3	(9)	393.1	(7)	423.4	(5)	484.8	(3)	426.5	(1)	- (-)	- (-)
TS	2313	YUN-YEUNG	86.2	(14)	111.2	(12)	136.0	(10)	150.8	(8)	125.3	(6)	176.6	(4)	195.0	(2)	-	(-)	- (-)	- (-)
TY	2314	KOINU	60.2	(37)	89.0	(35)	112.9	(34)	137.1	(32)	164.8	(30)	191.2	(28)	246.5	(25)	302.7	(23)	379.3 (18)	449.4 (17)
TY	2315	BOLAVEN	59.5	(29)	85.1	(27)	126.5	(25)	191.3	(23)	260.1	(21)	329.8	(19)	412.6	(17)	513.4	(15)	618.2 (13)	755.2 (11)
TS	2316	SANBA	91.1	(10)	168.7	(8)	268.0	(5)	287.7	(2)	312.0	(1)	-	(-)	-	(-)	-	(-)	- (-)	- (-)
TS	2317	JELAWAT	135.1	(5)	158.7	(3)	195.7	(1)	-	(-)	-	(-)	-	(-)	-	(-)	-	(-)	- (-)	- (-)
All	Annual	Mean	67.1	(432)	92.2	(398)	119.8	(364)	151.5	(330)	188.7	(301)	230.2	(272)	283.4	(244)	342.6	(216)	404.6 (192)	470.7 (175)

#### 2) Spread-Skill Relationship

Although position errors of GEPS ensemble mean forecasts were larger than those of the GSM, GEPS provides useful information on the reliability of TC track forecasts with its ensemble spread. Figure 4.12 shows the relationship between 6-hourly cumulative ensemble spreads in TC position forecasts and ensemble mean forecast position errors in 126-hour prediction. In an ideal EPS with a large number of samples, significant positional errors are observed when the ensemble spread is large. However, no clear correlation is seen from the figure. One of the reasons why it is considered non-ideal is that the number of samples is not enough.

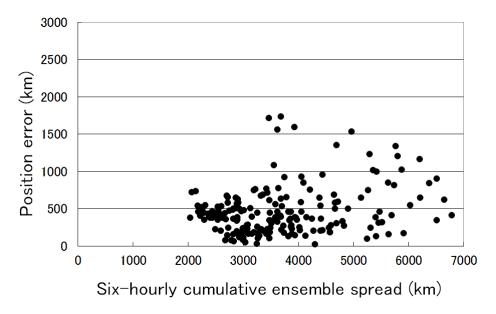


Figure 4.12 Relationship between six-hourly cumulative ensemble spread in TC position forecasts (km) and ensemble mean forecast position errors (km) in 126-hour predictions in 2023.

### 4.4 Verification for Other Guidance Models

### 4.4.1 Verification by WGNE

The Center utilizes other guidance models in addition to JMA's NWP models for operational TC track and intensity forecasting, including global deterministic NWP models from seven other centers (BOM, CMC, DWD, ECMWF, KMA, NCEP and UKMO). These models (as well as the Meteo France (FRN) model, the Naval Research Laboratory (NRL) model and National Centre for Medium Range Weather Forecasting (NCMRWF) model) are verified under the framework of WGNE (the Working Group on Numerical Experimentation), which is a collaborative working group for development of Earth system models (design, implementation, error diagnosis and model revision) across the full range of temporal and spatial scales. JMA works on inter-comparison of these models under the framework. Figures 4.13 and 4.14 show the results of the verification for center positions and 72-hour intensity forecasts by WGNE.

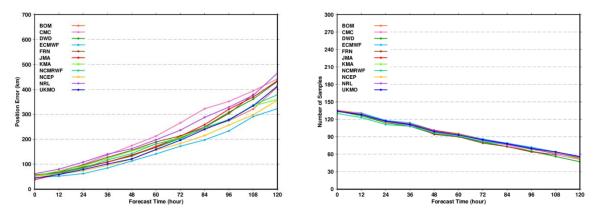


Figure 4.13 (Left) Positional errors for 2023 named TCs. The tropical depression (TD) stage and the extratropical cyclone (L) stage of targeted TCs is also included in this verification. (Right) Sample numbers.

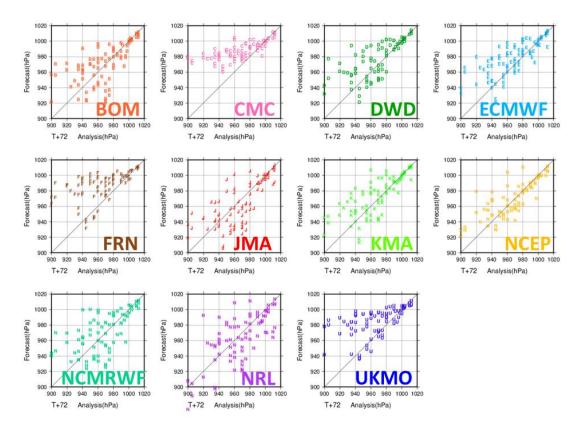


Figure 4.14 Scatter diagrams of 72-hour TC center pressure forecasts from 11 deterministic models for 2023. The tropical depression (TD) stage and the extra-tropical cyclone (L) stage of targeted TCs is also included in this verification.

# 4.4.2 Verification of Intensity Guidance Models

Intensity guidance

Consensus method TIFS&LGEM

TIFS

LGEM

0.6

0.6

351

351

351 0.7

0.3

Table 4.8 shows mean central pressure and maximum wind speed errors in TIFS and LGEM intensity guidance and related consensus. This section describes verification of the latest guidance data available for each initial time of real-time operation conducted for RSMC operational forecasting.

Table 4.8 Mean error and RMSE of central pressure (top) and maximum wind speed (bottom) forecasts from intensity guidance models produced by the Center in 2023. Num. represents number of samples.

·		24-h	our Fore	cast	48-h	our Fore	ecast	72-l	nour Fore	ecast	96-h	our Fore	cast	120-	hour For	ecast
Predict	ion	Error	RMSE	Num.	Error	RMSE	Num.	Error	RMSE	Num.	Error	RMSE	Num.	Error	RMSE	Num.
		(hPa)	(hPa)		(hPa)	(hPa)		(hPa)	(hPa)		(hPa)	(hPa)		(hPa)	(hPa)	
Intensity guidance	TIFS	-2.1	14.0	351	-2.3	16.4	289	-1.7	17.3	234	-0.2	19.3	188	2.9	21.5	149
model	LGEM	-0.1	13.9	351	-0.8	16.6	289	-1.8	16.6	234	-0.4	18.2	188	-	-	0
Consensus method	TIFS&LGEM	-1.1	13.5	351	-1.5	16.1	289	-1.7	16.6	234	-0.3	18.3	188	-	-	0
<u> </u>		24-	hour For	ecast	48-1	nour For	ecast	72-1	nour Fore	ecast	96-l	our Fore	cast	120-1	hour For	ecast
Predic	Error	RMSE	Num.	Error	RMSE	Num.	Error	RMSE	Num.	Error	RMSE	Num.	Error	RMSE	Num.	
		(m/s)	(m/s)		(m/s)	(m/s)		(m/s)	(m/s)		(m/s)	(m/s)		(m/s)	(m/s)	

289 -0.5

289

0.9

0.2

-1.8

-0.6

-1.2

234

7.9

8.7

8.8

188 -3.2

188

188

10.2

149

0

0

7.1

### 4.5 Verification of AMV-based Sea-surface Winds (ASWinds)

JMA produces Atmospheric Motion Vectors (AMVs) using successive satellite imagery from the Himawari-8/9 geostationary satellite. These are derived from the Full-disk observation conducted every 10 minutes and Region 3 tropical cyclone observation conducted over an area of 1,000 square kilometers every 2.5 – 5 minutes. Since July 2017, JMA has used the AMV-based Sea-surface Winds (ASWinds) product based on low-level AMVs (assigned below 700 hPa level) to estimate sea-surface winds in the vicinity of TCs. The ASWinds are derived at intervals of 10 – 30 minutes with frequent and wide-ranging wind distribution information. Figure 4.15 shows the distributions of ASWind derived using the Full-disk and Region 3 observations by Himawari-9 for TY Haikui (2311). The wide-area coverage and high temporal resolution of ASWinds data are also expected to support real-time determination of 30-kt wind radii for TC areas where low-level clouds appear in Himawari-8/9 imagery together with surface wind observations from satellite microwave scatterometers such as the ASCAT units on board MetOp polar-orbiting satellites (referred to here as "ASCAT winds").

JMA verified the quality of ASWinds data from Visible (B03:  $0.64~\mu m$ ), Short-wave Infrared (B07:  $3.9~\mu m$ ), and Infrared (B13:  $10.4~\mu m$ ) with respect to ASCAT wind data in the vicinity of 17 TCs occurring in 2023 (Table 4.9). Wind speed biases in ASWinds data from Full-disk and Region 3 observation were small at -0.6 to -0.4 m/s, and 0.0 to -0.5 m/s, respectively. Vector differences in ASWinds from Region 3 observation were slightly larger than those from Full-disk observation, which suggested that the use of high-frequency Region-3 observation data supports tracking to determine the movement of low-level cloud associated with mesoscale phenomena.

The mean distribution of ASWinds data from Full-disk and Region-3 observation (Figure 4.16) for 2023 suggests that the representation of Region-3 ASWinds is higher than that of Full-disk ASWinds, particularly near TC centers. This is attributed to the higher temporal frequency of Region-3 imagery.

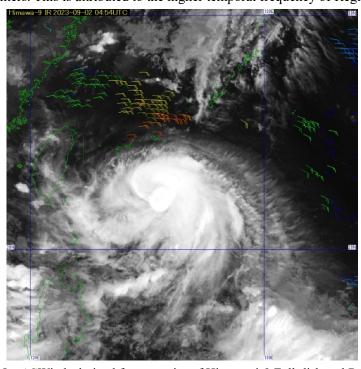


Figure 4.15 ASWinds derived from a series of Himawari-9 Full-disk and Region 3 Infrared (B13) and Shortwave Infrared (B07) images for TY Haikui (2311) at 0454 UTC on 2 September 2023.

Table 4.9 Vector Differences and biases of ASWinds (0.85 < QI) with reference to ASCAT winds within a square of 20 degrees centered at the TC center for 17 TCs in 2023.

# (a) ASWind (Full-disk)

	Number of	Vector Difference	Bias
	collocations	[m/s]	[m/s]
B03 (VIS)	275867	1.8	-0.4
B07 (SWIR)	244460	2.0	-0.6
B13 (IR)	222385	2.0	-0.6

# (b) ASWind (Region 3)

	Number of	Vector Difference	Bias
	collocations	[m/s]	[m/s]
B03 (VIS)	486919	3.1	0.5
B07 (SWIR)	529488	3.3	0.2
B13 (IR)	384599	3.1	0.0

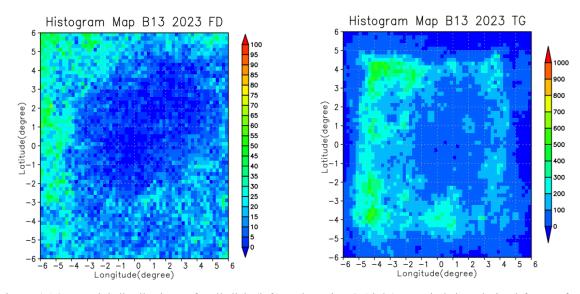


Figure 4.16 Spatial distributions of Full-disk (left) and Region 3 (right) ASWind data derived from Infrared (B13) images within a square of 12 degrees centered at TC center for 17 TCs in 2023.

#### 4.6 Verification of TC Central Pressure Estimates Based on Satellite Microwave Observations

JMA uses TC central pressure (Minimum Sea Level Pressure, or MSLP) estimates based on TC warm core intensity (i.e., the maximum temperature anomaly near the TC center) from microwave sounders on board polar-orbiting satellites as reference for JMA operational TC analysis. The Advanced Microwave Sounding Unit-A (AMSU-A) of the NOAA and MetOp series of polar-orbiting satellites has been used for MSLP estimation since 2013. JMA also began to use data from the Advanced Technology Microwave Sounder (ATMS) on board the Suomi-NPP and JPSS-1 (NOAA-20) satellites in 2015. The higher spatial resolution of ATMS observation (32 km at the sub-satellite point) as compared to AMSU-A (48 km) enables more accurate determination of warm core intensity. Figure 4.17 shows the MSLP estimates based on AMSU-A and ATMS observations (referred to here as AMSU/ATMS estimates) together with MSLP estimates based on the Dvorak technique (Dvorak estimates) and a product based on consensus between AMSU/ATMS estimates and Dvorak estimates (CONSENSUS) for TY Doksuri (2305).

Table 4.10 shows the results of AMSU and ATMS estimate verification with respect to JMA best track data for 2015 - 2023 together with Dvorak TC intensity estimates and CONSENSUS. The biases and root mean square errors (RMSEs) of AMSU estimates were -5.5 to 2.7 hPa and 10.0 to 14.0 hPa, respectively (Table 4.10a). It should be noted that the RMSE of CONSENSUS between AMSU estimates and Dvorak estimates is consistently smaller than that for AMSU and Dvorak estimates over a period of nine years, which is attributed to the benefits of independent information from the satellite microwave observation. The RMSE for ATMS estimates was smaller than that for AMSU (Table 4.10b), which indicates that the higher resolution of ATMS observation as compared to AMSU leads to more accurate determination of TC warm core intensity. As with the AMSU estimate result, the RMSEs of CONSENSUS between ATMS and Dvorak estimates were smaller than those of ATMS and Dvorak estimates. The superiority of CONSENSUS to individual estimates is seen in bias comparison.

Use of AMSU/ATMS estimates via CONSENSUS is expected to support JMA's operational TC intensity analysis, particularly when in-situ observation data are scarce and operational TC intensity analysis depends largely on the Dvorak estimates.

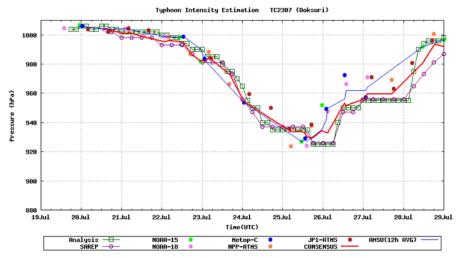


Figure 4.17 Time-series representation of Dvorak MSLP estimates, microwave-based MSLP estimates (AMSU and ATMS), CONSENSUS between Dvorak and AMSU/ATMS estimates and JMA analysis for TY Doksuri (2305) on the Numerical Typhoon Prediction (NTP) website

Table 4.10 (a) Bias and RMSE of Dvorak MSLP estimates, AMSU MSLP estimates and CONSENSUS between Dvorak and AMSU estimates with respect to the best track data for the previous nine years (2015 - 2023); (b) as per (a) but for ATMS estimates

# (a) BIAS and RMSE of central pressure estimates to best track for AMSU

	Year	2015	2016	2017	2018	2019	2020	2021	2022	2023
BIAS	AMSU	1.3	2.7	-2.9	-3.1	-2.5	-5.5	-2.9	-1.9	-0.6
(hPa)	Dvorak	0.1	-2.1	-2.0	-0.4	-2.9	-2.8	-2.1	-1.8	-0.3
	Consensus	0.3	-0.8	-2.6	-1.5	-3.2	-4.0	-2.8	-2.2	-0.8
RMSE	AMSU	12.8	13.8	10.0	12.4	11.7	14.0	13.1	11.3	12.6
(hPa)	Dvorak	7.5	9.6	7.2	7.0	9.2	8.4	7.9	6.5	8.6
	Consensus	6.8	8.2	6.7	6.7	7.6	7.9	6.6	6.3	6.2
Numb	per of Data	819	595	569	680	645	478	703	473	398

# (b) BIAS and RMSE of central pressure estimates to best track for ATMS

	Year	2015	2016	2017	2018	2019	2020	2021	2022	2023
BIAS	ATMS	3.0	4.1	1.8	0.9	1.9	0.9	1.7	1.1	2.9
(hPa)	Dvorak	-0.5	-1.4	-2.0	-0.9	-3.7	-3.6	-2.1	-2.7	-1.4
	Consensus	0.8	0.3	-0.7	-0.3	-1.9	-1.8	-0.9	-1.2	-0.1
RMSE	ATMS	11.9	13.0	8.7	11.4	9.9	9.0	10.9	8.1	11.8
(hPa)	Dvorak	7.8	8.5	7.9	7.9	9.7	9.6	8.5	8.0	8.3
	Consensus	6.1	7.1	6.3	7.0	7.1	6.0	6.0	5.7	5.4
Numl	per of Data	229	190	193	224	244	148	159	116	136

## 4.7 Verification of Storm Surge Prediction

Storm surge predictions have been provided since 2011 via the Numerical Typhoon Prediction (NTP) website to Typhoon Committee Members within the framework of the Storm Surge Watch Scheme (SSWS). The Asia-area storm surge ensemble prediction system has been operational and probabilistic forecast products have been provided since August 2022, with a forecast period extended to 132 hours. For details of the system and the new SSWS forecast products, refer to Hasegawa et al. (2023) on the NTP website. Verification of deterministic storm surge predictions was conducted on data from eight stations (Table 4.11) for which sea level observation information is provided on the University of Hawaii Sea Level Center (UHSLC) database website (<a href="http://uhslc.soest.hawaii.edu/data/?fd">http://uhslc.soest.hawaii.edu/data/?fd</a>) and the Global Sea Level Observing System (GLOSS) website (<a href="http://www.ioc-sealevelmonitoring.org/index.php">http://www.ioc-sealevelmonitoring.org/index.php</a>) for all named TCs that formed in 2023. Hourly hindcast data (from T = -5 to T = 0) and forecast data (from T = 1 to T = 132) were compared with observation data. Ensemble predictions were also verified with information including data from the Quarry Bay tide station (Hong Kong) for TY Saola (2309).

Table 4.11 Stations used for verification

	Station	Abbreviation	Member	Data Source
1	Quarry Bay	QB	Hong Kong	UHSLC
2	Shek Pik	SP	Hong Kong	GLOSS
3	Langkawi	LK	Malaysia	UHSLC
4	Legaspi Port	LG	Philippines	UHSLC
5	Manila South Harbor	ML	Philippines	UHSLC
6	Subic Bay	SB	Philippines	UHSLC
7	Busan	BS	Republic of Korea	GLOSS
8	Apra Harbor	AP	U.S.A.	UHSLC

Table 4.12 Storm surges exceeding 0.5 m observed at the eight stations for each named TC that formed in 2023

Station	Named TC	Storm surge [m]
BS	Khanun (2306)	0.59
QB	Saola (2309)	0.75
SP	Koinu (2314)	0.56

#### 4.7.1 Deterministic Prediction

Storm surges exceeding 1.0 m were not observed in any of eight stations in 2023 (Table 4.12). Figure 4.18 shows scatter diagrams of modeled storm surges (hindcast and forecast) against observation data. Verification results for 2023 (Figure 4.18) indicate that deterministic predictions tend to underestimate storm surges, which can be attributed to errors in official tracks, mainly for TY Saola.

The verification results shown in Figure 4.18 may be insufficient to evaluate model accuracy for TCs, given that there were sparse observation data for verification and remarkable storm surges were not observed at most stations. Accordingly, additional verification was conducted using data from stations in Japan, where sufficient observation data are available, and TCs frequently approach or make landfall in Japan. Although the characteristics of model forecasts may vary by region, the system is considered to have comparable accuracy at storm surge watch scheme stations.

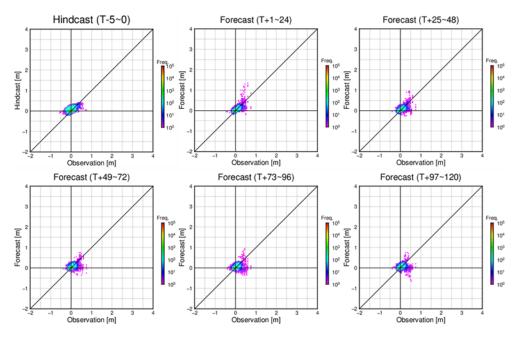


Figure 4.18 Scatter diagrams of modeled storm surges against observation data from eight stations for all the named TCs that formed in 2023 (top left: hindcast; others: forecast)

Figure 4.19 shows scatter diagrams of modeled storm surges (forecast) against observation data from around 200 stations (operated by JMA, the Ports and Harbours Bureau, the Japan Coast Guard, and the Geospatial Information Authority of Japan) in Japan. The verification period is from January to December 2023, and cases of TCs are extracted. Nine named TCs approached the country, including TY Lan (2307) making landfall. The diagrams indicate that forecasts for Japan compare well with observed storm surges, although some predictions exhibit significant errors (e.g., due to TY Khanun (2306)). Naturally, prediction errors increase with lead time.

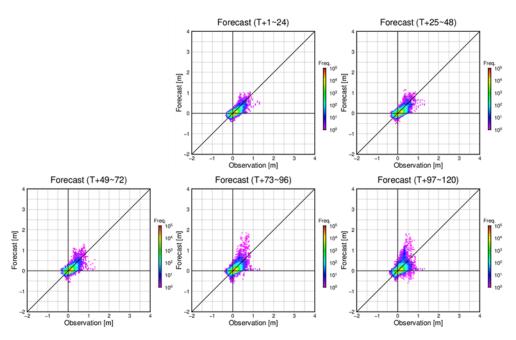


Figure 4.19 Scatter diagrams of modeled storm surges (forecast) against observation data from around 200 stations (operated by JMA, the Ports and Harbours Bureau, the Japan Coast Guard, and the Geospatial Information Authority of Japan) in Japan for TCs in 2023. All plots are three-hourly maximum values.

#### 4.7.2 Ensemble Prediction

Threat scores from ensemble prediction in Japan for TCs in 2023 (Figure 4.20; statistical period: as per deterministic forecast verification) generally peak in the probability range from 20 to 40%. The values are lower than expected even though the threshold is set low, and the effects of specific typhoons are significant. The results are probably affected by the low number of remarkable storm surges in 2023. The figures show that the system maintains scores of approximately 0.1 up to five days ahead.

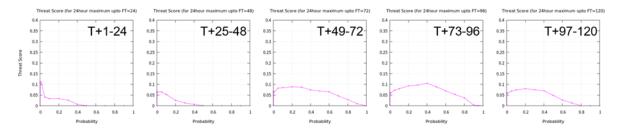


Figure 4.20 Threat scores of the ensemble prediction system for each probability against storm surges exceeding 0.5 m at around 200 stations in Japan in 2023.

## 4.7.3 Case Study

TY Saola (2309) passed through the Bashi Channel and moved westward over the South China Sea in August 2023, developing to a maximum wind speed of 55 m/s and a minimum pressure of 920 hPa. Figure 4.21 shows the analysis track and all predicted tracks (official forecast and 51 tracks calculated using GEPS) for the 72-hour period before the storm surge peak in Quarry Bay. The typhoon moved just south of Hong Kong, although many ensemble members with the initial time (00 UTC on 30 August 2023) had predicted eastern courses in this area. Accordingly, peak storm surges for these members were estimated to be lower and later than observed. Tracks of ensemble members were not uniformly predicted, highlighting uncertainties in TC track forecasting. Meanwhile, prediction for the peak storm surge in the official forecast was higher (maximum storm surge for Quarry Bay: 0.93 m (Figure 4.24); maximum storm tide: 3.14 m above mean sea level) than observation in Quarry Bay (maximum storm surge: 0.75 m; maximum storm tide: 3.04 m).

The ensemble system predicted a probability of storm surges exceeding 1.0 m along the eastern coast of Hong Kong (Figure 4.22), while no such surges were predicted for Quarry Bay (Figure 4.23). Accurate prediction of storm surges caused by TY Saola was challenging due to the uncertainty of TC track prediction (Figure 4.24).

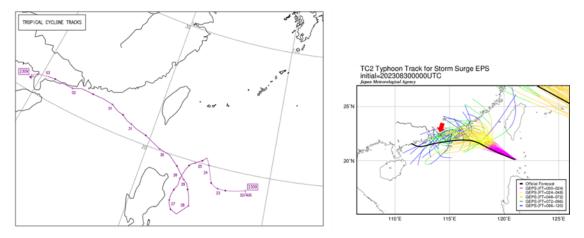


Figure 4.21 Analysis track (left) and predicted tracks (right) for TY Saola. In the figure on the right, colored lines show the 51 tracks from GEPS members, and the bold black line shows the official forecast. The red arrow shows the location of Quarry Bay.

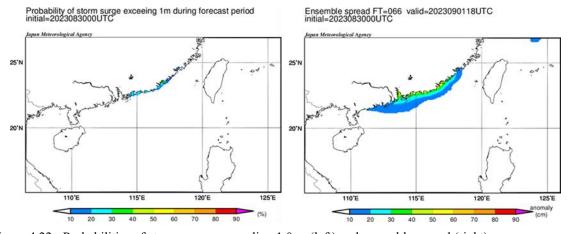


Figure 4.22 Probabilities of storm surges exceeding 1.0 m (left) and ensemble spread (right).

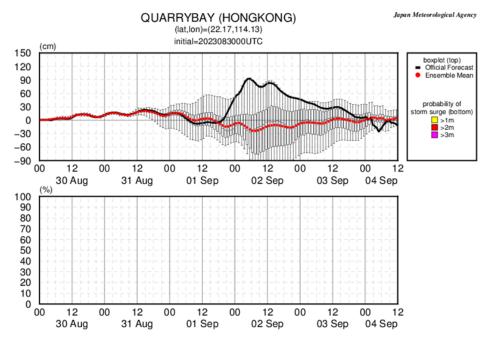


Figure 4.23 Time-series representation of storm surge boxplots (top), storm surge probability bars (bottom) for Quarry Bay.

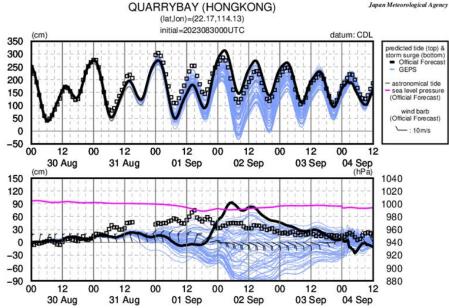


Figure 4.24 Time-series representation of storm tide and astronomical tide (top), storm surge, sea level pressure and surface wind (bottom) for Quarry Bay. Squares show hourly observation values.

## [Reference]

Hasegawa. H., N. Kohno, and H. Hayashibara, 2012: JMA's Storm Surge Prediction for the WMO Storm Surge Watch Scheme (SSWS). *RSMC Tokyo-Typhoon Center Technical Review*, **14**, 13-24.

Hasegawa. H., N. Kohno, M. Higaki, and M. Itoh, 2017: Upgrade of JMA's Storm Surge Prediction for WMO Storm Surge Watch Scheme (SSWS). *RSMC Tokyo-Typhoon Center Technical Review*, **19**, 26-34.

Hasegawa. H., J. Sugano, T. Fukuura and M. Higaki, 2023: Upgrade of JMA's Storm Surge Prediction for WMO Storm Surge Watch Scheme (SSWS) in 2022. RSMC Tokyo-Typhoon Center Technical Review, 25, 1-14.

# Appendices

Appendix 1
RSMC Tropical Cyclone Best Track Data in 2023

- Det	/Time	Center	Danitian	Central	Max Wind	CI num.	Grade	- Dete	/Time	Contor	Position	Central	Max Wind	Claum	Grade	Date/Time	Contor	Position	Central	May Wind	CI num.	Grade
Dati	(UTC)	Lat (N)		pressure (hPa)	(kt)	OI HUIII.	Graue	Date	(UTC)	Lat (N)		pressure (hPa)	(kt)	GI Huill.	Grade	(UTC)		Lon (E)	pressure (hPa)	(kt)	OI Hulli.	Grade
	(010)			NVU (2					(010)		Lon (E) Y MA	VAR (2				(010)			HOL (2			—
Apr.	19/00		159.6	1008	-	0.5	TD	May	19/18	6.1	149.6	1004	-	0.5	TD	Jun. 06/00	12.8	135.0	1004	-	0.0	TD
	19/06	4.3	159.1	1004	-	0.5	TD		20/00	6.1	149.4	1004	-	1.0	TD	06/06	13.1	135.1	1002	-	0.5	TD
	19/12	5.3	158.7	1008	_	1.0	TD		20/06	6.1	149.2	1004	-	1.5	TD	06/12	13.6	135.1	1000	35	1.0	TS
	19/18 20/00	6.9 8.1	158.0 157.8	1004 1006	_	1.5 1.5	TD TD		20/12 20/18	6.2 6.6	149.1 149.0	1000 994	35 45	2.0 2.5	TS TS	06/18 07/00	14.1 14.7	134.9 134.3	1000 998	35 40	1.5 2.0	TS TS
	20/06	9.1	157.1	1002	-	1.5	TD		21/00	7.0	148.7	992	50	3.0	STS	07/06	15.0	133.8	996	40	2.5	TS
	20/12	9.6	156.6	1000	35	2.0	TS		21/06	7.3	148.4	992	50	3.0	STS	07/12	15.1	133.2	992	45	2.5	TS
	20/18 21/00	9.9 10.1	156.3 156.0	998 998	40 40	2.5 2.5	TS TS		21/12 21/18	7.6 7.9	147.9 147.6	990 980	55 65	3.5 4.0	STS TY	07/18	15.5	132.4	990	50	3.0	STS
	21/06	10.1	155.7	996	45	3.0	TS		22/00	8.6	147.3	980	65	4.0	TY	08/00 08/06	15.8 16.0	131.6 131.1	985 980	55 60	3.5 4.0	STS STS
	21/12	10.4	155.3	1000	40	3.0	TS		22/06	9.2	147.1	975	70	4.5	TY	08/12	16.3	130.8	970	70	4.5	TY
	21/18	10.4	154.5	1002	35 -	3.0	TS		22/12	9.8	146.9	970	75	5.0	TY	08/18	16.8	130.4	965	75	5.0	TY
	22/00 22/06	10.3 10.3	153.8 153.1	1006 1004	_	2.5	TD TD		22/18 23/00	10.5 11.2	146.9 146.9	940 940	95 95	6.0 6.0	TY TY	09/00	17.2	130.4	965	75 75	5.0	TY
	22/12						Dissip.		23/06	11.8	146.5	920	105	7.0	TY	09/06 09/12	17.8 18.1	130.1 129.9	965 965	75 75	5.0 5.0	TY TY
									23/12	12.2	146.0	920	105	7.0	TY	09/18	18.5	129.9	960	80	5.0	TY
									23/18 24/00	12.5 13.1	145.7 145.5	920 935	105 95	7.0 6.0	TY TY	10/00	18.9	129.9	960	80	5.0	TY
									24/06	13.6	145.2	935	95	6.0	TY	10/06	19.9	130.2	960	80 75	5.0	TY TY
									24/12	13.8	144.7	935	95	6.0	TY	10/12 10/18	20.7 21.8	130.5 131.1	960 965	75 70	4.5 4.5	TY
									24/18	14.1	144.1	935	95	6.0	TY	11/00	23.0	131.7	970	65	4.0	TY
									25/00 25/06	14.2 14.6	143.5 142.8	925 905	100 110	6.5 7.0	TY TY	11/06	24.2	132.6	975	60	4.0	STS
									25/12	14.8	141.5	900	115	7.5	TY	11/12 11/18	25.6 26.4	133.8 135.3	980 980	55 55	4.0 3.5	STS STS
									25/18	14.9	140.4	900	115	7.5	TY	12/00	27.9	136.9	980	55	3.5	STS
									26/00 26/06	15.1 15.4	139.2 137.9	900 900	115 115	7.5 7.5	TY TY	12/06	29.5	138.1	985	50	3.5	STS
									26/12	15.7	136.5	900	115	7.5	TY	12/12	30.5	139.5	990	-	2.5	L
									26/18	16.0	134.9	900	115	7.5	TY	12/18 13/00	32.0 33.6	142.0 144.0	990 992	-	2.0	L L
									27/00	16.4	133.5	910	105	7.0	TY TY	13/06	34.5	146.4	992	_	-	Ĺ
									27/06 27/12	16.6 16.8	132.2 130.9	925 945	95 85	6.0 5.5	TY	13/12	35.8	148.8	996	-	-	L
									27/18	17.1	129.7	945	85	5.5	TY	13/18	38.1	152.0	996	-	-	L
									28/00	17.2	128.7	945	85	5.5	TY	14/00 14/06	38.5 39.1	155.0 158.5	996 996	_	_	L L
									28/06 28/12	17.6 18.0	127.9 127.4	945 945	85 85	5.5 5.5	TY TY	14/12	39.3	162.0	996	-	-	L
									28/18	18.6	126.7	945	85	5.5	TY	14/18	39.0	166.5	998	-	-	L
									29/00	19.0	126.2	945	85	5.5	TY	15/00 15/06	38.7 38.9	169.5 171.0	998 996	_	_	L
									29/06	19.4	125.8	945	85	5.5	TY	15/12	38.9	171.0	994	_	_	L
									29/12 29/18	19.7 20.1	125.6 125.4	945 945	85 85	5.5 5.5	TY TY	15/18	39.3	174.5	990	-	-	L
									30/00	20.3	125.1	950	80	5.0	TY	16/00	39.2	176.5	986	-	-	L
									30/06	20.6	125.0	950	80	5.0	TY	16/06 16/12	39.6 39.6	178.1 179.6	984 984	_	_	L L
									30/12 30/18	20.8 21.2	125.0 125.0	955 955	70 70	4.5 4.5	TY TY	16/18	39.7	180.9	986	-	_	Out
									31/00	21.4	125.1	955	70	4.5	TY							
									31/06	22.2	125.3	960	65	4.0	TY							
									31/09 31/12	22.5 22.7	125.4 125.4	960 960	65 65	4.0	TY TY							
									31/12	23.0	125.4	960	65	-	TY							
									31/18	23.6	125.6	965	60	3.5	STS							
									31/21	23.8	125.7	965	60	-	STS							
								Jun.	01/00 01/03	24.1 24.6	125.8 126.0	970 970	50 50	3.0	STS STS							
									01/06	24.9	126.1	970	50	3.0	STS							
									01/09	25.4	126.6	970	50	-	STS							
									01/12 01/15	25.9 26.4	127.1 127.6	970 970	50 50	3.0	STS							
										26.9		970	50	3.0	STS STS							
									01/21	27.2	128.8	970	50	-	STS							
									02/00		129.4	975	45	2.5	TS							
									02/06 02/12	28.2 28.9	131.0 132.8	975 980	45 45	2.5 2.5	TS TS							
									02/12		135.2	980	45	2.5	TS							
									03/00		137.8	984	-	2.0	L							
									03/06 03/12		140.8 144.7	990 996	-	1.5	L L							
									03/12	55.7	144./	220	-	_	L Dissip.							

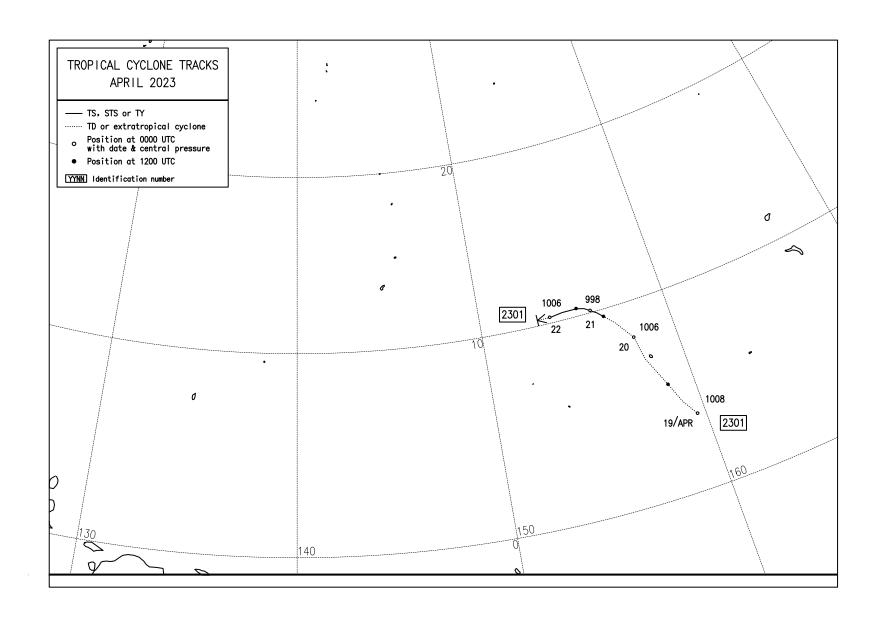
_				Central					·-		D 111	Central				09/00	30.9	129.3	970	50	3.5	STS
Dat	e/Time		Position	pressure	Max Wind	CI num.	Grade	Dat	e/Time	Center		pressure	Max Wind	GI num.	Grade	09/03	31.3	129.0	970	50	-	STS
	(UTC)	Lat (N)		(hPa)	(kt)				(UTC)	Lat (N)		(hPa)	(kt)			09/06	31.6	128.9	970	50	3.5	STS
lot	13/06	15.7	122.3	1002	.304)	1.0	TD	Jul.	26/18	10.5	138.1	1006	-	0.0	TD	09/09	31.9	128.8	970	50	-	STS
oui.	13/12	16.4	122.3	1002	_	1.0	TD	oui.	27/00	10.9	137.7	1006	-	0.0	TD	09/12 09/15	32.4 32.7	128.8 128.6	975 975	50 50	3.0	STS STS
	13/18	16.9	122.1	1000	-	1.0	TD		27/06	11.2	137.2	1004	-	0.5	TD	09/18	33.4	128.6	975	50	2.5	STS
	14/00	18.1	121.5	1000	-	1.0	TD		27/12	11.6	136.9	1004	-	1.0	TD	09/21	34.1	128.6	975	50	-	STS
	14/06 14/12	17.9	120.3	1000	_	1.5	TD		27/18 28/00	12.2 12.8	136.6 136.3	1002 1000	35	1.5 2.0	TD TS	10/00	34.8	128.7	980	45	2.0	TS
	14/12	17.4 17.8	119.3 118.6	998 996	_	1.5 1.5	TD TD		28/00	13.5	135.9	998	35 35	2.0	TS	10/06	36.6	128.1	986	-	2.0	L
	15/00	18.2	118.1	996	-	1.5	TD		28/12	14.1	135.5	998	35	2.0	TS	10/12 10/18	38.0 38.4	128.3 126.5	992 994	_	1.5 1.5	L L
	15/06	18.2	117.8	992	35	2.0	TS		28/18	14.9	134.7	996	40	2.0	TS	11/00	38.7	125.9	996	-	-	L
	15/12	18.3	117.0	990	40	2.5	TS		29/00	15.6	134.1	996	40	2.0	TS	11/06	39.2	124.9	996	-	-	L
	15/18 16/00	18.6	116.7	985	45 50	3.0 3.5	TS STS		29/06 29/12	16.1 16.8	133.8 133.6	992 985	45 50	2.5 3.0	TS STS	11/12	38.8	124.0	998	-	-	L
	16/06	18.8 19.2	116.1 115.3	980 980	50	3.5	STS		29/18	17.6	133.1	980	55	3.5	STS	11/18	37.6	124.9	1002	-	-	L
	16/12	19.5	114.6	980	50	3.5	STS		30/00	18.4	132.9	970	65	4.0	TY	12/00						Dissip.
	16/18	19.7	113.8	975	55	3.5	STS		30/06	19.6	132.7	965	70	4.5	TY							
	17/00	20.1	113.0	970	60	4.0	STS		30/12	20.3	132.4 132.1	960 950	75 80	5.0	TY							
	17/06 17/12	20.7 21.2	112.1 110.8	970 970	60 60	3.5 3.5	STS STS		30/18 30/21	21.1 21.5	132.1	950	80	5.0	TY TY	Date/Time	Center	Position	Central	Max Wind	CI num.	Grade
	17/12	21.4	109.7	975	55	3.5	STS		31/00	22.0	132.0	945	85	5.5	TY	(UTC)	Lat (N)		pressure (hPa)	(kt)		
	18/00	21.7	108.8	980	50	3.0	STS		31/03	22.4	131.8	945	85	-	TY	(010)	Lac (14)		N (230	_		
	18/06	22.4	107.5	985	45	2.5	TS		31/06	22.8	131.6	945	85	5.5	TY	Aug. 07/00	22.5	149.0	1004	-	1.0	TD
	18/12	22.0	106.3	996	-	2.0	TD		31/09 31/12	23.1 23.4	131.3 131.1	945 935	85 90	6.0	TY TY	07/06	22.8	149.4	1002	-	1.5	TD
	18/18 19/00	22.1	105.8	1000	-	-	TD Dissip.		31/15	23.8	130.7	935	90	-	TY	07/12	23.1	149.8	1004	-	2.0	TD
	. 10, 00						Влоопр.		31/18	24.1	130.3	935	90	6.0	TY	07/18	23.6	149.9	1002	-	2.0	TD
									31/21	24.4	129.8	935	90	-	TY	08/00 08/06	23.9 24.2	149.4 148.8	1000 996	35 40	2.5 2.5	TS TS
								Aug.	01/00	24.6	129.4	930	95 95	6.0	TY	08/00	24.4	148.3	992	45	3.0	TS
Dat	e/Time	Center	Position	Central	Max Wind	CI num.	Grade		01/03 01/06	24.8 25.0	129.0 128.7	930 930	95 95	6.0	TY TY	08/18	24.4	147.6	992	45	3.0	TS
	(UTC)		Lon (E)	pressure (hPa)	(kt)				01/09	25.2	128.4	930	95	-	TY	09/00	24.3	146.9	990	50	3.0	STS
				SURI (					01/12	25.3	128.0	930	95	6.0	TY	09/06	24.6 24.8	146.1	985 980	50 55	3.0	STS STS
Jul.	20/06	12.6	133.7	1004	-	0.5	TD		01/15	25.3	127.6	930	95	-	TY	09/12 09/18	25.0	145.4 144.7	980	55 60	3.5 4.0	STS
	20/12	13.2	133.7	1006	-	1.0	TD		01/18 01/21	25.5 25.7	127.4 127.0	935 935	90 90	5.5 -	TY TY	10/00	25.2	143.9	970	65	5.0	TY
	20/18	13.7	133.5	1004		1.5	TD		02/00	25.7	126.9	935	90	5.5	TY	10/06	25.5	143.5	960	75	5.0	TY
	21/00	13.8	133.0	1002	35	2.0	TS		02/03	26.1	126.5	935	90	-	TY	10/09	25.8	143.4	955	80		TY
	21/06 21/12	13.9 14.0	132.8 132.5	1002 1002	35 35	2.0 2.0	TS TS		02/06	26.1	126.1	935	90	5.5	TY	10/12 10/15	26.0 26.2	143.2 143.0	950 950	85 85	5.5	TY TY
	21/18	14.2	132.2	1002	35	2.0	TS		02/09	26.1	125.8	935	90	-	TY	10/13	26.4	142.9	940	90	6.0	TY
	22/00	14.3	131.7	998	40	2.5	TS		02/12 02/15	26.2 26.2	125.6 125.3	935 935	90 90	5.5	TY TY	10/21	26.6	143.0	940	90	-	TY
	22/06	14.3	131.0	998	40	2.5	TS		02/18	26.5	125.0	935	90	5.5	TY	11/00	26.9	142.9	940	90	6.0	TY
	22/12	14.4	130.3	994	45	2.5	TS		02/21	26.5	124.8	935	90	-	TY	11/03	27.1	142.9	940	90	-	TY
	22/18 23/00	14.6 14.7	129.7 129.0	990 985	50 55	3.0 3.5	STS STS		03/00	26.6	124.7	940	85	5.5	TY	11/06 11/09	27.4 27.7	142.9 142.9	940 940	90 90	6.0	TY TY
	23/06	14.9	128.3	980	60	3.5	STS		03/03 03/06	26.7 26.6	124.5	940	85	-	TY TY	11/12	27.7	142.6	940	90	6.0	TY
	23/12	15.0	127.8	980	60	3.5	STS		03/00	26.6	124.2 124.2	945 945	80 80	5.0	TY	11/15	28.0	142.4	940	90	-	TY
	23/18	15.1	127.0	970	70	4.5	TY		03/12	26.6	124.2	960	70	4.5	TY	11/18	28.2	142.4	950	85	5.5	TY
	24/00	15.2	126.6	965	75	5.0	TY		03/15	26.7	124.3	960	70	-	TY	12/00	28.6	141.9	950	85	5.5	TY
	24/06 24/12	15.7 16.5	126.3 125.8	950 940	85 90	5.5 6.0	TY TY		03/18	26.8	124.3	965	65	4.0	TY	12/06 12/12	28.9 29.1	141.4 140.7	950 955	85 80	5.5 5.0	TY TY
	24/18	16.9	125.1	925	100	6.5	TY		03/21 04/00	26.9 27.0	124.4 124.5	965 970	65 60	3.5	TY STS	12/18	29.3	140.7	965	75	4.5	TY
	25/00	17.6	124.6	925	100	6.5	TY		04/03	27.0	124.8	970	60	-	STS	13/00	29.8	139.6	965	75	4.5	TY
	25/06	18.3	123.7	925	100	6.5	TY		04/06	27.2	125.1	970	60	3.5	STS	13/06	30.3	138.9	965	75	4.5	TY
	25/12 25/18	18.9 19.0	122.7 121.6	925 925	100 100	6.5 6.5	TY TY		04/09	27.3	125.5	970	60	-	STS	13/12	30.7	138.6	965	75 70	4.5	TY
	26/00	18.9	121.4	940	90	5.5	TY		04/12 04/15	27.5 27.5	125.7 126.0	970 970	60 60	3.0	STS STS	13/18 14/00	31.2 31.8	138.1 137.5	970 970	70	4.5 4.5	TY TY
	26/06	19.3	121.0	950	85	5.5	TY		04/18	27.7	126.4	970	55	3.0	STS	14/03	32.0	137.2	970	70	-	TY
	26/12	19.5	120.6	955	80	5.0	TY		04/21	27.8	126.6	970	55	-	STS	14/06	32.3	136.9	970	65	4.0	TY
	26/18	20.0	120.0	955	80	5.0	TY		05/00	27.7	126.8	970	55	3.0	STS	14/09	32.6	136.8	970	65	-	TY
	27/00 27/06	20.7 21.1	119.8 119.3	955 955	75 75	4.5 4.5	TY TY		05/03	27.7	127.2	970	55 50	- 2.0	STS	14/12 14/15	32.8 33.0	136.6 136.4	975 975	60 60	3.5	STS STS
	27/12	21.8	119.1	955	80	5.0	TY		05/06 05/09	27.8 27.8	127.6 128.1	970 970	50 50	3.0	STS STS	14/15	33.3	136.4	975	60	3.0	STS
	27/18	22.8	118.9	955	80	5.0	TY		05/12	27.8	128.4	970	50	3.0	STS	14/19	33.5	136.0	975	60	-	STS
	28/00	24.2	118.8	965	70	5.0	TY		05/15	27.9	128.7	970	50	-	STS	14/21	33.7	135.8	975	60	-	STS
	28/06	25.3	118.3	985	50 40	4.5	STS		05/18	28.0	128.9	970	50	3.0	STS	15/00	34.1	135.3	980	55	3.0	STS
	28/12 28/18	27.1 28.9	117.9 117.0	994 996	40 35	4.0 3.5	TS TS		05/21	27.9	129.0	970	50 50	- 2.0	STS STS	15/03 15/04	34.5 34.7	135.0 134.9	985 985	50 50	_	STS STS
	29/00	30.6	115.1	998	-	3.0	TD		06/00 06/03	27.8 27.8	129.5 129.7	970 970	50 50	3.0	STS	15/04	35.1	134.9	985	50	2.5	STS
	29/06	31.9	114.7	998	-	-	TD		06/06	27.8	129.9	970	50	3.0	STS	15/09	35.4	134.8	990	45	-	TS
	29/12	33.0	114.5	998	-	-	TD		06/09	27.8	130.3	970	50	-	STS	15/12	36.0	134.7	990	45	2.5	TS
	29/18	33.8	114.4	998	_	_	TD		06/12	27.4	130.4	970	50	3.0	STS	15/18	37.0	134.8	990	40	2.0	TS
	30/00 30/06	35.4 36.1	114.0 113.7	1000 1000	_	_	TD TD		06/15	27.4	130.7	970 970	50 50	- 2.0	STS STS	16/00 16/06	38.2 39.7	135.5 136.1	990 990	40 40	2.0 2.0	TS TS
	30/00	36.7	113.7	1000	_	_	TD		06/18 06/21	27.5 27.6	130.9 131.0	970	50 50	3.0	STS	16/06	40.6	136.6	990	40	2.0	TS
	30/18						Dissip.		07/00	27.8	131.2	970	50	3.0	STS	16/18	42.0	137.7	990	40	2.0	TS
									07/03	27.9	131.2	970	50	-	STS	17/00	44.2	138.4	990	40	1.5	TS
									07/06	27.9	131.1	970	50	3.0	STS	17/06	44.8	139.4	990	-	1.5	L
									07/09	28.0	131.1	970	50 45	- 2.0	STS	17/12 17/18	45.8 46.9	141.1	992 992	_	-	L L
									07/12 07/15	28.2 28.3	131.1 131.1	975 975	45 45	3.0	TS TS	17/18 18/00	46.9	144.2 147.5	992	_	_	L
									07/18	28.4	131.1	975	45	3.0	TS	18/06	48.5	150.6	998	-	-	L
									07/21	28.6	131.1	975	45	-	TS	18/12	49.2	154.3	1000	-	-	Ĺ
									08/00	28.9	131.0	975	45	3.0	TS	18/18						Dissip.
									08/03	29.1	130.9	975	45 50	- 2 5	TS							
									08/06 08/09	29.4 29.7	130.7 130.6	970 970	50 50	3.5	STS STS							
									08/12	29.9	130.4	970	50	3.5	STS							
									08/15	30.2	130.1	970	50	-	STS							
									08/18	30.4	129.7	970	50	3.5	STS							
									08/21	30.6	129.5	970	50	-	STS							

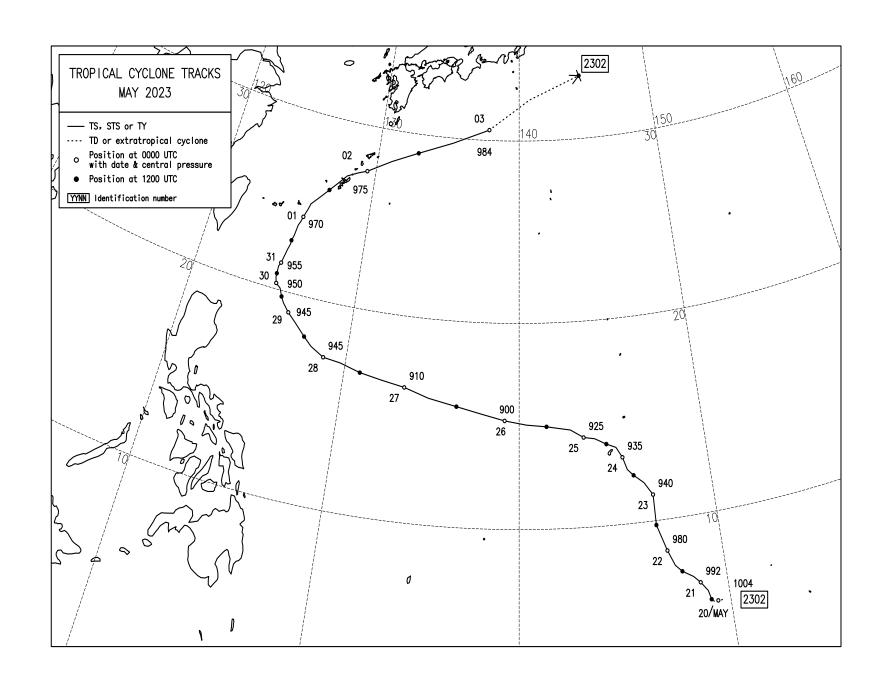
				Central								Central								Central			
Date	e/Time		Position	pressure		CI num.	Grade	Date	e/Time		Position	pressure	Max Wind	CI num.	Grade	Dat	e/Time		Position	pressure	Max Wind	CI num.	Grade
	(UTC)		Lon (E)	(hPa)	(kt)				(UTC)		Lon (E)	(hPa)	(kt)				(UTC)		Lon (E)	(hPa)	(kt)		
۸۰۰۰	12/00	15.6	180.1	RA (230 975	80	5.0	Out	Aug.	22/00	18.8	128.3	DLA (23 1006	-	0.0	TD	Aug.	23/18	16.9	5 DAN 151.6	1REY (2 1002	2310)	_	TD
Aug.	12/06	16.3	179.1	980	75	5.0	TY	, tug.	22/06	18.6	127.5	1004	-	0.5	TD	Aug.	24/00	17.1	152.0	1002	_	0.0	TD
	12/12	17.0	178.0	980	75	5.0	TY		22/12	18.5	126.8	1004	-	1.0	TD		24/06	17.3	152.4	1000	-	0.5	TD
	12/18	17.8	176.9	980	75	5.0	TY		22/18	18.5	126.5	1004	_	1.0	TD		24/12	17.6	153.1	1002	-	1.0	TD
	13/00 13/06	18.1 18.1	175.4 174.1	985 990	70 65	4.5 4.0	TY TY		23/00 23/06	18.5 18.6	126.2 125.9	1006 1004	_	1.5 1.5	TD TD		24/18 25/00	18.0 18.7	153.8 154.7	998 998	35 35	1.5 2.0	TS TS
	13/12	18.1	172.7	994	55	3.5	STS		23/12	18.8	125.6	1006	-	1.5	TD		25/06	20.0	155.5	994	40	2.0	TS
	13/18	18.3	171.4	998	50	3.0	STS		23/18	19.5	125.3	1004	-	1.5	TD		25/12	21.5	155.3	994	40	2.0	TS
	14/00	18.7	170.2	1000	45	2.5	TS		24/00	20.0	125.1	1006	-	1.5	TD		25/18	23.0	154.7	994	40	2.0	TS
	14/06	19.3	169.2	1000	45	2.5	TS		24/06 24/12	20.5 20.2	124.8 124.5	1002 1002	35 35	2.0 2.5	TS TS		26/00	24.2	154.0	990	45	2.5	TS
	14/12 14/18	19.8 20.2	168.6 168.2	1000 1004	45 35	2.5 2.5	TS TS		24/18	20.1	124.3	1002	40	2.5	TS		26/06 26/12	26.1 27.8	152.9 151.1	985 985	50 50	3.0 3.0	STS STS
	15/00	20.2	167.9	1004	-	2.5	TD		25/00	19.9	124.0	998	45	2.5	TS		26/18	29.6	149.3	985	50	3.0	STS
	15/06	21.5	167.8	1006	-	2.5	TD		25/06	19.8	123.8	994	50	3.0	STS		27/00	31.7	147.3	985	50	3.0	STS
	15/12	22.6	168.2	1010	-	2.5	TD		25/12 25/18	19.6 19.2	123.6 123.4	980 975	65 70	4.0 4.5	TY TY		27/06	33.9	145.7	985	50	3.0	STS
	15/18	23.5	168.2	1010	-	-	TD		26/00	18.5	123.4	970	75	5.0	TY		27/12	35.6	144.6	985	50	3.0	STS
	16/00 16/06	24.1 25.4	168.3 168.7	1010 1010	-	_	TD TD		26/06	18.0	123.2	955	85	5.5	TY		27/18 28/00	37.1 38.5	144.2 144.6	990 990	45 45	3.0 3.0	TS TS
	16/12	26.9	168.7	1010	_	_	TD		26/12	17.6	123.0	950	90	6.0	TY		28/06	39.6	145.4	990	45	3.0	TS
	16/18	27.9	168.5	1010	-	-	TD		26/18 27/00	17.2 16.8	122.9	940	95 05	6.0	TY		28/12	40.6	147.2	985	50	3.0	STS
	17/00	29.0	168.2	1012	-	-	TD		27/00	16.5	122.9 123.0	940 940	95 95	6.0 6.0	TY TY		28/18	41.0	149.5	985	50	2.5	STS
	17/06	29.8	167.7	1010	-	-	TD		27/12	16.2	123.2	940	95	6.0	TY		29/00	41.2	152.3	990	45	2.0	TS
	17/12 17/18	30.5 31.2	167.2 166.6	1012 1010	_	_	TD TD		27/18	16.0	123.7	955	85	5.0	TY		29/06 29/12	41.1 41.3	156.7 161.2	992 992	_	1.5 -	L L
	18/00	31.6	166.2	1012	-	-	TD		28/00	16.8	124.4	960	80	5.0	TY		29/18	41.4	165.7	992	-	-	L
	18/06	31.9	165.9	1012	-	-	TD		28/06 28/12	17.5 17.9	124.2 124.0	955 955	85 85	5.5 5.5	TY TY		30/00	42.4	172.7	988	-	-	L
	18/12	32.1	166.2	1012	-	-	TD		28/18	18.3	123.8	955	85	5.5	TY		30/06	44.5	178.8	980	-	-	L
	18/18	32.5	166.9	1012	-	_	TD		29/00	18.5	123.5	955	85	5.5	TY		30/12	46.2	182.1	974	-	-	Out
	19/00 19/06	32.9 33.2	167.4 168.0	1012 1012	_	_	TD TD		29/06	18.9	123.1	950	90	6.0	TY								
	19/12	33.2	168.7	1012	-	-	TD		29/12 29/18	19.3 19.9	122.7 121.9	940 935	95 100	6.5 6.5	TY TY								
	19/18	33.1	169.4	1012	-	-	TD		30/00	20.1	121.0	920	105	7.0	TY	Date	/Time	Center F	Position	Central	Max Wind	CLnum	Grade
	20/00	32.9	170.4	1012	-	-	TD		30/06	20.4	120.3	920	105	7.0	TY	Date				pressure		OI HUIII.	Grade
	20/06	32.5 32.4	171.6 172.7	1010 1010	-	_	TD TD		30/12	20.7	119.6	920	105	7.0	TY		(UTC)	Lat (N)		(hPa) KUI (23	(kt)		
	20/12 20/18	32.4	173.9	1008	_	_	TD		30/18	20.9	118.7	920	105	7.0	TY	Aug.	27/06	18.3	144.3	998	-	0.5	TD
	21/00	33.0	174.9	1008	-	-	TD		31/00 31/06	21.1 21.2	118.2 117.8	920 920	105 105	7.0 7.0	TY TY		27/12	18.4	144.0	1000	-	1.0	TD
	21/06	33.5	175.7	1008	-	-	TD		31/12	21.5	117.3	935	100	6.5	TY		27/18	18.3	143.4	998	-	1.5	TD
	21/12	34.3	177.1	1010	-	-	L		31/18	21.6	116.8	940	95	6.5	TY		28/00	18.6	142.4	998	-	2.0	TD
	21/18	35.2	178.3	1010	_	_	L	Sep.	01/00	21.9	116.2	940	95	6.5	TY		28/06 28/12	18.7 18.7	141.3 140.4	998 998	-	2.0 2.0	TD TD
	22/00 22/06	36.2 37.0	179.6 181.2	1008 1008	_	_	L Out		01/06 01/12	22.0 22.0	115.4 114.4	940 950	95 85	6.5 5.5	TY TY		28/18	18.6	139.4	996	35	2.0	TS
									01/12	22.0	113.4	970	70	5.0	TY		29/00	18.9	138.0	994	40	2.5	TS
									02/00	21.7	112.7	980	60	4.5	STS		29/06	19.0	137.4	990	45	3.0	TS
									02/06	21.7	111.9	990	50	4.5	STS		29/12	19.1	136.7	990	45	3.0	TS
									02/12	21.7	111.1	996	35	4.0	TS		29/18 30/00	19.5 20.1	136.5 136.2	990 990	45 45	3.0 3.0	TS TS
									02/18 03/00	21.6 21.4	110.5 109.7	998 1000	_	3.5	TD TD		30/06	20.5	135.6	990	45	3.0	TS
									03/06	21.4	109.4	1000	-	_	TD		30/12	21.1	135.1	990	45	3.0	TS
									03/12	20.9	109.3	1000	-	-	TD		30/18	21.1	133.7	985	50	3.0	STS
									03/18						Dissip.		31/00 31/06	21.1 21.1	133.0 132.0	980 980	55 55	3.5 3.5	STS STS
																	31/12	21.1	131.1	980	55	3.5	STS
																	31/18	21.5	130.3	980	55	3.5	STS
																Sep.	01/00	22.0	129.4	975	60	3.5	STS
																	01/06	22.2	128.4	975	60	3.5	STS
																	01/12 01/18	21.9 21.7	127.6 127.0	970 970	65 65	4.0 4.0	TY TY
																	02/00	22.1	126.3	965	70	4.5	TY
																	02/06	22.4	125.3	960	75	5.0	TY
																	02/12	22.7	124.3	960	75	5.0	TY
																	02/18 03/00	22.7 22.6	123.1 122.6	945 950	85 80	5.5 5.5	TY TY
																	03/00	22.9	121.5	965	65	5.5	TY
																	03/12	22.8	120.1	975	55	5.0	STS
																	03/18	22.6	120.0	980	50	4.5	STS
																	04/00	23.1	119.8	985	45	4.0	TS
																	04/06 04/12	23.2 23.9	119.2 118.6	985 992	45 40	3.5 3.0	TS TS
																	04/12	23.5	117.3	996	35	2.5	TS
																	05/00	23.4	116.8	1000	-	2.0	TD
																	05/06	23.5	116.5	1000	-	-	TD
																	05/12	23.5	116.1	1002	-	-	TD
																	05/18 06/00	23.3 23.2	115.5 115.1	1004 1006	_	_	TD TD
																	06/06			. , , ,			Dissip.

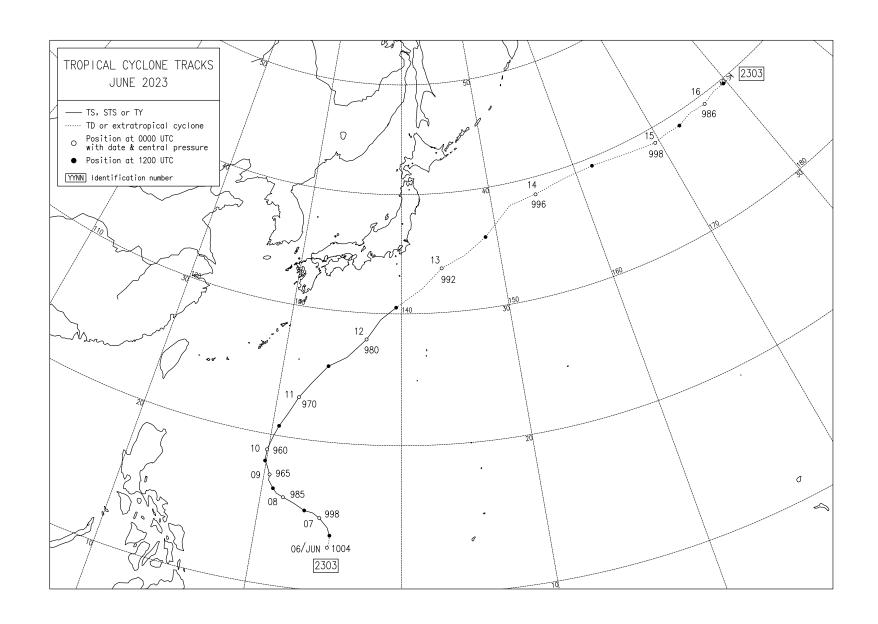
Date	/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade	Date	e/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade	Date/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)				(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)			(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)		
				OGI (2					•		_	INU (23	14)		•	_		BOLA				
۸	29/18	11.3	154.7	1004		0.5	TD	Sep.	28/12	15.8	139.0	1004		0.0	TD	Oct. 06/06	9.4		1006	,	_	TD
Aug.		12.2			_	0.5	TD	зер.	28/18	15.6	137.5	1004	_	0.5	TD			155.3		_	-	TD
	30/00		154.5	1004		1.0							_			06/12	9.7	155.0	1006		0.0	
	30/06	12.8	154.4	1002	-	1.5	TD		29/00	15.3	135.8	1004		0.5	TD	06/18	9.8	154.8	1004	-	0.5	TD
	30/12	13.3	154.3	1000	35	2.0	TS		29/06	15.2	135.1	1002	-	1.0	TD	07/00	9.9	154.5	1004	-	1.0	TD
	30/18	14.0	154.4	998	40	2.0	TS		29/12	15.6	134.2	1004	-	1.5	TD	07/06	9.9	154.1	1002	-	1.5	TD
	31/00	15.1	154.5	998	40	2.5	TS		29/18	15.5	132.3	1000	35	1.5	TS	07/12	9.9	153.7	1000	35	2.0	TS
	31/06	16.7	154.2	994	45	2.5	TS		30/00	15.3	131.8	1000	35	2.0	TS	07/18	9.9	153.3	1000	35	2.0	TS
	31/12	18.0	153.9	994	45	2.5	TS		30/06	16.1	131.4	998	35	2.0	TS	08/00	9.8	152.8	1000	35	2.5	TS
	31/18	19.0	152.9	994	45	2.5	TS		30/12	16.5	130.6	996	40	2.0	TS	08/06	9.8	152.3	998	40	2.5	TS
Sep.	01/00	20.4	151.9	994	45	2.5	TS		30/18	17.0	130.2	992	45	2.5	TS	08/12	9.9	151.6	996	45	3.0	TS
	01/06	22.0	150.8	998	40	2.5	TS	Oct.	01/00	17.4	129.5	990	50	3.0	STS	08/18	10.1	150.8	992	50	3.0	STS
	01/12	23.4	149.4	998	40	2.5	TS		01/06	17.9	128.8	990	50	3.0	STS	09/00	10.5	150.1	990	55	3.5	STS
	01/18	24.4	148.5	998	40	2.5	TS		01/12	18.3	128.4	985	55	3.5	STS	09/06	11.1	149.3	990	55	3.5	STS
									01/18	18.7	128.0	975	65	4.0	TY		11.7	148.6	990	55	3.5	STS
	02/00	25.4	147.7	1000	35	2.0	TS		02/00	19.2	127.3	965	75	5.0	TY	09/12						
	02/06	27.1	146.3	1000	35	2.0	TS				126.6		80		TY	09/18	12.7	147.7	985	60	4.0	STS
	02/12	28.6	144.9	1000	35	2.0	TS		02/06	19.7		955		5.5		10/00	13.7	146.6	980	65	4.5	TY
	02/18	29.1	143.0	1000	35	2.0	TS		02/12	20.0	126.2	950	85	6.0	TY	10/06	14.4	145.7	975	70	5.0	TY
	03/00	29.5	142.0	1002	-	2.0	TD		02/18	20.2	125.5	940	90	6.0	TY	10/12	15.1	144.9	970	75	5.5	TY
	03/06	30.2	140.7	1002	-	2.0	TD		03/00	20.5	125.1	940	90	6.0	TY	10/18	16.0	144.5	955	85	6.0	TY
	03/12	30.5	139.7	1002	-	2.0	TD		03/06	21.2	124.9	940	90	6.0	TY	11/00	17.1	144.0	935	100	7.0	TY
	03/18	31.2	138.2	1002	-	2.0	TD		03/12	21.7	124.7	940	90	6.0	TY	11/06	18.2	143.4	910	110	7.5	TY
	04/00	31.8	137.1	1002	_	1.5	TD		03/18	22.1	124.0	950	85	6.0	TY	11/12	18.9	143.0	905	115	7.5	TY
	04/06	31.8	135.7	1002	_	1.5	TD		04/00	22.2	123.5	950	85	6.0	TY	11/18	19.7	142.8	905	115	7.5	TY
	04/12	31.6	134.5	1004	_	-	TD		04/06	22.2	122.7	940	90	6.0	TY	12/00	20.6	142.9	905	115	7.5	TY
					_	_			04/12	22.0	122.0	940	90	6.0	TY	12/06	21.8	143.4	905	115	7.5	TY
	04/18	31.5	133.3	1004	_		TD		04/18	22.0	121.2	940	90	6.0	TY							
	05/00	31.1	131.8	1004	-	-	TD		05/00	22.0	120.8	960	80	6.0	TY	12/12	22.7	144.3	905	115	7.5	TY
	05/06	31.0	132.0	1004	-	-	TD		05/06	22.0	120.0	975	70	5.5	TY	12/18	24.0	145.4	920	105	7.0	TY
	05/12	31.2	132.4	1004	-	-	TD									13/00	25.5	146.9	925	100	6.0	TY
	05/18	31.8	132.7	1004	-	-	TD		05/12	22.0	119.1	975	70	5.5	TY	13/06	27.2	148.7	935	95	5.5	TY
	06/00	32.1	133.3	1004	-	-	TD		05/18	21.9	118.3	980	65	5.0	TY	13/12	29.2	151.0	935	90	5.5	TY
	06/06	32.1	134.0	1002	-	-	TD		06/00	21.8	117.7	970	75	5.0	TY	13/18	31.3	153.5	945	85	5.0	TY
	06/12	32.1	134.6	1004	-	-	TD		06/06	21.7	116.9	960	80	5.5	TY	14/00	34.1	156.6	950	80	4.5	TY
	06/18						Dissip.		06/12	21.5	116.3	960	80	5.5	TY	14/06	37.1	160.2	950	75	4.0	TY
	00/10						Dissip.		06/18	21.2	115.7	955	85	5.5	TY	14/12	40.2	164.6	950	-	3.5	L
									07/00	21.2	115.4	955	85	5.5	TY	14/18	42.9	168.0	950	_	0.0	Ĺ
									07/06	21.2	115.2	955	85	5.5	TY					_	_	
									07/12	21.3	115.1	960	80	5.0	TY	15/00	44.3	170.8	952	_	_	L
Det	e/Time	Contor	Position	Central	May Wind	CI num.	Grade		07/18	21.4	114.9	970	75	5.0	TY	15/06	44.7	174.9	954	-	-	L
Date			FOSILION	pressure	Wax Willu	Of Hulli.	Grade									15/12	45.1	179.2	956	-	-	L
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)				08/00	21.5	114.6	975	70	4.5	TY	15/18	45.3	183.4	956	-	-	Out
		TS	YUN-	YEUNG	(2313)				08/06	21.6	114.3	975	70	4.5	TY							
Sep.	04/06	20.0	129.4	1002	_	0.5	TD		08/12	21.7	114.0	980	65	4.5	TY							
оор.	04/12	20.5	130.3	1002	_	1.0	TD		08/18	21.8	113.7	992	55	4.0	STS							
	04/12	20.9	130.7	1002	_	1.5	TD		09/00	21.7	113.3	998	45	3.5	TS				Central			
									09/06	21.4	112.8	1010	-	3.0	TD	Date/Time	Center	Position	pressure	Max Wind	CI num.	Grade
	05/00	21.3	131.0	1004		1.5	TD		09/12	21.2	112.6	1012	-	-	TD	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)		
	05/06	21.9	131.5	1002	-	2.0	TD		09/18	20.9	112.4	1012	-	-	TD	(010)						
	05/12	22.7	131.9	1000		2.0	TS		10/00		-	_			Dissip.				NBA (23			
	05/18	24.1	132.5	1000	35	2.0	TS									Oct. 17/06	15.9	110.2	1006	-	0.0	TD
	06/00	25.6	133.1	1000	35	2.0	TS									17/12	16.1	110.0	1006	-	0.5	TD
	06/06	26.6	134.2	998	40	2.5	TS									17/18	16.5	109.7	1006	-	1.0	TD
	06/12	27.4	134.8	998	40	2.5	TS									18/00	17.1	109.3	1002	35	1.5	TS
	06/18	28.5	135.6	998	40	2.5	TS									18/06	17.6	108.7	1002	35	1.5	TS
	07/00	29.7	136.5	998	40											18/12	18.3	108.3	1002	35	2.0	TS
						2.5	TS									18/18	18.7	108.4	1002	35	2.0	TS
	07/06	30.9	137.0	998	40	2.5	TS															
	07/12	31.7	137.0	998	40	2.5	TS									19/00	19.4	108.7	1002	35	2.0	TS
	07/18	32.6	137.0	998	40	2.5	TS									19/06	20.0	109.0	1002	35	2.0	TS
	08/00	32.7	137.1	998	40	2.5	TS									19/12	21.0	109.4	1000	40	2.5	TS
	08/06	32.6	137.4	1000	35	2.0	TS									19/18	21.4	109.5	1002	35	2.5	TS
		33.6	138.0	1004	-	1.5	TD									20/00	21.4		1008	-	2.0	TD
	08/18		138.2			1.0	TD									20/06		109.7	1008	-	1.5	TD
	09/00	04.2	100.2	1000		1.0	Dissip.									20/12						Dissip
	00/00						DISSID.									20/12						≥.33íµ
																Date/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade
																(UTC)		Lon (E)		(kt)		
																(010)						
																			WAT (2			
																Dec. 15/12	6.7	138.2	1006	-	0.0	TD

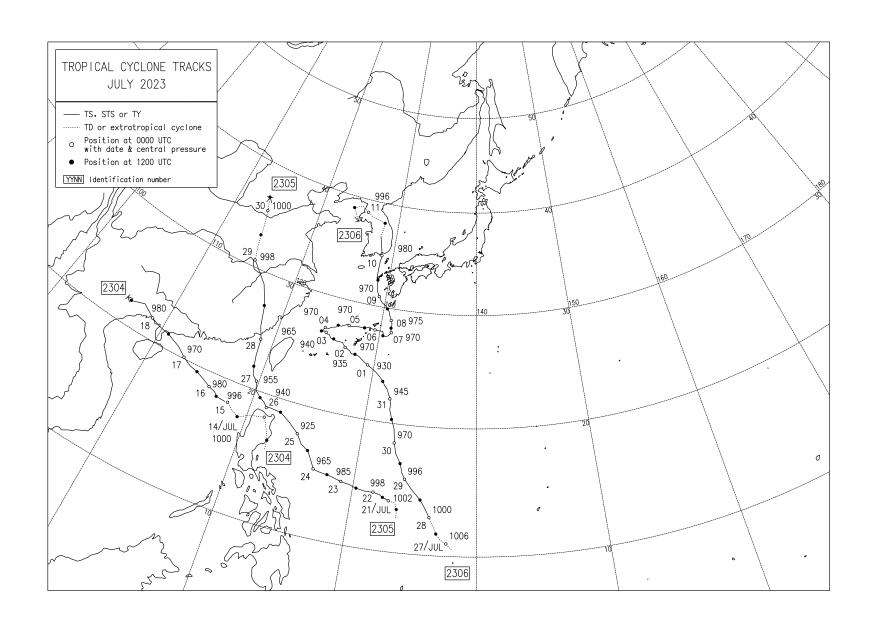
Date	/Time	Center	Position	Central pressure	Max Wind	CI num.	Grade
	(UTC)	Lat (N)	Lon (E)	(hPa)	(kt)		
		TS	JELA	WAT (2	2317)		
Dec.	15/12	6.7	138.2	1006	-	0.0	TD
	15/18	6.9	136.0	1004	-	0.0	TD
	16/00	6.9	134.8	1006	-	0.5	TD
	16/06	6.9	133.3	1004	-	0.5	TD
	16/12	7.0	131.9	1006	-	0.5	TD
	16/18	6.9	131.1	1004	-	1.0	TD
	17/00	6.9	130.3	1006	-	1.5	TD
	17/06	7.5	129.6	1002	35	2.0	TS
	17/12	7.4	128.5	1002	35	2.0	TS
	17/18	7.4	127.4	1002	35	2.0	TS
	18/00	7.4	126.3	1008	-	2.0	TD
	18/06	7.3	123.9	1006	-	-	TD
	18/12						Dissip.

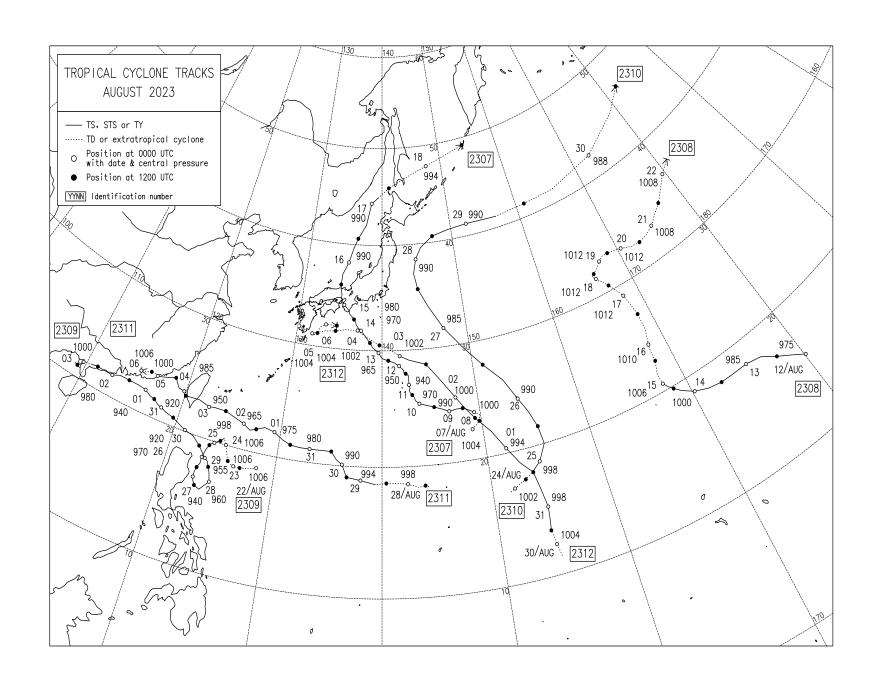
# Appendix 2 Monthly Tracks of Tropical Cyclones in 2023

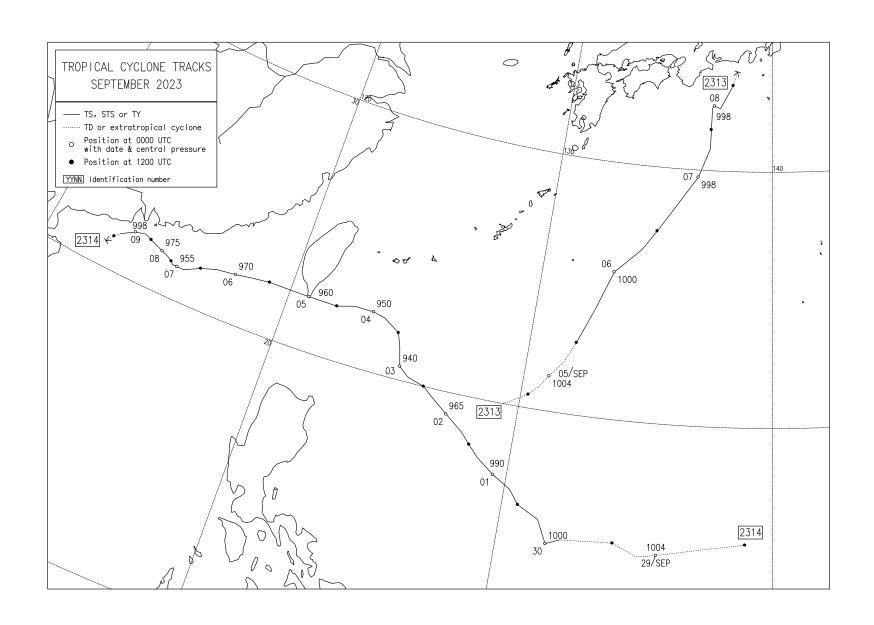


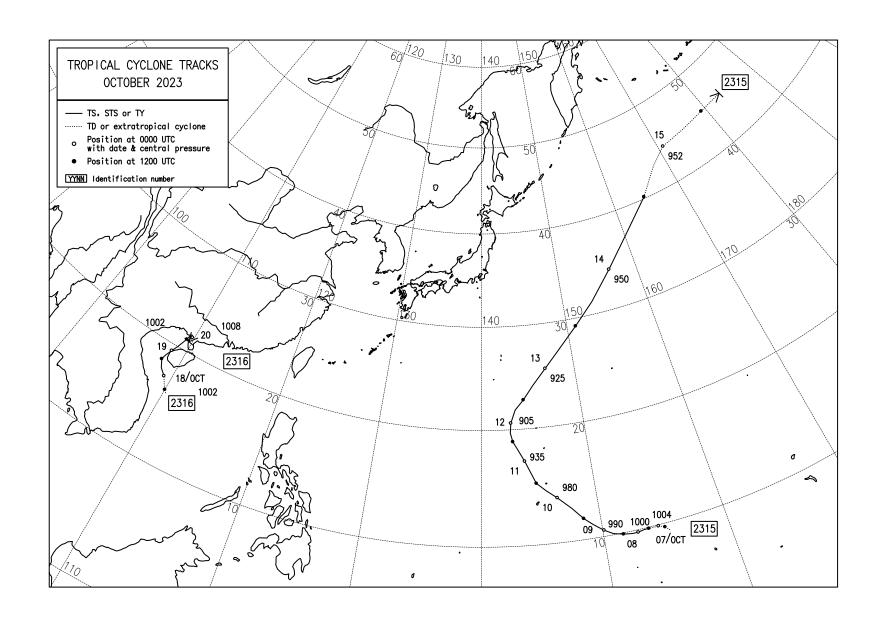


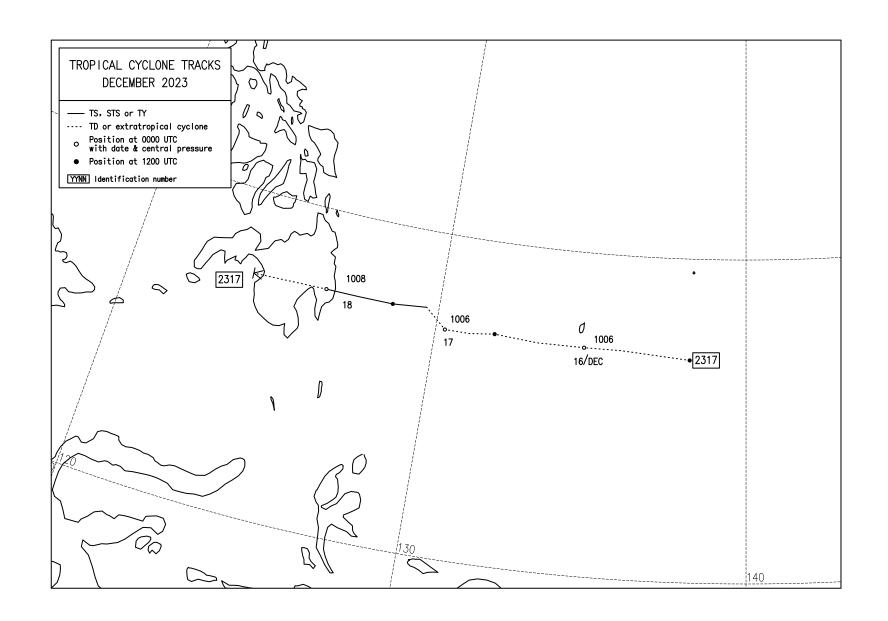












Appendix 3
Errors of Track and Intensity Forecasts for Each Tropical Cyclone in 2023

Date/	Time	Gra	ade		Cent	er Pos	sition	(km)		Cer	itral F	ressu	re (hI	Pa)		Max.	Wind	(kt) <sup>†</sup>	
	(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					
								Sanv	vu(230	1)									
Apr.	19/06	TD	TD	99	67	184	104			0	2	-2			5	0	5		
	19/12	TD	TD	80	22	109				2	-2				0	5			
	19/18	TD	TD	229	71	74				2	0				0	0			
	20/00	TD	TD	105	56	74				2	-4				0	5			
	20/06	TD	TS	16	165	167				6	-2				-10	5			
	20/12	TS	TS	0	88					4					-5				
	20/18	TS	TS	22	46					0					0				
	21/00	TS	TS	16															
	21/06	TS	TS	31															
	21/12	TS	TS	74															
	21/18	TS	TS	157															
	22/00	TD	TS																
	22/06	TD	TS																
	TS/STS/		mean	50	67					2					-3				
Valid: T	S/STS/T	Y	sample	6	2	0	0	0	0	2	0	0	0	0	2	0	0	0	0
Initial: T	TD(befor	e upg.)	mean	106	76	122	104			2	-1	-2			-1	3	5		
Valid: T	itial: TD(before upg. alid: TD/TS/STS/TY		sample	5	5	5	1	0	0	5	5	1	0	0	5	5	1	0	0

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gra	ade		Cent	er Pos	sition	(km)		Cen	tral P	ressu	re (hP	a)	1	Max	Wind	(kt) <sup>†</sup>	
Bace	(UTC)	Best	Prov.	T=0 <sup>‡</sup>				` /	=120										=12
	(010)	Best	1101.	1-0			-,2		ar(2302		-10	-,2		-120	1-21	_ 10	-,2		-12
May.	19/18	TD	TD	70	46	135	180		204	6	14	50	55	30	-10	-20	-40	-40	-20
-	20/00	TD	TD	71	33	117	182	214	257	6	10	35	20	25	-10	-10	-25	-15	-1.
	20/06	TD	TS	65	44	113	139	194	370	2	10	55	20	35	-5	-10	-35	-15	-2
	20/12	TS	TS	60	90	105	140	196	242	2	15	50	15	40	-5	-15	-30	-10	-2
	20/18	TS	TS	16	133	119	179	217	262	10	45	50	15	40	-10	-35	-30	-10	-2
	21/00	STS	STS	25	113	129	168	255	248	10	40	30	15	35	-10	-30	-20	-10	-2
	21/06	STS	STS	40	102	113	156	244	231	5	50	15	30	25	-5	-30	-10	-15	-1
	21/12	STS	STS	11	84	102	119	162	164	10	50	15	35	25	-10	-30	-10	-20	-1
	21/18	TY	TY	16	57	70	92	112	39	30	35	0	25	25	-20	-20	0	-15	-1
	22/00	TY	TY	16	11	49	162	144	<b>79</b>	30	20	10	25	15	-20	-10	-5	-15	
	22/06	TY	TY	25	24	76	178	126	74	40	15	30	25	0	-25	-5	-15	-15	
	22/12	TY	TY	22	11	121	171	160	54	35	5	25	15	-30	-20	0	-15	-10	2
	22/18	TY	TY	11	39	127	144	96	11	30	0	15	5	-40	-15	5	-10	-5	2
	23/00	TY	TY	0	43	123	131	70	91	5	10	15	-5	-40	0	0	-10	5	2
	23/06	TY	TY	0	66	163	118	75	123	-25	20	5	-25	-30	15	-10	-5	20	2
	23/12	TY	TY	11	87	133	107	68	161	-25	25	5	-45	-30	15	-15	-5	30	2
	23/18	TY	TY	0	<b>79</b>	107	86	77	146	-15	25	5	-45	-30	10	-15	-5	30	2
	24/00	TY	TY	16	68	<b>76</b>	43	101	115	15	25	5	-40	-30	-5	-15	0	25	2
	24/06	TY	TY	11	65	58	31	90	89	35	25	-20	-40	-25	-15	-15	15	25	1
	24/12	TY	TY	11	48	<b>78</b>		100	104	40	15	-40	-35	-20	-20	-10	25	20	1
	24/18	TY	TY	0	48	58		128	203	25	15	-40	-35	-10	-15	-10	25	20	
	25/00	TY	TY	11	48	53		157	230	15	-5	-40	-25	-5	-10	5	25	15	
	25/06	TY	TY	15	58	68		173	168	10	-15	-30	-20	0	-5	15	20	10	
	25/12	TY	TY	11	44	68		188	182	10	-35	-20	-10	-5	-5	25	15	5	]
	25/18	TY	TY	11	31	39		170	139	10	-35	-20	-10	-5	-5	25	15	5	1
	26/00	TY	TY		15	35	69	94	43	-5	-40	-20	-5	5	10	30	15	5	
	26/06	TY	TY	15	24	61		127	106	-20	-40	-20	-10	-10	20	30	15	5	]
	26/12	TY	TY	0	11	72		125	130	-40	-30	-20	-15	-5	25	20	10	10	
	26/18	TY	TY	11	11	42		116	147	-30	-25	-20	-5	-5	20	15	5	5	
	27/00	TY	TY	0	25	53	94	<b>76</b>	129	-20	-20	-25	-5	-10	15	10	10	5	]
	27/06	TY	TY		24		100		226	-20	-20	-25	-10	-10	15	10	10	10	1
	27/12	TY	TY	0	44		119		382	-10	-10	-15	-5	0	10	5	10	5	1
	27/18	TY	TY	0	54		174		612	-10	0	-5	-5	5	10	0	5	5	
	28/00	TY	TY	11	54		136		630	0	0	0	-10	0	0	0	5	15	]
	28/06	TY	TY	11	43				755	10	10	5	0	5	-5	-5	5	10	
	28/12	TY	TY		54		212		878	10	5	5	0	0	-5	5	5	10	
	28/18	TY	TY	0	43	107		434	965	5	-5	-5	5	5	-5	5	5	5	
	29/00	TY	TY		43			460		0	-5	-10	5		0	5	15	5	
	29/06	TY	TY	0	24		157			0	-10	-10	5		0	10	15	5	
	29/12	TY	TY			121				-5	-10	-10	-5 -		10	10	15	5	
	29/18	TY	TY			108		733		0	-5 -	0	-5		5	10	10	5	
	30/00	TY	TY		46		297			5	-5	0			5	15	10		
	30/06	TY	TY		0		392 422			0	-5 -	0			10	15	10		
	30/12	TY	TY		11					5	-5	-5			5	15	5		
	30/18	TY	TY			107	414			0	0	0			10 15	10	5		
	31/00 31/06	TY TY	TY TY			126 210				-5 -5	0				15 15	10 10			
	31/06	TY	TY			210				-5	0				10	5			
	31/12	STS	STS	0 22		205				5	5				5	0			
Jun.	01/00	STS	STS	0	24	203				0	3				5	U			
Juli.	01/06	STS	STS	11	46					0					5				
	01/00	STS	STS	15	33					5					0				
	01/12	STS	STS	11	22					5					0				
	02/00	TS	TS	51	44					3					U				
	02/00	TS	TS	20															
	02/00	TS	TS	46															
	02/12	TS	TS	53															
	J2/10	15	13	55															
Initial:	TS/STS/	ΓY	mean	12	43	98	158	210	240	4	3	-3	-5	-3	1	1	4	5	
	S/STS/T		sample		50	46	42	38	34	50	46	42	38	34	50	46	42	38	3
											11								-1
nitial: T	D(before	e upg.)	mean	69	41	122	167	200	277	5	II	47	32	30	-0	-13	-33	-23	- 1

 $<sup>^{\</sup>dagger}$ Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Гime	Gr	ade		Cent	er Pos	sition	(km)		Cer	ntral F	ressu	re (hI	Pa)	]	Max.	Wind	(kt) <sup>†</sup>	•
	(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120
								Guch	nol(230	)3)									
Jun.	06/00	TD	TD	54	92	35	58	70	359	4	7	15	15	5	-5	-10	-20	-20	-5
	06/06	TD	TD	47	54	46	40	89	290	6	12	15	15	0	-5	-15	-20	-20	0
	06/12	TS	TS	95	40	25	46	123	362	2	15	5	5	-15	0	-15	-10	-5	15
	06/18	TS	TS	15	24	15	56	182	410	2	15	5	-5	-20	0	-15	-10	5	20
	07/00	TS	TS	33	53	11	39	192	400	0	0	-10	-20	-30	0	-5	0	15	25
	07/06	TS	TS	22	48	39	78	213	450	5	0	-10	-25	-20	-5	-5	0	20	20
	07/12	TS	TS	11	31	40	112			15	0	-10	-30		-15	-5	5	25	
	07/18	STS	TS	24	21	33	137	289		15	5	-15	-20		-15	-10	10	20	
	08/00	STS	STS	25	15	21	156	335		20	10	-5	-15		-15	-5	10	15	
	08/06	STS	STS	11	25	67	241	406		10	10	-5	-15		-5	-5	10	15	
	08/12	TY		0	31		306			5	5	-10			-5	0	15		
	08/18	TY	TY	15	15	140				5	5	-10			-5	0	10		
	09/00	TY		11	24					5	0	-5			-5	5	10		
	09/06	TY	TY	11		156	298			15	0	-5			-10	5	10		
	09/12	TY		0	44	215				15	-5				-5	10			
	09/18	TY		0		165				10	-5				0	10			
	10/00	TY		0		146				0	-5				5	10			
	10/06	TY		0	57	115				0	-5				5	10			
	10/12	TY		11						-5					10				
	10/18	TY		0	24					0					5				
	11/00	TY		0	41					0					0				
	11/06	STS	STS	0	10					0					0				
	11/12	STS	STS	108															
	11/18	STS	STS	39															
	12/00	STS	STS	23															
	12/06	STS	TS	15															
Initial:	IS/STS/	ГҮ	mean	20	38	90	174	250	406	6	3	-6	-16	-21	-3	-1	5	14	20
Valid: T	S/STS/T	Y	sample	24	20	16	12	8	4	20	16	12	8	4	20	16	12	8	4
Initial: T	D(before	e upg.)	mean	50	73	40	49	79	324	5	10	15	15	3	-5	-13	-20	-20	-3
Valid: T	D/TS/ST	S/TY	sample	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/Time	Gr	ade		Cent	er Pos	sition	(km)		Cer	ntral F	ressu	re (hl	Pa)	]	Max.	Wind	(kt) <sup>†</sup>	-
(UTC)	Best	Prov.	T=0 <sup>‡</sup>	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24				=120
							Tali	m(2304	4)									
Jul. 14/00	TD	TD	85	44	115	33	200		-2	5	0	0		5	-5	0	0	
14/06	TD	TD	57	85	138	133	259		-2	0	-5	5		5	0	10	-5	
14/12	TD	TD	46	129	110	145	227		0	-5	-5	-16		0	5	10	20	
14/18	TD	TD	0	70	33	114	141		5	-5	-15	-10		-5	5	20	10	
15/00	TD	TD	0	61	52	138			10	0	-20			-10	0	25		
15/06	TS	TS	0	39	54	170			5	0	-25			-5	0	30		
15/12	TS	TS	0	39	77				0	-5				0	10			
15/18	TS	TS	0	25	54				0	-5				0	10			
16/00	STS	STS	0	21	56				0	0				5	0			
16/06	STS	STS	11	47	118				0	0				5	0			
16/12	STS	STS	0	49					0					5				
16/18	STS	STS	0	35					0					0				
17/00	STS	STS	0	15					0					0				
17/06	STS	STS	22	69					5					-5				
17/12	STS	STS	0															
17/18	STS	STS	21															
18/00	STS	STS	0															
18/06	TS	TS	0															
18/12	TD	TD																
Initial: TS/STS	/TV	mean	4	38	72	170			1	-2	-25			1	4	30		
Valid: TS/STS/		sample	13	30 9	5	1/0	0	0	9	5	-23 1	0	0	9	5	1	0	0
Initial: TD(befo		mean	38	<u>-</u>	90	113	207		2	-1	<u>-9</u>	-5		-1	1	13	6	
Valid: TD/TS/S'	10,	sample	5	5	5	5	4	0	5	5	5	4	0	5	5	5	4	0

<sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gr	ade		Cent	er Pos	sition	(km)		Cer	ntral P	ressu	re (hI	Pa)		Max.	Wind	(lzt) <sup>†</sup>	•
Date,	(UTC)	Best	Prov.	$T=0^{\ddagger}$					=120										-120
-	(010)	Dest	110V.	1=0	-24	-+0			uri(230		-70	-12	-70	-120	1-2-	-40	-12	-70	-120
Jul.	20/06	TD	TD	44	103	175	39	85	200	0	2	14	35	50	0	0	-15	- 30	-35
3 41.	20/12	TD		79		116	35	75	340	-2	-4	-10	10	20	0	0	5	-10	-15
	20/18	TD	TD		134	75	48	74	278	-2	0	0	25	20	0	-5	-5	-20	-15
	21/00	TS	TS	22	141	33		107	333	0	0	0	25	5	0	-5	-5	-20	-5
	21/06	TS	TS		116	34		139	289	0	0	5	15	-5	0	-5	-5	-10	0
	21/12	TS	TS	11	15	44		167	356	4	0	15	15	-10	-5	-5	-10	-10	5
	21/18	TS	TS	0	58	165	199		480	8	10	30	10	-20	-10	-15	-20	-5	10
	22/00	TS	TS	0	44	183	229	412	572	9	10	25	-5	-10	-10	-15	-15	5	10
	22/06	TS	TS	34	44	120	201	344	448	10	20	15	-25	-5	-10	-20	-10	15	5
	22/12	TS	TS	0	63	86	171	356	334	5	15	0	-20	10	-5	-10	0	15	-5
	22/18	STS	STS	11	76	82	204	304	347	0	10	0	-10	25	0	-5	0	5	-25
	23/00	STS	STS	15	48	39	122	263	261	0	10	-15	5	25	0	-5	10	0	-25
	23/06	STS	STS	0	22	48	137	306	234	5	0	-15	15	0	-5	0	10	-15	-5
	23/12	STS	STS	0	25	42	123	226	145	10	0	-20	20	-4	-5	0	15	-25	0
	23/18	TY	TY	22	31	43	116	178	74	15	0	-15	20	-2	-10	0	10	-25	0
	24/00	TY	TY	0	25	49	70	120		10	-15	-15	10		-5	10	15	-15	
	24/06	TY	TY	0	21	39	126	103		0	-15	0	5		0	10	5	-10	
	24/12	TY	TY	0	31	81	159	105		0	-20	0	-4		0	15	0	-5	
	24/18	TY	TY	0	21	<b>78</b>	166	216		0	-20	5	-6		0	15	-5	0	
	25/00	TY	TY	0	35	47	156			-15	-20	5			10	20	-5		
	25/06	TY	TY	0	15	64	161			-25	-20	-10			15	20	5		
	25/12	TY	TY	0	57	98	204			-20	-5	0			15	5	-10		
	25/18	TY	TY	0	57	133	110			-20	10	-4			15	-5	-5		
	26/00	TY	TY	11	25	102				-15	15				15	-10			
	26/06	TY	TY	0	33	125				-5	0				10	0			
	26/12	TY		0	30	105				-5	-2				5	-10			
	26/18	TY		0	42	67				-5	-4				5	-5			
	27/00	TY		0	88					-15					15				
	27/06	TY		0	60					-5					0				
	27/12	TY		0	41					-4					0				
	27/18	TY		0	29					-4					-5				
	28/00	TY		0															
	28/06	STS	TY	32															
	28/12	TS	TS	22															
	28/18	TS	TS	0															
	29/00	TD	TD																
Initial:	TS/STS/	ΓY	mean	6	46	79	144	232	323	-2	-1	0	4	1	1	-1	-1	-6	-3
Valid: T			sample	32	28	24	20	16	12	28	24	20	16	12	28	24	20	16	12
Initial: T			mean	41	111	122	41	78	273	-1	-1	1	23	30	0	-2	-5	-20	-22
Valid: T	D/TS/ST	S/TY	sample	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/T	(UTC)	Gra Best	Prov.	T=0 <sup>‡</sup>			sition	(KIII)		CCII	u ai i	10334	re (hF	α)		Max.	W IIIU	(Kt)	
	· /1	Dest	1101.		-74	-48	-72	-96	-120	T=24	-48	-72	-96	-120	T-24	-48			-120
Jul.	26/18			1=0	-24	-40			un(230		-40	-12	-70	-120	1-24	-40	-12	-70	-120
		TD	TD	213	156	193		268	454	0	2	12	35	40	5	0	-10	-25	-25
	27/00	TD	TD		147		245	269	376	0	0	20	35	45	0	0	-15	-25	-30
	27/06	TD	TD	252	123	264	275	395	466	2	2	20	20	25	0	-5	-15	-10	-15
	27/12	TD	TD	212	127	246	296	442	530	2	9	20	30	25	0	-10	-15	-15	-15
	27/18	TD	TS	174	155	262	328	522	715	2	10	30	30	20	0	-10	-20	-15	-10
	28/00	TS	TS	<b>79</b>			332		776	2	20	35	35	40	0	-20	-25	-20	-25
	28/06	TS	TS	39			380		727	-2	5	5	20	25	0	-5	-5	-15	-25
	28/12	TS	TS	11			419		727	5	10	15	20	40	-5	-10	-10	-15	-35
	28/18	TS	TS	22			359		612	5 15	15	15	15	45	-5 15	-10	-10	-10	-40
	29/00 29/06	TS TS	TS TS	70 56		249		562 463	653 615	15 15	20 20	20 20	30 30	50 45	-15 -15	-15 -15	-15 -15	-20 -20	-45 -40
	29/00	STS	TS	0		278	402	480	646	15	30	20	35	30	-15	-20	-15	-25	-30
	29/12	STS	STS	0	150	306	405		723	20	25	15	35	25	-15	-15	-10	-30	-25
	30/00	TY	STS	0		306			713	20	20	25	30	20	-15		-15	-25	-20
	30/06	TY	STS	0		239	262	354	585	15	20	25	25	20	-10	-15	-15	-20	-20
	30/12	TY	TY	0	117	152	134		411	25	20	15	5	5	-15	-15	-10	0	-5
	30/18	TY	TY	0	75	35	37	146	258	15	15	15	0	-5	-10	-10	-10	5	15
	31/00	TY	TY	0	23	37	63	30	89	15	15	10	-5	-5	-10	-10	-5	10	15
	31/06	TY	TY	10	39	44	45	40	193	5	10	5	-20	-20	-5	-5	0	20	30
	31/12	TY	TY	0	54	30	24	148	326	5	10	-10	-20	-20	-5	-5	10	20	30
	31/18	TY	TY	0	11	15	70	236	396	-10	0	-20	-25	-20	5	0	20	30	30
Aug.	01/00	TY	TY	0	15	30	160	305	494	-10	-5	-25	-25	-20	5	5	25	30	30
	01/06	TY	TY	0	24				377	-5	0	-20	-20	-15	5	5	20	25	20
	01/12	TY	TY	0	46	90	231		488	-5	-15	-20	-20	-20	5	15	20	25	25
	01/18	TY	TY	0	46		186	285	351	-5	-20	-20	-20	-20	5	20	25	25	25 25
	02/00	TY TY	TY TY	0	40 15	121 77	187	317 111	329	-5 10	-25 -20	-20 -20	-20 -20	-20 -20	5 10	25 20	25 25	25 25	25 25
	02/06 02/12	TY	TY	0	41	136		150	158 182	-10 -15	-20	-20	-20	-25	15	15	20	20	25
	02/12	TY	TY	11	41	89		135	239	-15	-20	-20	-20	-25	15	15	20	20	25
	03/00	TY	TY	10	23	30		150	328	-10	-10	-20	-20	-25	15	10	20	20	25
	03/06	TY	TY	0	45	37		133	251	-15	-15	-20	-20	-20	15	15	20	20	20
	03/12	TY	TY	0	45	50		125	209	-10	-10	-20	-25	-20	10	15	20	25	20
	03/18	TY	TY	30	52	30	73	198	334	-5	-10	-15	-20	-15	10	20	20	25	20
	04/00	STS	TY	40	10	10	92	162	272	-5	-10	-15	-20	-15	10	20	20	25	20
	04/06	STS	TY	0	11	49	178	211	279	-5	-10	-15	-15	0	15	20	20	20	10
	04/12	STS	TY	0	11	89	186	199	313	-5	-15	-20	-10	0	15	20	25	15	5
	04/18	STS	STS	0	11	74	150	203	376	0	-10	-15	0	0	10	15	20	10	5
	05/00	STS	STS	0	10	52	116		413	0	-10	-15	0	-5	10	15	20	10	10
	05/06	STS	STS	0	20	77		227		0		-10	0		10	15	15	10	
	05/12	STS	STS	0	44	83		229			-15		-5		10	20	15	10	
	05/18	STS	STS	0	56	70		189		5 5	-5 -5	0	0		5	15	10	5	
	06/00	STS	STS	20	22	35	57 22	82			-5 -5	0	-5		5	15 10	10	10	
	06/06 06/12	STS STS	STS STS	15 37	15 15	40 37	15			0 -5	-5 -5	-5 -10			5 10	10	10 10		
	06/12	STS	STS	11	49	31	35			-5 -5		-10			10	10	10		
	07/00	STS	STS	11	31	29	67			-5 -5	-5				10	10	15		
	07/06	STS	STS	35	40	28	٠,			0	-5				5	10			
	07/12	TS	STS	24	53	57				0	-10				5	10			
	07/18	TS	STS	24	36	65				0	-10				5	10			
	08/00	TS	STS	0	65	110				0	-5				5	5			
	08/06	STS	STS	0	36					0					5				
	08/12	STS	STS	10	48					-5					5				
	08/18	STS	STS	0	14					-5					5				
	09/00	STS	STS	0	51					-5					10				
	09/06	STS	STS	0															
	09/12	STS	STS	0															
	09/18	STS	STS	11															
	10/00	TS	TS	0															
Initial: T	S/STS/T	Y	mean	11	53	101	161	271	419	0	-1	-4	-3	0	3	5	8	8	4
Valid: TS			sample	53	49	45	41	37	33	49	45	41	37	33	49	45	41	37	33
Initial: TI			mean	221				379	508	1	5	20	30	31	1	-5		-18	-19
Valid: TI	D/TS/STS	S/TY	sample	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5	5

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

 $<sup>^{\</sup>ddagger}\text{Position error of provisional analysis}$ 

Date/7	Гіте	Gr	ade		Cent	er Pos	sition	(km)		Cer	ntral F	ressu	re (hl	Pa)		Max.	Wind	(kt) <sup>†</sup>	<del></del>
	(UTC)	Best	Prov.	T=0 <sup>‡</sup>				` ′	-120	T=24			,	· ·					-120
	(010)	Dest	1101.	1-0	-2-	-+0	-12		n(2307			-12	-70	-120	1-2-	-40	-12	-70	-120
Aug.	07/00	TD	TD	190	176	127	69	104	125	-2	4	15	40	20	0	-10	-20	-40	-25
riug.	07/06	TD		181	102	45	128	134	253	2	5	15	20	10	-5	-5	-20	-25	-20
	07/12	TD		174	67	52	126	94	118	6	10	25	20	0	-10	-10	-30	-25	-10
	07/18	TD		82	24	32	60	15	66	4	10	30	5	-10	-5	-10	-30	-15	-5
	08/00	TS		73	39	32	20	30	102	2	10	20	5	-10	-5	-10	-25	-15	-5
	08/06	TS		24	11	40		121	171	5	15	20	0	-15	-5	-20	-25	-10	0
	08/12	TS		30	10	32		145	149	5	20	15	-5	-15	-5	-25	-20	-5	0
	08/18	TS		0	11	41		170	198	10	30	5	-15	-20	-10	-30	-15	0	5
	09/00	STS		15	15	46		190	210	10	25	0	-15	-20	-10	-25	-10	0	5
	09/06	STS		15	15	15		145	239	15	25	0	-15	-20	-15	-20	-10	0	10
	09/12	STS		10	23		123		286	25	10	-5	-10	5	-25	-10	-5	-5	-10
	09/18	STS		0	22	23		142	284	30	0	-15	-15	5	-25	-5	0	0	-10
	10/00	TY		11	24	22	56	66	253	25	0	-15	-15	-20	-20	-5	0	0	10
	10/06	TY		0	20	24	91	150	277	20	0	-15	-15	-25	-15	-5	0	5	15
	10/12	TY		11	31	37	48	112	265	5	-10	-20	-25	-15	-5	5	5	15	10
	10/18	TY	TY	11	31	10		117	240	-10	-20	-20	-25	-15	5	10	10	15	15
	11/00	TY	TY	15	20	37	48		193	-15	-30	-25	-20	-10	10	15	15	20	10
	11/06	TY		0	39	51	69	107	67	-15	-15	-5	-10	0	10	10	10	10	5
	11/12	TY	TY	0	39	80	83	98	52	-15	-15	-10	-15	0	10	10	15	15	5
	11/18	TY	TY	15	31	44	24	118	183	-15	-5	-5	-10	0	10	5	5	15	0
	12/00	TY	TY	0	15	15	65	85	101	-10	0	-5	0	4	5	0	5	5	-5
	12/06	TY	TY	0	11	19	80	41		-5	-5	-5	-5		0	5	5	5	
	12/12	TY	TY	0	24	29	121	108		0	-5	-10	0		-5	5	5	0	
	12/18	TY	TY	0	45	43	107	47		0	0	-5	0		-5	0	5	0	
	13/00	TY	TY	11	9	100	62	142		-5	-5	0	4		0	5	0	-5	
	13/06	TY		10	15	44	69			0	-5	0			0	0	0		
	13/12	TY	TY	19	38	48	8			-5	-10	0			5	5	0		
	13/18	TY	TY	0	11	58	40			-5	-5	0			5	5	0		
	14/00	TY	TY	11	30	52	101			-5	-5	0			5	5	0		
	14/06	TY	TY	0	22	28				-5	-5				5	5			
	14/12	STS		15	24	54				-10	-5				10	5			
	14/18	STS		0		112				-5	0				10	0			
	15/00	STS	STS	14		106				-5	-5				5	0			
	15/06	STS		14	80					-5					5				
	15/12	TS		9	121					-5					5				
	15/18	TS		9	128					0					0				
	16/00	TS		11	58					0					0				
	16/06	TS		0															
	16/12	TS		56															
	16/18	TS		59															
	17/00	TS	TS	22															
Initial:	IS/STS/7	Ϋ́	mean	13	33	44	68	121	192	0	-1	-4	-10	-10	-1	-2	-1	3	4
Valid: T			sample	37	33	29	25	21	17	33	29	25	21	17	33	29	25	21	17
Initial: T	D(before	e upg.)	mean	157	93	64	96	87	140	3	7	21	21	5	-5	-9	-25	-26	-15
Valid: TI	D/TS/STS	S/TY	sample	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Гіте	Gra	ade		Cent	er Pos	sition	(km)		Cer	tral P	ressu	re (hP	a)		Max.	Wind	(kt) <sup>†</sup>	-
	(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120
								Dor	a(2308	3)									·
Aug.	12/00	TY	TY	15	40	87				15	4				-25	-5			
	12/06	TY	TY	21	35	92				2	-2				-5	5			
	12/12	TY	TY	0	94	118				-4	-8				10	15			
	12/18	TY	TY	15	138	175				-8	-12				10	20			
	13/00	TY	TY	54	124					-8					10				
	13/06	TY	STS	53	81					-4					5				
	13/12	STS	STS	21	42					-2					0				
	13/18	STS	STS	0	15					-6					10				
	14/00	TS	TS	0															
	14/06	TS	TS	0															
	14/12	TS	TS	15															
	14/18	TS	TS	33															
	15/00	TD	TS																
	15/06	TD	TD																
Initial:	IS/STS/T	ſΥ	mean	19	71	118				-2	-5				2	9			
Valid: T	S/STS/T	Y	sample	12	8	4	0	0	0	8	4	0	0	0	8	4	0	0	0
Initial: T	D(before	e upg.)	mean																
Valid: T	D/TS/STS	S/TY	sample	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

<sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gr	ade		Cent	er Pos	sition	(km)		Cer	ntral P	ressu	re (hl	Pa)	]	Max.	Wind	(kt) <sup>†</sup>	-
	(UTC)	Best	Prov.	T=0 <sup>‡</sup>	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					=120
	•							Sao	la(2309	9)									
Aug.	23/18	TD	TD	67	92	159	266	352	278	-2	21	52	30	20	-5	-30	-50	-30	-20
	24/00	TD	TD	54	124	139	169	176	276	2	24	45	15	15	-10	-30	-35	-10	-10
	24/06	TS	TS	46	<b>79</b>	59	97	49	214	0	30	35	5	5	-5	-25	-25	-5	-5
	24/12	TS	TS	43	49	48	108	54	169	12	20	10	-15	0	-10	-10	0	10	0
	24/18	TS	TS	33	39	107	165	105	139	15	25	-15	-15	5	-10	-10	10	10	-5
	25/00	TS	STS	22	42	139	129	168	208	15	25	-20	-15	20	-10	-10	15	10	-10
	25/06	STS	STS	25	31	128	149	206	304	20	20	-15	-15	15	-10	-5	10	10	-5
	25/12	TY	TY	0	34	140	129	176	333	10	0	-20	-5	15	-10	0	15	5	-5
	25/18	TY	TY	22	39	116	117	177	333	20	-15	-20	0	15	-15	10	15	0	-5
	26/00	TY	TY	11	48	46	139	220	335	15	-20	-35	0	15	-10	15	20	0	-5
	26/06	TY	TY	0	88	119	178	253	283	10	-20	-30	0	15	-5	15	15	0	-5
	26/12	TY	TY	0	112	150	169	255	298	0	-20	-20	15	25	0	15	10	-5	-20
	26/18	TY	TY	0	116	144	192	292	408	-20	-35	-15	30	45	15	20	5	-15	-35
	27/00	TY	TY	0	39	152	194	316	386	-40	-35	0	55	54	25	20	0	-35	-50
	27/06	TY	TY	0	64	139	175	235	274	-35	-30	0	55	58	20	15	0	-35	-55
	27/12	TY	TY	0	96		162		257	-35	-20	0	25	42	20	10	0	-20	-35
	27/18	TY	TY	0	98	130	221	252	403	-20	-15	20	20	15	15	5	-10	-15	-10
	28/00	TY	TY	11	111	156	206	247	417	-5	20	30	20	0	5	-10	-15	-15	5
	28/06	TY	TY	0	77	117	113	186	372	0	20	30	20	-10	0	-10	-15	-15	15
	28/12	TY	TY	15	54	136	124		386	10	20	20	10	-16	-5	-10	-15	-5	30
	28/18	TY	TY	0	52	139	86	227		5	30	15	-10		-5	-15	-10	10	
	29/00	TY	TY	0	74	94		248		30	35	15	-20		-15	-20	-10	20	
	29/06	TY	TY	0	42	46				30	35	20	-20		-15	-20	-15	25	
	29/12	TY		0	43	21		291		20	15	5	-21		-10	-10	0	35	
	29/18	TY		0	62	53				15	10	-15			-5	-5	10		
	30/00	TY		0	33		104			20	10	-20			-10	-10	15		
	30/06	TY	TY	0	57	69				20	10	-15			-10	-10	10		
	30/12	TY	TY	10	25	45	136			5	5	-16			-5	-5	20		
	30/18	TY	TY	0	54	83				10	10				-5	-10			
	31/00	TY	TY	11	39	93				10	0				-5	0			
	31/06	TY	TY	0	39	76				15	-5				-10	5			
	31/12	TY		10	43	86				20	-4				-10	10			
	31/18	TY		0	53					0					0				
Sep.	01/00	TY		0	38					5					-5				
	01/06	TY		0	33					0					0				
	01/12	TY		0	94					-4					10				
	01/18	TY		0															
	02/00	STS	STS	25															
	02/06	STS	STS	0															
	02/12	TS	TS	11															
	02/18	TD	TD																
[nitial• '	TS/STS/	ΓV	moor	8	59	100	141	210	307		4	-2	5	18	-3	-2	2	-1	-11
	S/STS/T		mean sample	38	34	30	26	22	18	34	30	26	22	18	34	30	26	22	-11 18
	D(before		mean	61		149	217		277	0	23	49	23	18	-8	-30	-43	-20	-15
	D/TS/ST	10,	sample	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
. and . 1	-/10/01	J, 1 1	sample																

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

ime	Gr	ade		Cent	er Pos	sition	(km)		Cer	ntral F	ressu	re (hI	Pa)	]	Max.	Wind	$(kt)^{\dagger}$	
(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					=120
•							Damı	rey(23)	10)									
24/00	TD	TD	259	455	331	591	370	758	0	6	13	10	12	0	-5	-10	-10	-10
24/06	TD	TD	295	257	275	125	413		4	11	13	10		-5	-10	-10	-10	
24/12	TD	TD	310	150	219	223	177		4	11	13	15		-5	-10	-10	-15	
24/18	TS	TS	204	65	209	69	183		4	11	6	13		-5	-10	-5	-15	
25/00	TS	TS	31	94	157	73	457		8	13	6	6		-10	-15	-5	-5	
25/06	TS	TS	0	90	24	136			5	5	0			-5	-5	0		
25/12	TS	TS	0	59	69	150			5	5	9			-5	-5	-10		
25/18	TS	TS	54	29	80	120			5	0	9			-5	0	-10		
26/00	TS	TS	30	96	33	108			5	0	4			-5	0	-5		
26/06	STS	TS	0	29	51				0	-5				-5	5			
26/12	STS	TS	49	14	28				-5	0				0	0			
26/18	STS	TS	29	35	45				-15	0				10	0			
27/00	STS	TS	19	49	0				-10	-5				10	5			
27/06	STS	TS	22	48					-5					5				
27/12	STS	TS	0	54					0					0				
27/18	TS	TS	0	11					0					0				
28/00	TS	TS	37	55					-5					5				
28/06	TS	TS	0															
28/12	STS	TS	48															
28/18	STS	STS	0															
29/00	TS	TS	0															
S/STS/T	ΓY	mean	29	52	70	109	320		-1	2	6	10		-1	-3	-6	-10	
/STS/T	Y	sample	18	14	10	6	2	0	14	10	6	2	0	14	10	6	2	0
D(before	e upg.)	mean	288					758	3	9	13	12	12	-3	-8	-10	-12	-10
)/TS/STS	S/TY	sample	3	3	3	3	3	1	3	3	3	3	1	3	3	3	3	1
	24/00 24/06 24/12 24/18 25/00 25/06 25/12 25/18 26/00 26/12 26/18 27/00 27/12 27/18 28/00 28/12 28/18 29/00 S/STS/T O(before	CUTC         Best           24/00         TD           24/06         TD           24/12         TD           24/18         TS           25/00         TS           25/06         TS           25/12         TS           26/00         TS           26/06         STS           26/12         STS           27/00         STS           27/06         STS           27/12         STS           27/18         TS           28/06         TS           28/12         STS           28/12         STS	CUTC)         Best         Prov.           24/00         TD         TD           24/06         TD         TD           24/12         TD         TD           24/18         TS         TS           25/00         TS         TS           25/06         TS         TS           25/12         TS         TS           25/18         TS         TS           26/00         TS         TS           26/06         STS         TS           26/12         STS         TS           27/00         STS         TS           27/06         STS         TS           27/12         STS         TS           28/06         TS         TS           28/12         STS         TS           28/12         STS         TS           29/00         TS         TS           SVSTS/TY         mean           smple         D(before upg.)         mean	CUTC)         Best         Prov.         T=0 <sup>‡</sup> 24/00         TD         TD         259           24/06         TD         TD         295           24/12         TD         TD         310           24/18         TS         TS         204           25/00         TS         TS         31           25/06         TS         TS         0           25/12         TS         TS         0           25/12         TS         TS         54           26/06         TS         TS         30           26/06         STS         TS         0           26/12         STS         TS         49           26/12         STS         TS         29           27/00         STS         TS         19           27/06         STS         TS         0           27/12         STS         TS         0           28/00         TS         TS         0           28/12         STS         TS         0           28/12         STS         TS         0           28/12         STS         TS         0	CUTC         Best         Prov.         T=0 <sup>‡</sup> =24           24/00         TD         TD         259         455           24/06         TD         TD         295         257           24/12         TD         TD         310         150           24/18         TS         TS         204         65           25/00         TS         TS         31         94           25/06         TS         TS         0         90           25/12         TS         TS         0         59           25/12         TS         TS         30         96           26/06         TS         TS         30         96           26/06         STS         TS         0         29           26/12         STS         TS         49         14           26/18         STS         TS         29         35           27/00         STS         TS         19         49           27/12         STS         TS         0         54           27/18         TS         TS         0         11           28/06         TS         TS	CUTC         Best         Prov.         T=0 <sup>‡</sup> =24         =48           24/00         TD         TD         259         455         331           24/06         TD         TD         295         257         275           24/12         TD         TD         310         150         219           24/18         TS         TS         204         65         209           25/00         TS         TS         31         94         157           25/06         TS         TS         0         90         24           25/12         TS         TS         0         59         69           25/12         TS         TS         54         29         80           25/12         TS         TS         30         96         33           26/00         TS         TS         30         96         33           26/06         STS         TS         49         14         28           26/12         STS         TS         29         35         45           27/00         STS         TS         19         49         0           27/12	CUTC)         Best         Prov.         T=0 <sup>‡</sup> =24         =48         =72           24/00         TD         TD         259         455         331         591           24/06         TD         TD         295         257         275         125           24/12         TD         TD         310         150         219         223           24/18         TS         TS         204         65         209         69           25/00         TS         TS         31         94         157         73           25/06         TS         TS         0         90         24         136           25/12         TS         TS         0         59         69         150           25/12         TS         TS         30         96         33         108           25/12         TS         TS         30         96         33         108           26/00         TS         TS         30         96         33         108           26/12         STS         TS         49         14         28           26/12         STS         TS         19 </td <td>(UTC)         Best         Prov.         T=0<sup>‡</sup>         =24         =48         =72         =96           Dami           24/00         TD         TD         259         455         331         591         370           24/06         TD         TD         295         257         275         125         413           24/12         TD         TD         310         150         219         223         177           24/18         TS         TS         204         65         209         69         183           25/00         TS         TS         31         94         157         73         457           25/06         TS         TS         0         90         24         136           25/12         TS         TS         0         59         69         150           25/12         TS         TS         30         96         33         108           25/12         TS         TS         30         96         33         108           26/06         STS         TS         49         14         28           26/12         STS         TS</td> <td>(UTC)         Best         Prov.         T=0<sup>‡</sup>         =24         =48         =72         =96         =120           Damrey(23)           24/00         TD         TD         259         455         331         591         370         758           24/06         TD         TD         295         257         275         125         413           24/12         TD         TD         310         150         219         223         177           24/18         TS         TS         204         65         209         69         183           25/00         TS         TS         31         94         157         73         457           25/06         TS         TS         0         90         24         136           25/12         TS         TS         0         59         69         150           25/12         TS         TS         0         59         69         150           25/12         TS         TS         30         96         33         108           26/06         TS         TS         30         96         33         108      &lt;</td> <td>(UTC)         Best         Prov.         T=0<sup>†</sup>         =24         =48         =72         =96         =120         T=24           24/00         TD         TD         259         455         331         591         370         758         0           24/06         TD         TD         295         257         275         125         413         4           24/12         TD         TD         310         150         219         223         177         4           24/18         TS         TS         204         65         209         69         183         4           25/00         TS         TS         31         94         157         73         457         8           25/06         TS         TS         0         90         24         136         5           25/12         TS         TS         0         59         69         150         5           25/12         TS         TS         54         29         80         120         5           25/12         TS         TS         30         96         33         108         5           26/06</td> <td>(UTC)         Best         Prov.         T=0<sup>‡</sup>         =24         =48         =72         =96         =120         T=24         =48           24/00         TD         TD         259         455         331         591         370         758         0         6           24/06         TD         TD         295         257         275         125         413         4         11           24/12         TD         TD         310         150         219         223         177         4         11           24/18         TS         TS         204         65         209         69         183         4         11           25/00         TS         TS         31         94         157         73         457         8         13           25/06         TS         TS         0         90         24         136         5         5         5           25/12         TS         TS         0         59         69         150         5         5         5           25/12         TS         TS         30         96         33         108         5         0</td> <td>  CUTC   Best   Prov.   T=0<sup>‡</sup>   =24   =48   =72   =96   =120   T=24   =48   =72   =24   =48   =72   =96   =120   T=24   =48   =72   =24   =48   =72   =24   =48   =72   =24   =48   =72   =24   =48   =72   =24   =</td> <td>  CUTC   Best</td> <td>  CUTC   Best</td> <td>  CUTC   Best</td> <td>  CUTC   Best</td> <td>  Cutto   Best</td> <td>  Currect   Best   Prov.   T=0    =24   =48   =72   =96   =120   T=24   =48   =72   =96   =120   T=24   =48   =72   =96   =96   =96   =120   T=24   =48   =72   =96   =9</td>	(UTC)         Best         Prov.         T=0 <sup>‡</sup> =24         =48         =72         =96           Dami           24/00         TD         TD         259         455         331         591         370           24/06         TD         TD         295         257         275         125         413           24/12         TD         TD         310         150         219         223         177           24/18         TS         TS         204         65         209         69         183           25/00         TS         TS         31         94         157         73         457           25/06         TS         TS         0         90         24         136           25/12         TS         TS         0         59         69         150           25/12         TS         TS         30         96         33         108           25/12         TS         TS         30         96         33         108           26/06         STS         TS         49         14         28           26/12         STS         TS	(UTC)         Best         Prov.         T=0 <sup>‡</sup> =24         =48         =72         =96         =120           Damrey(23)           24/00         TD         TD         259         455         331         591         370         758           24/06         TD         TD         295         257         275         125         413           24/12         TD         TD         310         150         219         223         177           24/18         TS         TS         204         65         209         69         183           25/00         TS         TS         31         94         157         73         457           25/06         TS         TS         0         90         24         136           25/12         TS         TS         0         59         69         150           25/12         TS         TS         0         59         69         150           25/12         TS         TS         30         96         33         108           26/06         TS         TS         30         96         33         108      <	(UTC)         Best         Prov.         T=0 <sup>†</sup> =24         =48         =72         =96         =120         T=24           24/00         TD         TD         259         455         331         591         370         758         0           24/06         TD         TD         295         257         275         125         413         4           24/12         TD         TD         310         150         219         223         177         4           24/18         TS         TS         204         65         209         69         183         4           25/00         TS         TS         31         94         157         73         457         8           25/06         TS         TS         0         90         24         136         5           25/12         TS         TS         0         59         69         150         5           25/12         TS         TS         54         29         80         120         5           25/12         TS         TS         30         96         33         108         5           26/06	(UTC)         Best         Prov.         T=0 <sup>‡</sup> =24         =48         =72         =96         =120         T=24         =48           24/00         TD         TD         259         455         331         591         370         758         0         6           24/06         TD         TD         295         257         275         125         413         4         11           24/12         TD         TD         310         150         219         223         177         4         11           24/18         TS         TS         204         65         209         69         183         4         11           25/00         TS         TS         31         94         157         73         457         8         13           25/06         TS         TS         0         90         24         136         5         5         5           25/12         TS         TS         0         59         69         150         5         5         5           25/12         TS         TS         30         96         33         108         5         0	CUTC   Best   Prov.   T=0 <sup>‡</sup>   =24   =48   =72   =96   =120   T=24   =48   =72   =24   =48   =72   =96   =120   T=24   =48   =72   =24   =48   =72   =24   =48   =72   =24   =48   =72   =24   =48   =72   =24   =	CUTC   Best	CUTC   Best	CUTC   Best	CUTC   Best	Cutto   Best	Currect   Best   Prov.   T=0    =24   =48   =72   =96   =120   T=24   =48   =72   =96   =120   T=24   =48   =72   =96   =96   =96   =120   T=24   =48   =72   =96   =9

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Mug. 27/06   TD   TD   59 24 248 272 296 2120   T=24 48 272 296 2120   TD   TD   TD   TD   TD   TD   TD   T	Date/	Time	Gr	ade		Cent	er Po	sition	(km)		Cer	ntral F	ressu	ıre (hl	Pa)	1	Max.	Wind	(kt) <sup>†</sup>	<del></del>
Aug.   27/06   TD   TD   59   244   278   79   109   358   -2   0   -5   0   0   5   0   5   0   5   0   -5		(UTC)	Best	Prov.	T-0 <sup>‡</sup>					=120										=120
Aug.   27/06   TD   TD   TD   59   244   278   79   109   358   -2   0   -5   0   0   0   5   0   0   5   0   0	-	` /			1-0															
27/12   TD   TD   0   255   302   119   204   537   -2   0   -5   0   5   5   0   5   5   0   0   0	Aug.	27/06	TD	TD	59	244	278	79	109	358	-2	0	-5	0	0	5	0	5	0	0
27/18					0															
28/06					21	285	192	84	318		0	0	0	0	10	0	0	0	0	-10
28/12		28/00	TD	TS	67	328	74	262	445	721	0	0	5	5	15	0	0	-5	-5	-15
28/18		28/06	TD	TS	116	213	67	265	402	706	6	4	10	5	10	-10	-5	-10	-5	-10
Part		28/12	TD	TS	0	169	94	279	446	632	8	4	5	0	20	-10	-5	-5	0	-20
Part		28/18	TS	TS	0	123	166	377	544	648	6	0	-5	0	35	-5	0	5	0	-30
29/12		29/00	TS	TS	0	192	358	561	<b>741</b>	1034	2	5	0	5	30	0	-5	0	-5	-25
29/18		29/06	TS	STS	0	114	289	422	803	1229	-10	-10	-5	15	20	15	10	5	-15	-15
STS   10   206   375   518   640   1060   0   10   10   12   11   10   10   0   30   -5     30/06		29/12	TS	STS	84	146	396	493	617	945	-20	-25	-15	15	15	30	25	15	-10	-5
30/06					81															
30/12																				
30/18																				
STR   STR					_															
31/06   STS   STS   0   98   283   359   452   0   10   10   13   10   0   0   0   -10					_					1152					2					0
Sep.   01/00   STS   TY   0   112   235   224     10   30   9     0   -20   -5																				
Sep.   01/00   STS   TY   0   112   235   224   10   30   9   0   -20   -5   5   5   10   10   10   10   10   10																				
Sep.         01/00         STS         TY         0         112         235         224         10         30         9         0         -20         -5         5         1         2         101/06         STS         TY         0         57         126         112         15         15         15         0         -5         -5         5         5         10           01/12         TY         TY         TY         11         15         84         30         15         5         -7         -5         5         5         10         -5         0         10         0         10         10         0         -15         0         10         0         10         0         -5         0         10         0         -5         0         10         0         -5         5         5         -5         0         10         0         -5         0         10         0         -5         5         5         -5         5         5         -5         5         5         -5         5         -5         5         -5         5         -5         5         -5         5         -5         0         -5 </td <td></td>																				
01/06   STS   TY   0   57   126   112   15   15   0   -5   -5   5   5   10	C								340					4					-5	
01/12	Sep.																			
01/18																				
02/00																				
02/06								124					-11					10		
02/12																				
02/18																				
03/00																				
03/06												_								
03/12   STS   TY   21   49   -2   5   10																				
03/18   STS   TY   24   84   -11   10   10					21	49														
04/00 TS STS 15 04/06 TS TS 0 04/12 TS TS 0 04/18 TS TS 0 05/00 TD TD  Initial: TS/STS/TY mean 11 119 251 385 626 1046 3 4 5 16 16 5 2 1 -12 -11 Valid: TS/STS/TY sample 29 25 21 17 13 9 25 21 17 13 9 25 21 17 13 9 25 21 17 13 9 25 21 17 13 9 25 21 17 13 9 25 21 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2				TY	24	84										10				
04/12 TS TS 0 04/18 TS TS 0 04/18 TS TS 0 05/00 TD		04/00	TS	STS	15															
04/18 TS TS 05/000 TD TD       TS TS 05/000 TD       TS 15/000		04/06	TS	TS	0															
O5/00         TD         TD           Initial: TS/STS/TY         mean sample         11 119 251 385 626 1046 3 4 5 16 16 5 2 1 7 13 9 15 16 16 16 16 16 16 16 16 16 16 16 16 16		04/12	TS	TS	0															
Initial: TS/STS/TY         mean sample         11 119 251 385 626 1046 29 25 21 17 13 9 25 21 17 13 9 25 21 17 13 9 25 21 17 2 2 2 10 -2 -2 -2 -2 -10         3 4 5 16 16 5 2 1 -12 -11 18 19 25 21 17 13 9 25 21 17 13 9 25 21 17 13 9 25 21 17 13 13 9 25 21 17 13 18 19 25 21 17 13 18 19 25 21 27 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		04/18	TS	TS	0															
Valid: TS/STS/TY         sample         29         25         21         17         13         9         25         21         17         13         9         25         21         17         13         9           Initial: TD(before upg.)         mean         44         249         168         181         321         579         2         1         2         2         10         -2         -2         -2         -2         -10		05/00	TD	TD																
Valid: TS/STS/TY         sample         29         25         21         17         13         9         25         21         17         13         9         25         21         17         13         9           Initial: TD(before upg.)         mean         44         249         168         181         321         579         2         1         2         2         10         -2         -2         -2         -2         -10	Initial:	TS/STS/	ΓY	mean	11	119	251	385	626	1046	3	4	5	16	16	5	2	1	-12	-11
Initial: TD(before upg.) mean 44 249 168 181 321 579 2 1 2 2 10 -2 -2 -2 -10										9	25	21		13	9	25	21	17	13	9
Valid: TD/TS/STS/TY         sample         6 <td>Initial: T</td> <td>TD(before</td> <td>e upg.)</td> <td>mean</td> <td>44</td> <td>249</td> <td>168</td> <td>181</td> <td>321</td> <td>579</td> <td>2</td> <td>1</td> <td>2</td> <td>2</td> <td>10</td> <td></td> <td>-2</td> <td>-2</td> <td>-2</td> <td>-10</td>	Initial: T	TD(before	e upg.)	mean	44	249	168	181	321	579	2	1	2	2	10		-2	-2	-2	-10
	Valid: T	D/TS/ST	S/TY	sample	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6	6

<sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gr	ade		Cent	er Pos	sition	(km)		Cer	tral P	ressu	re (hl	Pa)		Max.	Wind	(kt) <sup>†</sup>	-
	(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120					=120
								Kiro	gi(231	2)									
Aug.	29/18	TD	TD	65	68	137	148	203	394	2	0	-2	-2	-4	-5	0	0	0	5
	30/00	TD	TD	0	78	107	190	207	597	2	0	-4	-4	0	-5	0	5	5	0
	30/06	TD	TD	11	109	205	314	437		4	-6	-4	-2		-5	10	5	0	
	30/12	TS	TS	0	158	168	359			0	-8	-4			0	15	5		
	30/18	TS	TS	0	134	181	269			-2	-8	-4			5	15	5		
	31/00	TS	TS	25	133	234				-4	-8				10	10			
	31/06	TS	STS	11	142	261				-8	-4				15	5			
	31/12	TS	STS	25	166	288				-6	-2				10	0			
	31/18	TS	STS	62	120	166				-4	-2				5	0			
Sep.	01/00	TS	STS	10	131					-2					5				
	01/06	TS	STS	0	155					-2					0				
	01/12	TS	TS	60	185					-2					0				
	01/18	TS	TS	63	67					-2					0				
	02/00	TS	TS	0															
	02/06	TS	TS	15															
	02/12	TS	TS	10															
	02/18	TS	TS	33															
	03/00	TD	TS																
	03/06	TD	TD																
Initial:	TS/STS/	ΓY	mean	22	139	216	314			-3	-5	-4				8			
	S/STS/T		sample	14	10	6	2	0	0	10	6	2	0	0	10	6	2	0	0
Initial: T	TD(befor	e upg.)	mean	26	85	149	217	282	495	3	-2	-3	-3	-2	-5	3	3	2	3
Valid: T	D/TS/ST	S/TY	sample	3	3	3	3	3	2	3	3	3	3	2	3	3	3	3	2

<sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gra	ade		Cent	er Pos	sition	(km)		Cei	ntral P	ressu	re (hl	Pa)		Max.	Wind	(kt) <sup>†</sup>	
	(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24				
							Y	un-ye	eung(2	313)									
Sep.	04/06	TD	TD	86	204	334	637	861		-2	-6	-8	-10		5	5	10	10	
	04/12	TD	TD	79	207	213	551	849		0	-6	-8	-14		0	5	10	15	
	04/18	TD	TD	79	185	295	574	672		0	-6	-8	-16		0	5	10	15	
	05/00	TD	TD	39	181	399	686			0	-6	-8			0	5	10		
	05/06	TD	TD	21	141	278	421			2	-6	-10			-5	5	15		
	05/12	TS	TS	78	166	307				0	-4				0	5			
	05/18	TS	TS	129	83	150				0	-4				0	5			
	06/00	TS	TS	10	124	210				0	-4				0	5			
	06/06	TS	TS	15	145	356				-4	-6				5	10			
	06/12	TS	TS	33	130					-4					5				
	06/18	TS	TS	20	76					-4					5				
	07/00	TS	TS	10	93					-4					5				
	07/06	TS	TS	11	208					-4					5				
	07/12	TS	TS	53															
	07/18	TS	TS	28															
	08/00	TS	TS	44															
	08/06	TS	TS	56															
	08/12	TD	TD																
Initial:	TS/STS/	ΓY	mean	41	128	256				-3	-5				3	6			
	S/STS/T		sample	12	8	4	0	0	0	8	4	0	0	0	8	4	0	0	0
Initial: 7	D(befor	e upg.)	mean	61	184	304	574			0	-6	-8	-13		0	5	11	13	
Valid: T	D/TS/ST	S/TY	sample	5	5	5	5	3	0	5	5	5	3	0	5	5	5	3	0

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gr	ade		Cent	er Po	sition	(km)		Cen	tral P	ressu	re (hF	Pa)		Max	Wind	(kt) <sup>†</sup>	<u> </u>
	(UTC)	Best	Prov.	T=0 <sup>‡</sup>				. ,	=120				•						-120
	(010)	Dest	1101.	1-0	-27	-40	-12		nu(2314		-40	-12	-/0	-120	1-2-	0	-12	-70	-120
Sep.	29/06	TD	TD	0	02	211	310		114	0	6	39	50	40	0	-15	-40	-45	-35
Бер.	29/12	TD	TD	0			310		174	2	9	40	45	40	-5	-15	-40	-40	-35
	29/12	TS	TS	25		290			196	4	15	45	30	35	-5	-20	-40	-30	-30
	30/00	TS	TS	76		256			76	0	15	25	0	-10	-5	-20	-20	-5	0
	30/06	TS	TS	22		158	63	57	31	0	25	20	10	-25	-5	-25	-15	-5	15
	30/12	TS	TS	0	86	105	57	30	15	0	25	20	10	-20	-5	-25	-15	-5	10
	30/12	TS	TS	0	55	83	88	56	83	5	30	0	10	-25	-10	-25	-5	-5	15
Oct.	01/00	STS	STS	0	74	80	61	41	135	10	25	0	-10	-15	-15	-20	0	5	5
Oct.	01/06	STS	STS	0	97	84		173	346	15	10	10	-20	10	-15	-5	-5	10	-10
	01/00	STS	STS	0	80	53		215	378	10	10	10	-5	25	-10	-5	-5	0	-25
	01/12	TY	TY	0	52	22		187	357	10	0	15	-10	30	-10	0	-10	0	-35
	02/00	TY		0	43	21		197	349	0	0	5	15	39	0	0	-10	-25	-45
	02/06	TY		0	11	11		144	305	0	10	-5	30	39	0	-5	-5	-35	-45
	02/00	TY	TY	0	30	56		115	153	0	15	-5	30	40	0	-10	-5	-35	-45
	02/12	TY	TY	0	45	78			188	0	20	-5	43	36	0	-15	-5	-45	-45
	03/00	TY		0	47	108			199	5	10	10	45	33	-5	-15	-20	-50	-40
	03/06	TY		0	15	123			302	15	-5	20	45	33	-10	-5	-25	-50	-40
	03/12	TY	TY	0	25		184		257	15	5	32	40	28	-10	-10	-30	-45	-35
	03/18	TY		0	43		244		286	15	5	39	30	16	-10	-10	-40	-40	-25
	04/00	TY		0	38				200	10	20	43	33	10	-10	-25	-45	-40	
	04/06	TY		0	38		265			0	30	43	33		-5	-30	-45	-40	
	04/12	TY	TY	11			204			0	30	38	28		-5	-30	-40	-35	
	04/18	TY		0	83		189			-5	37	30	16		0	-40	-40	-25	
	05/00	TY		0		175		-10		15	39	31	10		-15	-40	-40		
	05/06	TY		0	99	160				25	39	33			-20	-40	-40		
	05/12	TY	TY	0	80	103	61			25	34	26			-20	-35	-35		
	05/18	TY		0	98	84	43			35	28	14			-30	-35	-25		
	06/00	TY		0	91	70	43			30	23	10			-25	-25	-15		
	06/06	TY		0	46	15				20	15				-15	-10			
	06/12	TY	TY	0	24	68				15	10				-10	-5			
	06/18	TY		0	22	88				0	-2				0	5			
	07/00	TY		0	56	103				-5	-13				5	20			
	07/06	TY		0	57					-5					5				
	07/12	TY	TY	11	56					-10					10				
	07/18	TY	TY	11	39					-7					10				
	08/00	TY	TY	15	53					-6					10				
	08/06	TY	TY	0															
	08/12	TY	TY	0															
	08/18	STS	STS	0															
	09/00	TS	TS	10															
	09/06	TD	TS																
	09/12	TD	TD																
T .*** 1 .	TO IOTO "	FW 7				105	121	150	2:-				40						
Initial:			mean	5	64		134		215	7	17	19	19	16	-7 24		-22		-22
Valid: T			sample	38	100	242	210	220	17	34	30	26	21	17	34	30	26	21	25
Initial: T			mean	0	_		310	_	144	1	8	40	48	40	-3	-15	-40	-43	-35
vana: T	D/TS/ST	<b>Y/ I Y</b>	sample	2	<u>2</u>	<u>2</u>	<u>2</u>	2	2	2	2	2	2	2	2	2	2	2	2

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gr	ade		Cent	er Pos	sition	(km)		Cer	ntral F	ressu	re (hl	Pa)	1	Max.	Wind	(kt) <sup>†</sup>	<del></del>
	(UTC)	Best	Prov.	T=0 <sup>‡</sup>				` ′	=120				,	· ·	T=24				=120
	` /			1-0					en(23										
Oct.	06/12	TD	TD	11	101	230	240	341	220	2	2	0	10	65	0	-5	-5	-15	-45
	06/18	TD	TD	35	67	109	144	187	148	2	6	0	15	50	0	-10		-15	-35
	07/00	TD	TD	16	25	11	167	201	300	0	2	-5	20	35	5	-5	0	-20	-25
	07/06	TD	TS	49	25	35	181	192	330	-4	-15	-20	30	30	5	10	10	-20	-20
	07/12	TS	TS	0	55	88	186	140	269	-6	-25	-20	35	30	10	20	10	-25	-20
	07/18	TS	TS	0	40	90	128	111	397	-2	-20	-5	35	15	5	15	0	-25	-10
	08/00	TS	TS	11	49	104	67	143	548	0	-15	15	35	10	0	10	-15	-25	-5
	08/06	TS	TS	44	64	123	59	123	544	-5	-20	30	30	-10	5	10	-20	-20	5
	08/12	TS	TS	35	64	89		176	689	-5	-10	35	20	-10	5	5	-20	-15	10
	08/18	STS	STS	25	43	58	33	132	613	-10	0	35	5	-10	10	0	-20	-5	10
	09/00	STS	STS	11	73	31	24		749	-15	5	20	-5	-15	10	-10	-15	0	10
	09/06	STS	STS	11	48	11		349	963	-10	30	20	-15	-15	5	-20	-15	5	15
	09/12	STS	STS	11	24	44	98			-5	35	20	-15		0	-25	-15	10	
	09/18	STS		25	54	53				0	30	5	-20		-5	-20	-5	10	
	10/00	TY		0	68	43				15	30	0	-15		-15	-20	0	10	
	10/06	TY			15	74		871		40	20	-10	-5		-25	-15	5	10	
	10/12 10/18	TY TY			15	84 113	427			35 20	20 5	-10 -20			-25 -15	-15 -5	10 10		
	11/00	TY				172	581			10	-5	-20 -15			-15 -10	-5	10		
	11/06	TY			33		634			0	-15	-15 -5			-10 -5	5	10		
	11/00	TY			38		034			-5	-15	-3			0	10	10		
	11/12	TY			55	343				-15	-20				5	10			
	12/00	TY								-20	-25				10	15			
	12/06	TY			118					-20	-15				10	15			
	12/12	TY	TY	15	147					-25					15				
	12/18	TY	TY	10	188					-25					15				
	13/00	TY	TY	11	230					-25					15				
	13/06	TY	TY	10	177					-5					10				
	13/12	TY	TY	31															
	13/18	TY	TY	44															
	14/00	TY	TY																
	14/06	TY	TY	24															
Initial:	TS/STS/	ΓY	mean	14	73	148	218	331	597	-3	-1	6	7	-1	1	-1	-4	-6	2
Valid: T	S/STS/T	Y	sample	28	24	20	16	12	8	24	20	16	12	8	24	20	16	12	8
Initial: T	TD(before	e upg.)	mean	28	54	96	183	230	249	0	-1	-6	19	45	3	-3	0	-18	-31
Valid: T	D/TS/STS	S/TY	sample	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gra	ade		Cent	er Pos	sition	(km)		Cer	ntral F	ressu	re (hF	Pa)		Max.	Wind	(kt) <sup>†</sup>	-
	(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120
								Sank	oa(231	6)									
Oct.	17/06	TD	TD	0	25	152	269			-2	-4	-6			0	5	5		
	17/12	TD	TD	11	46	222				-2	-2				0	0			
	17/18	TD	TD	0	34	198				-2	-2				0	5			
	18/00	TS	TD	11	43					0					0				
	18/06	TS	TS	25	74					-2					5				
	18/12	TS	TS	22	144					-2					5				
	18/18	TS	TS	<b>79</b>	130					-4					10				
	19/00	TS	TS	39															
	19/06	TS	TS	64															
	19/12	TS	TS	11															
	19/18	TS	TS	0															
	20/00	TD	TS																
	20/06	TD	TS																
Initial:	TS/STS/	ΓY	mean	31	98					-2					5				
Valid: T	S/STS/T	Y	sample	8	4	0	0	0	0	4	0	0	0	0	4	0	0	0	0_
Initial: T	TD(before	e upg.)	mean	4	35	190	269			-2	-3	-6			0	3	5		
Valid: T	D/TS/ST	S/TY	sample	3	3	3	1	0	0	3	3	1	0	0	3	3	1	0	0

<sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

Date/	Time	Gr	ade		Cent	er Pos	sition	(km)		Cei	ntral F	ressu	re (hF	Pa)		Max.	Wind	(kt) <sup>†</sup>	
	(UTC)	Best	Prov.	$T=0^{\ddagger}$	=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120	T=24	=48	=72	=96	=120
	-							Jelav	vat(23)	17)									
Dec.	16/00	TD	TD	35	129	180				-4	-6				5	5			
	16/06	TD	TD	11	145	228				-2	-4				0	5			
	16/12	TD	TD	63	80					2					0				
	16/18	TD	TD	102	135					0					0				
	17/00	TD	TS	149	214					-6					5				
	17/06	TS	TS	66															
	17/12	TS	TS	55															
	17/18	TS	TS	47															
	18/00	TD	TD																
	TS/STS/T		mean	56															
_Valid: T	S/STS/T	Y	sample	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Initial: T	TD(before	e upg.)	mean	72	141	204				-2	-5				2	5			
Valid: T	D/TS/ST	S/TY	sample	5	5	2	0	0	0	5	2	0	0	0	5	2	0	0	0

<sup>&</sup>lt;sup>†</sup>Max. wind for TDs are treated as 30 kt in this validation

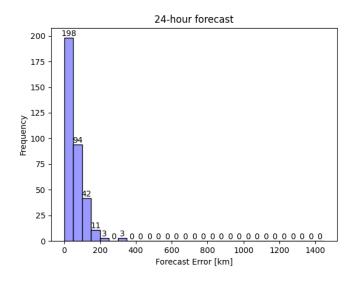
<sup>&</sup>lt;sup>‡</sup>Position error of provisional analysis

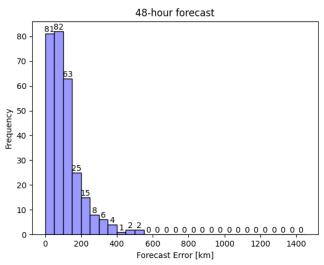
Appendix 4
Monthly and Annual Frequencies of Tropical Cyclones

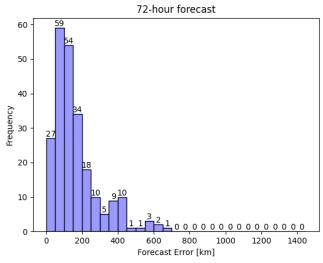
Monthly and annual frequencies of tropical cyclones that attained TS intensity or higher in the western North Pacific and the South China Sea for 1951 - 2023

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
1951		1	1	2	1	1	3	3	2	4	1	2	21
1952						3	3	5	3	6	3	4	27
1953		1			1	2	1	6	3	5	3	1	23
1954			1		1		1	5	5	4	3	1	21
1955	1	1	1	1		2	7	6	4	3	1	1	28
1956			1	2		1	2	5	6	1	4	1	23
1957	2			1	1	1	1	4	5	4	3		22
1958	1			1	1	4	7	5	5	3	2	2	31
1959		1	1	1			2	5	5	4	2	2	23
1960				1	1	3	3	10	3	4	1	1	27
1961	1		1		2	3	4	6	6	4	1	1	29
1962		1		1	2		5	8	4	5	3	1	30
1963				1		4	4	3	5	4		3	24
1964					2	2	7	5	6	5	6	1	34
1965	2	1	1	1	2	3	5	6	7	2	2		32
1966				1	2	1	4	10	9	5	2	1	35
1967		1	2	1	1	1	7	9	9	4	3	1	39
1968				1	1	1	3	8	3	5	5		27
1969	1		1	1			3	4	3	3	2	1	19
1970		1				2	3	6	5	5	4		26
1971	1		1	3	4	2	8	5	6	4	2		36
1972	1		-	-	1	3	7	5	4	5	3	2	31
1973							7	5	2	4	3		21
1974	1		1	1	1	4	4	5	5	4	4	2	32
1975	1		•	•	•		2	4	5	5	3	1	21
1976	1	1		2	2	2	4	4	5	1	1	2	25
1977	•	•	1	_	-	1	3	3	5	5	1	2	21
1978	1		1	1		3	4	8	5	4	4	2	30
1979	1		1	1	2	5	4	2	6	3	2	2	24
1980			1	1	4	1	4	2	6	4	1	1	24
1981			1	2		3	4	8	4	2	3	2	29
1982			3		1	3	3	5	5	3	1	1	25
1983			3		1	1	3	5	2	5	5	2	23
1984						2	5	5	4	7	3	1	27
	2				1	3	1	8	5	4	1	2	
1985	2	1		1	1 2	2	4	4	3	5	4	3	27 29
1986	1	1		1	2					2			
1987	1			1		2	4	4	6		2	1	23
1988	1				1	3	2	8	8	5	2	1	31
1989	1			1	2	2	7	5	6	4	3	1	32
1990	1			1	1_	3_	4	6	4	4	4	1	29
1991			2	1	1	1	4	5	6	3	6		29
1992	1	1				2	4	8	5	7	3	_	31
1993			1			1	4	7	6	4	2	3	28
1994				1	1	2	7	9	8	6		2	36
1995				1		1	2	6	5	6	1	1	23
1996		1		1	2		6	5	6	2	2	1	26
1997				2	3	3	4	6	4	3	2	1	28
1998							1	3	5	2	3	2	16
1999				2		1	4	6	6	2	1		22
2000					2		5	6	5	2	2	1	23
2001						2	5	6	5	3	1	3	26
2002	1	1			1	3	5	6	4	2	2	1	26
2003	1			1	2	2	2	5	3	3	2		21
2004				1	2	5	2	8	3	3	3	2	29
2005	1		1	1	1		5	5	5	2	2		23
2006					1	2	2	7	3	4	2	2	23
2007				1	1		3	4	5	6	4		24
2008				1	4	1	2	4	4	2	3	1	22
2009					2	2	2	5	7	3	1		22
2010			1				2		4	2			14
2011					2	3	4	<u>5</u>	7	1	***************************************	1	21
2012			1		1	4	4	5	3	5	1	1	25
2013	1	1				4	3	6	8	6	2		31
2014	2	1		2		2	5	1	5	2	1	2	23
2015	1	1	2	1	2	2	3	4	5	4	1	1	27
2016			_		_	-	4	7	7	4	3	1	26
2017				1		1	8	6	3	3	3	2	27
2017	1	1	1	1		4	5	9	4	1	3	2	29
2019	1	1	1			1	4	5	6	4	6	1	29
2019	1	1			1	1	4	8	3	6	3	1	23
2020		1		1	<u>1</u>	<u>1</u>	3	<u>0</u> .	<u>3</u> .	4	<u>3</u> .	<u>1</u>	22
		1		2	1	2	2	5	7				
2022				1	1	1	3		2	5 2	1	1 1	25 17
2023	-	-		1	1	1	3	6				1	17
Normal													
1991-2020	0.3	0.3	0.3	0.6	1.0	1.7	3.7	5.7	5.0	3.4	2.2	1.0	25.1

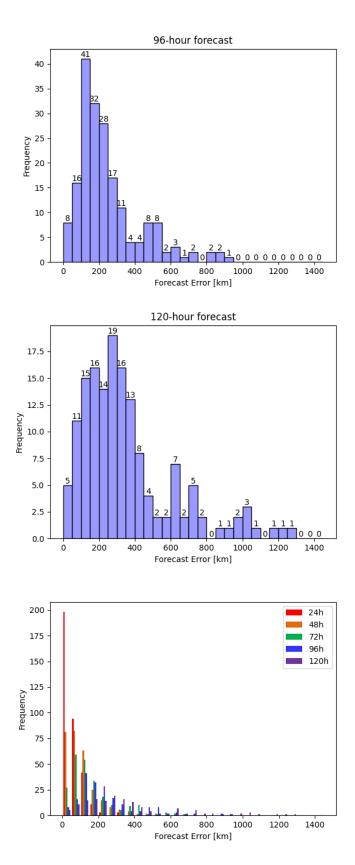
# **Appendix 5 Other Verification Charts**



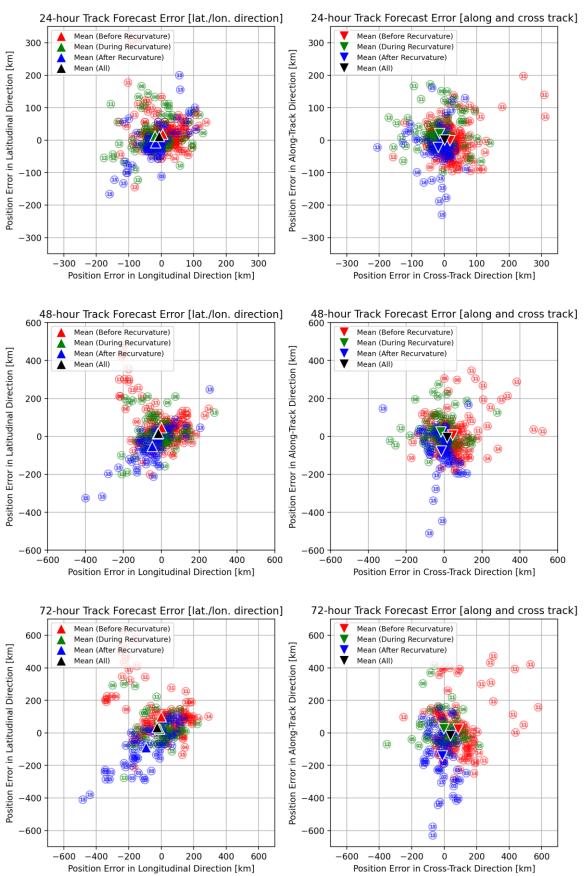




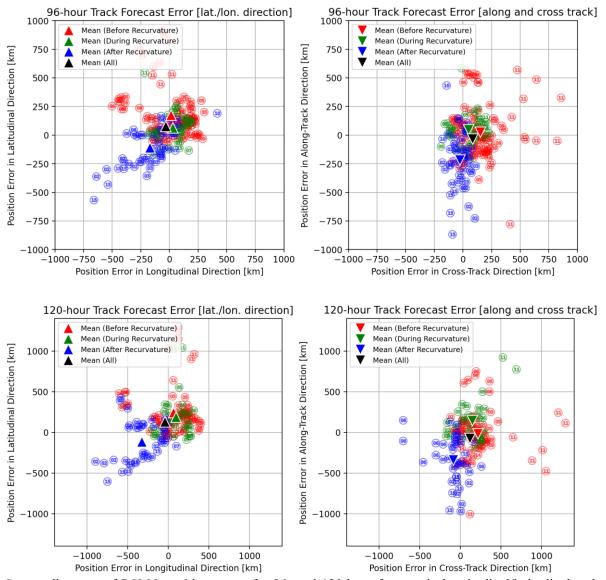
Histograms of RSMC 24-, 48- and 72 hour forecast position errors



Histograms of RSMC 96-hour, 120-hour and all lead time forecast position errors



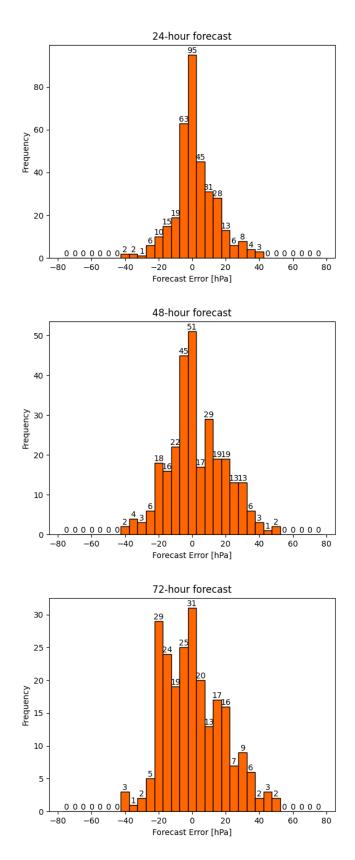
Scatter diagrams of RSMC position errors for 24-, 48- and 72-hour forecast in longitudinal/latitudinal and cross/along-track directions: Red, green and blue circles with TC number and triangles denote biases for each initial time and mean biases in the stages before, during and after recurvature, respectively. Black triangles indicate mean bias for all initial time.



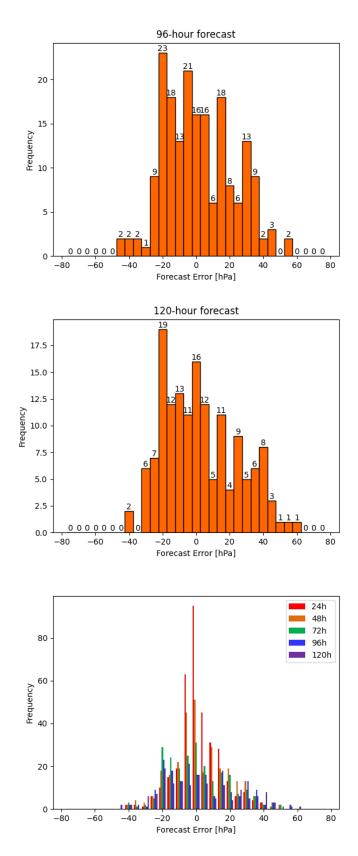
Scatter diagrams of RSMC position errors for 96- and 120-hour forecast in longitudinal/latitudinal and cross/along-track directions: Red, green and blue circles with TC number and triangles denote biases for each initial time and mean biases in the stages before, during and after recurvature, respectively. Black triangles indicate mean bias for all initial time.

Annual mean errors, RMSEs and mean improvement ratios of RSMC maximum wind speed forecasts

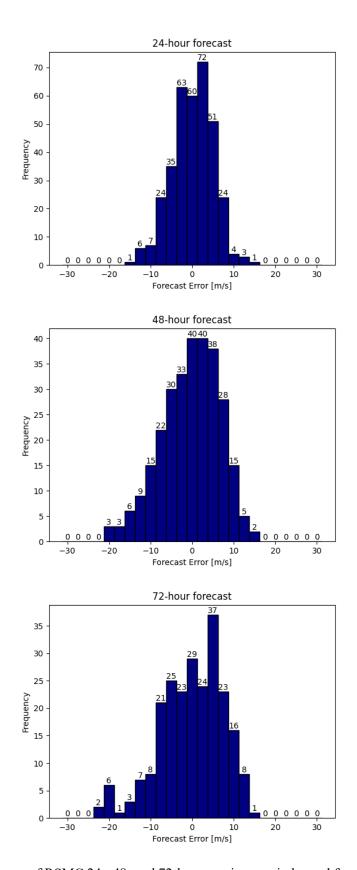
	-	×	2	24-hour Fo	orecast	-		18-hour I	Forecas	t	-	2-hour F	orecas	t	9	6-hour F	Forecas	t	1	20-hour F	orecas	t
	Tropical Cyc	lone	Error	RMSE 1	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE	Num.	Impr.	Error	RMSE 1	Num.	Impr.
			(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)	(m/s)	(m/s)		(%)
TS	Sanvu	(2301)	-1.3	1.8	2	76	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TY	Mawar	(2302)	0.3	6.2	50	6	0.6	8.1	46	19	1.9	7.2	42	40	2.6	7.1	38	47	2.7	7.4	34	49
TY	Guchol	(2303)	-1.5	3.8	20	13	-0.5	4.3	16	40	2.6	4.8	12	39	7.1	8.4	8	-56	10.3	10.4	4	-613
STS	Talim	(2304)	0.3	1.9	9	53	2.1	3.3	5	23	15.4	15.4	1	-1011	-	-	0	-	-	-	0	-
TY	Doksuri	(2305)	0.6	4.3	28	39	-0.4	5.6	24	43	-0.5	4.9	20	61	-3.2	7.0	16	49	-1.5	5.9	12	47
TY	Khanun	(2306)	1.6	5.0	49	-5	2.6	7.3	45	9	4.1	8.8	41	7	4.0	10.3	37	-13	2.3	12.9	33	-75
TY	Lan	(2307)	-0.7	5.1	33	-1	-1.1	6.0	29	28	-0.6	5.5	25	41	1.6	4.9	21	40	1.8	4.3	17	31
TY	Dora	(2308)	2.9	4.1	7	65	6.9	7.6	3	64	-	-	0	-	-	-	0	-	-	-	0	-
TY	Saola	(2309)	-1.4	5.6	34	31	-0.9	6.5	30	49	1.1	6.6	26	54	-0.7	8.9	22	47	-5.7	12.1	18	40
STS	Damrey	(2310)	-0.4	3.1	14	12	-1.3	3.4	10	41	-3.0	3.5	6	63	-5.1	5.8	2	48	-	-	0	
TY	Haikui	(2311)	2.6	5.3	25	13	1.2	5.3	21	31	0.3	5.4	17	25	-5.9	7.1	13	4	-5.4	7.5	9	1
TS	Kirogi	(2312)	2.6	3.6	10	45	3.9	5.0	6	68	2.6	2.6	2	88	-	-	0	-	-	-	0	-
TS	Yun-yeung	g (2313)	1.6	2.0	8	-6	3.2	3.4	4	32	-	-	0	-	-	-	0	-	-	-	0	-
TY	Koinu	(2314)	-3.5	6.0	34	10	-8.7	11.4	30	-10	-11.5	13.9	26	-15	-12.2	15.8	21	-30	-11.3	16.1	17	-41
TY	Bolaven	(2315)	0.6	6.0	24	-2	-0.4	7.2	20	26	-2.3	6.6	16	43	-3.0	8.1	12	35	1.0	6.0	8	37
TS	Sanba	(2316)	2.6	3.2	4	-31	-	-	0	-	-	-	0	-	-	-	0	-	-	-	0	-
TS	Jelawat	(2317)			0				0				0				0				0	
	Annual Mean (	Total)	0.1	5.1	351	17	-0.4	7.2	289	26	-0.2	7.9	234	30	-0.6	9.2	190	22	-0.8	10.4	152	14



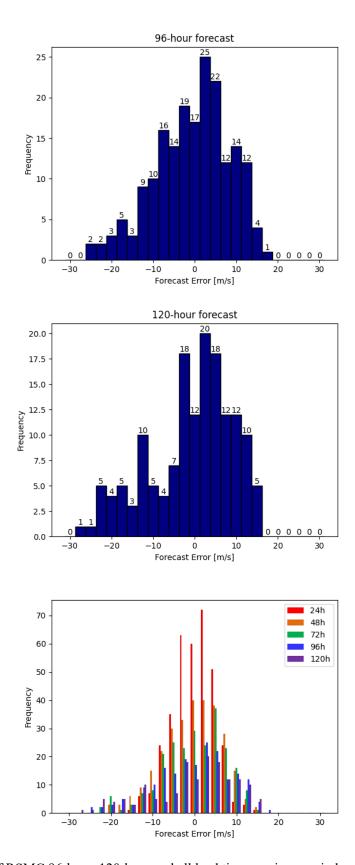
Histograms of RSMC 24-, 48- and 72-hour pressure forecast errors



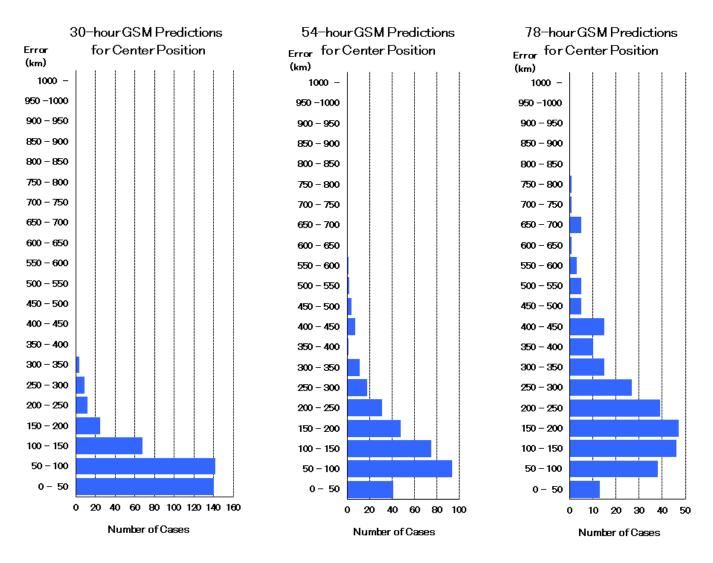
Histograms of RSMC 96-hour, 120-hour and all lead time pressure forecast errors



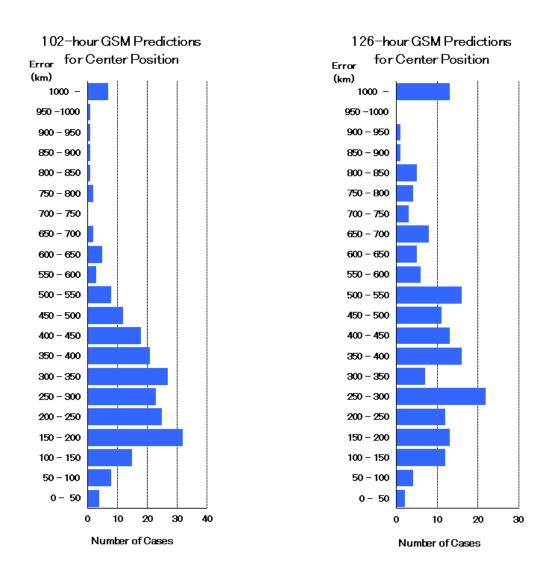
Histograms of RSMC 24-, 48- and 72-hour maximum wind speed forecast errors



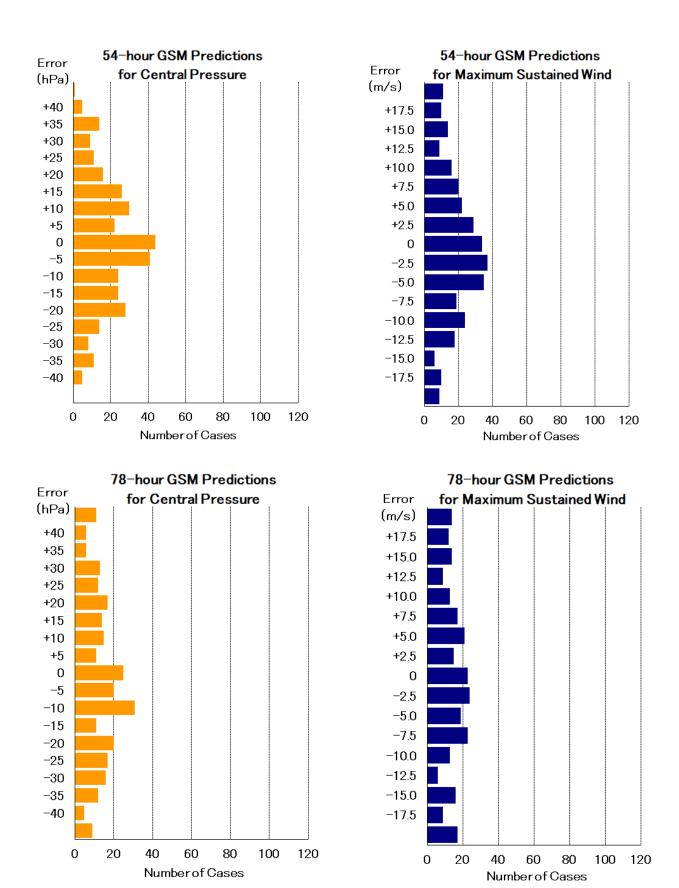
Histograms of RSMC 96-hour, 120-hour and all lead time maximum wind speed forecast errors



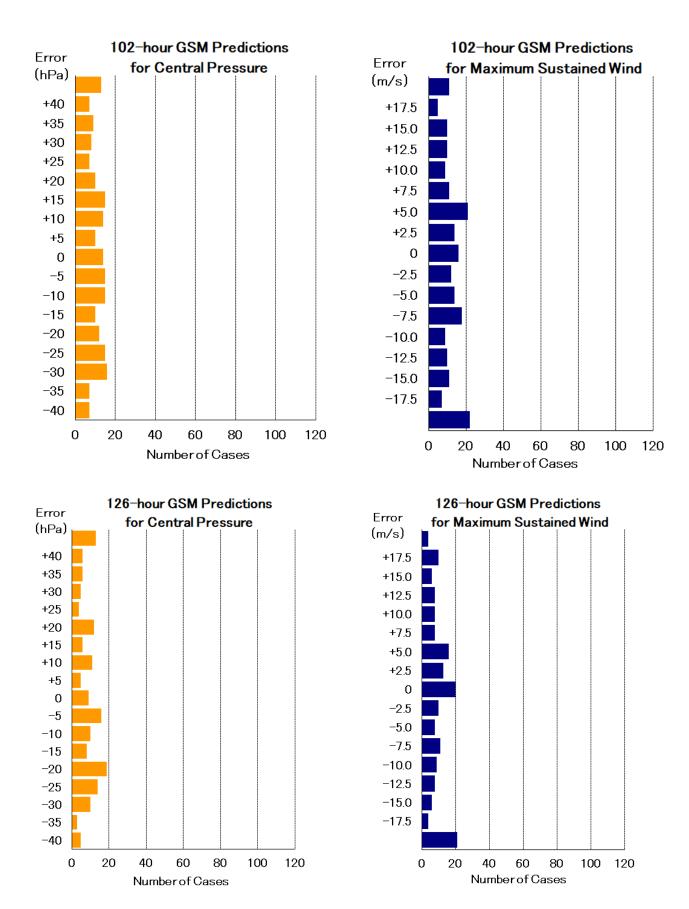
Histograms of GSM position errors for 30-, 54-, and 78-hour prediction



Histograms of GSM position errors for 102- and 126-hour prediction



Histograms of GSM intensity errors for (top) 54- and (bottom) 78-hour prediction



Histograms of GSM intensity errors for (top) 102- and (bottom) 126-hour prediction

# Appendix 6 Code Forms of RSMC Products

#### (1) RSMC Tropical Cyclone Advisory (WTPQ50-55 RJTD)

WTPQii RJTD YYGGgg

RSMC TROPICAL CYCLONE ADVISORY

NAME class ty-No. name (common-No.)

**ANALYSIS** 

PSTN YYGGgg UTC LaLa.La N LoLoLo.Lo E (or W) confidence

MOVE direction SpSpSp KT

PRES PPPP HPA

 $\underline{MXWD}$  VmVmVm  $\underline{KT}$ 

GUST VgVgVg KT

50KT RdRdRd NM (or 50KT RdRdRd NM octant RdRdRd NM octant)
30KT RdRdRd NM (or 30KT RdRdRd NM octant RdRdRd NM octant)

**FORECAST** 

24HF YYGGggF UTC LaLa.LaF N LoLoLo.LoF E (or W) FrFrFr NM 70%

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

GUST VgVgVg KT

Ft1Ft1<u>HF</u> YYGGggF <u>UTC</u> LaLa.LaF N LoLoLo.LoF E (or W) FrFrFr <u>NM 70%</u>

MOVE direction SpSpSp KT

PRES PPPP HPA

GUST VgVgVg KT

MXWD VmVmVm KT

Ft2Ft2<u>HF</u> YYGGggF <u>UTC</u> LaLa.La<sub>F</sub> N LoLoLo.Lo<sub>F</sub> E (or W) FrFrFr <u>NM 70%</u>

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

GUST VgVgVg KT

 $Ft3Ft3\underline{HF}\ YYGGggF\ \underline{UTC} \quad LaLa.La_F\ N\ LoLoLo.Lo_F\ E\ (or\ W)\ FrFrFr\ \underline{NM\ 70\%}$ 

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

 $\underline{GUST}\,VgVgVg\,\underline{KT}$ 

 $Ft4Ft4Ft4\underline{HF}\ YYGGgg_F\underline{UTC}\quad LaLa.La_F\ N\ LoLoLo.Lo_F\ E\ (or\ W)\ FrFrFr\ \underline{NM\ 70\%}$ 

MOVE direction SpSpSp KT

PRES PPPP HPA

MXWD VmVmVm KT

GUST VgVgVg KT=

#### Notes:

#### a. <u>Underlined</u> parts are fixed.

b. Abbreviations

PSTN : Position

MOVE : Movement

PRES : Pressure

MXWD : Maximum wind

HF : Hour forecast

c. Symbolic letters

i i : '20', '21', '22', '23', '24' or '25'

YYGGgg : Time of observation submitting the data for analysis in UTC

class : Intensity classification of the tropical cyclone 'TY', 'STS', 'TS' or 'TD'

ty-No. : Domestic identification number of the tropical cyclone adopted in Japan given in four digits (same as the

international identification number)

name : Name assigned to the tropical cyclone from the name list prepared by the Typhoon Committee

common-No. : International identification number of the tropical cyclones given in four digits

LaLa.La : Latitude of the center position in "ANALYSIS" part

LoLoLo.Lo : Longitude of the center position in "ANALYSIS" part

confidence : Confidence of the center position. 'GOOD', 'FAIR' or 'POOR'

direction : Direction of movement given in 16 azimuthal direction such as 'N', 'NNE', 'NE' and 'ENE'

SpSpSp : Speed of movement
PPPP : Central pressure
VmVmVm : Maximum sustained wind
VgVgVg : Maximum gust wind

RdRdRd : Radii of 30knots and 50knots wind

octant : Eccentric distribution of wind given in 8 azimuthal direction such as 'NORTH', 'NORTHEAST' and 'EAST'

Ft1Ft1 : 48 (00, 06, 12 and 18 UTC) or 45 (03, 09, 15 and 21 UTC)
Ft2Ft2 : 72 (00, 06, 12 and 18 UTC) or 69 (03, 09, 15 and 21 UTC)
Ft3Ft3 : 96 (00, 06, 12 and 18 UTC) or 93 (03, 09, 15 and 21 UTC)
Ft4Ft4 Ft4 : 120 (00, 06, 12 and 18 UTC) or 117 (03, 09, 15 and 21 UTC)

YYGGgg<sub>F</sub> : Time in UTC on which the forecast is valid

LaLa.La<sub>F</sub> : Latitude of the center of 70% probability circle in "FORECAST" part
LoLoLo.Lo<sub>F</sub> : Longitude of the center of 70% probability circle in "FORECAST" part

FrFrFr : Radius of 70% probability circle

d. MOVE is optionally described as 'ALMOST STATIONARY' or '(direction) SLOWLY', depending on the speed of movement.

#### Example:

WTPQ50 RJTD 080000
RSMC TROPICAL CYCLONE ADVISORY
NAME TY 1919 HAGIBIS (1919)
ANALYSIS
PSTN 080000UTC 16.9N 143.8E GOOD
MOVE WNW 13KT
PRES 915HPA
MXWD 105KT
GUST 150KT
50KT 100NM
30KT 350NM EAST 240NM WEST
FORECAST
24HF 090000UTC 19.8N 140.0E 60NM 70%
MOVE NW 10KT
PRES 915HPA
MXWD 105KT
GUST 150KT
48HF 100000UTC 22.8N 138.4E 90NM 70%
MOVE NW 08KT
PRES 915HPA
MXWD 105KT
GUST 150KT
48HF 100000UTC 26.5N 136.3E 120NM 70%
MOVE NNW 08KT
PRES 925HPA
MXWD 105KT
GUST 150KT
72HF 110000UTC 26.5N 136.3E 120NM 70%
MOVE NNW 10KT
PRES 925HPA
MXWD 100KT
GUST 140KT
96HF 120000UTC 31.6N 135.9E 170NM 70%
MOVE N 13KT
PRES 940HPA
MXWD 090KT
GUST 130KT
120HF 130000UTC 37.5N 142.5E 240NM 70%
MOVE NE 20KT
PRES 980HPA
MXWD 060KT

#### (2) RSMC Guidance for Forecast by GSM (FXPQ20-25 RJTD)

FXPQ i i RJTD YYGGgg RSMC GUIDANCE FOR FORECAST

NAME class ty-No. name (common-No.)

PSTN YYGGgg UTC LaLa.La N LoLoLo.Lo E (or W)

PRES PPPP HPA

GUST 085KT =

MXWD WWW KT

FORECAST BY GLOBAL MODEL

<u>MXW</u>D PRES TIME **PSTN** 

(CHANGE FROM T=0)

T=006 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=012 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=018 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

<u>T=132</u> LaLa.La N LoLoLo.Lo E (or W) appp <u>HPA</u> awww <u>KT=</u>

#### Notes:

Underlined parts are fixed.

Symbolic letters

'20', '21', '22', '23', '24' or '25' YYGGgg Initial time of the model in UTC

class Intensity classification of the tropical cyclone 'T', 'STS', 'TS' or 'TD'

PPPP Central pressure in hPa WWW Maximum wind speed in knots a Sign of ppp and www (+, - or blank)

Absolute value of change in central pressure from T=0, in hPa ppp Absolute value of change in maximum wind speed from T=0, in knots www

#### Example:

FXPQ20 RJTD 180600

RSMC GUIDANCE FOR FORECAST NAME TY 0001DANEY (0001)

PSTN 180000UTC 15.2N 126.3E

PRES 905HPA MXWD 105KT

FORECAST BY GLOBAL MODEL

PRES MXWD (CHANGE FROM T=0) TIME PSTN

T=006 15.4N 125.8E +018HPA -008KT

T=012 15.5N 125.6E +011HPA -011KT T=018 15.8N 125.7E +027HPA -028KT

T=132 20.7N 128.8E +021HPA -022KT=

### (3) RSMC Guidance for Forecast by GEPS (FXPQ30-35 RJTD)

FXPQii RJTD YYGGgg

RSMC GUIDANCE FOR FORECAST

NAME class ty-No. name (common-No.)

PSTN YYGGgg UTC LaLa.La N LoLoLo.Lo E (or W)

PRES PPPP HPA

MXWD WWW KT

FORECAST BY GLOBAL ENSEMBLE PREDICTION SYSTEM

TIME **PSTN PRES** MXWD

(CHANGE FROM T=0)

T=006 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=012 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=018 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT

T=132 LaLa.La N LoLoLo.Lo E (or W) appp HPA awww KT=

#### **Notes:**

a. <u>Underlined</u> parts are fixed.

#### b. Symbolic letters

'30', '31', '32', '33', '34' or '35'

YYGGgg Initial time of the model in UTC

class Intensity classification of the tropical cyclone 'T', 'STS', 'TS' or 'TD'

PPPP Central pressure in hPa WWW Maximum wind speed in knots Sign of ppp and www (+, - or blank)

Absolute value of change in central pressure from T=0, in hPa ppp www Absolute value of change in maximum wind speed from T=0, in knots

#### Example:

FXPQ30 RJTD 231200 RSMC GUIDANCE FOR FORECAST NAME TY 1826 YUTU (1826) PSTN 231200UTC 12.0N 149.6E PRES 965HPA MXWD 75KT

FORECAST BY GLOBAL ENSEMBLE PREDICTION SYSTEM

PRES MXWD (CHANGE FROM T=0) **PSTN** TIME T=006 12.7N 149.1E -002HPA +001KT T=012 13.2N 148.3E -001HPA +004KT T=018 13.8N 147.6E -005HPA +004KT

T=132 18.0N 129.9E -033HPA +030KT=

#### (4) RSMC Prognostic Reasoning (WTPQ30-35 RJTD)

#### **Example:**

WTPQ30 RJTD 231200

RSMC TROPICAL CYCLONE PROGNOSTIC REASONING REASONING NO.10 FOR TY 1826 YUTU (1826)

1.GENERAL COMMENTS

TY YUTU IS LOCATED AT 12.0N, 149.6E. INFORMATION ON THE CURRENT POSITION IS BASED ON ANIMATED MSI. POSITIONAL ACCURACY IS GOOD. THE SYSTEM IS IN A FAVORABLE ENVIRONMENT FOR DEVELOPMENT UNDER THE INFLUENCE OF HIGH SSTS, HIGH TCHP AND WEAK VWS. THIS HAS CAUSED THE SYSTEM TO DEVELOP OVER THE LAST SIX HOURS. HOWEVER, THE INFLUENCE OF DRY AIR IS UNFAVORABLE FOR SYSTEM DEVELOPMENT. INFORMATION ON CURRENT INTENSITY IS BASED ON DVORAK INTENSITY ANALYSES.

2.SYNOPTIC SITUATION

THE SYSTEM IS MOVING WESTWARD ALONG THE SOUTHERN PERIPHERY OF A MID-LEVEL SUB-TROPICAL HIGH. ANIMATED MSI SHOWS THE APPEARANCE OF AN EYE. WATER VAPOR IMAGERY SHOWS DRY AIR IN THE DIRECTION OF THE MOVEMENT. DMSP-F18/SSMIS 89 GHZ MICROWAVE IMAGERY SHOWS THE SYSTEM HAS A BAND WITH CURVATURE INDICATING THE CSC.

3.TRACK FORECAST

THE SYSTEM WILL MOVE NORTHWESTWARD ALONG THE PERIPHERY OF A MID-LEVEL SUB-TROPICAL HIGH UNTIL FT12. THE SYSTEM WILL THEN MOVE WEST-NORTHWESTWARD ALONG THE PERIPHERY OF A MID-LEVEL SUB-TROPICAL HIGH UNTIL FT120. THE JMA TRACK FORECAST IS BASED ON GSM PREDICTIONS, AND REFERENCE TO OTHER NWP MODELS. JMA TRACK FORECAST CONFIDENCE IS FAIR UNTIL FT48 BUT LOW THEREAFTER DUE TO SIGNIFICANT DIFFERENCES AMONG NUMERICAL MODEL OUTPUTS.

4.INTENSITY FORECAST

THE SYSTEM WILL DEVELOP UNTIL FT48 DUE TO THE INFLUENCE OF INTERACTION WITH HIGH SSTS, HIGH TCHP, WEAK VWS AND GOOD UPPER LEVEL OUTFLOW. THE SYSTEM WILL THEN MAINTAIN ITS INTENSITY UNTIL FT72 DUE TO THE INFLUENCE OF INTERACTION WITH HIGH SSTS, HIGH TCHP AND DRY AIR. THE JMA INTENSITY FORECAST IS BASED ON GUIDANCE DATA. =

#### (5) RSMC Tropical Cyclone Best Track (AXPQ20 RJTD)

AXPQ20 RJTD YYGGgg

RSMC TROPICAL CYCLONE BEST TRACK

NAME ty-No. name (common-No.)

PERIOD FROM MMMDDTTUTC TO MMMDDTTUTC

DDTT LaLa.LaN LoLoLo.LoE PPPHPA WWWKT DDTT LaLa.LaN LoLoLo.LoE PPP<u>HPA</u> WWW<u>KT</u> DDTT LaLa.LaN LoLoLo.LoE PPP $\underline{HPA}$  WWW $\underline{KT}$ DDTT LaLa.LaN LoLoLo.LoE PPPHPA WWWKT

DDTT LaLa.LaN LoLoLo.LoE PPP<u>HPA</u> WWW<u>KT</u> DDTT LaLa.LaN LoLoLo.LoE PPP<u>HPA</u> WWW<u>KT</u>

REMARKS1)

TD FORMATION AT MMMDDTT<u>UTC</u> FROM TD TO TS AT MMMDDTTUTC

DISSIPATION AT MMMDDTT<u>UTC=</u>

#### **Notes:**

- Underlined parts are fixed.
- 1) REMARKS is given optionally.
- c. Symbolic letters

MMM Month in UTC given such as 'JAN' and 'FEB'

DD Date in UTC TT Hour in UTC PPP Central pressure WWW : Maximum wind speed

#### Example:

AXPQ20 RJTD 020600

RSMC TROPICAL CYCLONE BEST TRACK
NAME 0001 DAMREY (0001)
PERIOD FROM OCT1300UTC TO OCT2618UTC
1300 10.8N 155.5E 1008HPA //KT 1306 10.9N 153.6E 1006HPA //KT
1312 11.1N 151.5E 1004HPA //KT 1318 11.5N 149.8E 1002HPA //KT
1400 11.9N 148.5E 1000HPA //KT 1406 12.0N 146.8E 998HPA 35KT

1712 14.6N 129.5E 905HPA 105KT 1718 14.7N 128.3E 905HPA 105KT

2612 32.6N 154.0E 1000HPA //KT 2618 33.8N 157.4E 1010HPA //KT

REMARKS

TD FORMATION FROM TD TO TS FROM TS TO ST AT OCT1300UTC TO TS TO STS AT OCT1406UTC AT OCT1512UTC FROM STS TO TY FROM TY TO STS AT OCT1600UTC TO STS AT OCT2100UTC FROM STS TO TS FROM TS TO L AT OCT2112UTC AT OCT2506UTC DISSIPATION AT OCT2700UTC=

#### (6) Tropical Cyclone Advisory for SIGMET (FKPQ30-35 RJTD)

FKPQ i i RJTD YYGGgg

TC ADVISORY

DTG: yyyymmdd/time Z

TCAC: **TOKYO** TC: name NR: number

PSN: N LaLa.LaLa E LoLoLo.LoLo

MOV: direction SpSpSp KT

PPPP HPA <u>C:</u> MAX WIND: WWW KT

FCST PSN +6HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo\*

FCST MAX WIND +6HR: WWW KT\*

FCST PSN +12HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo

FCST MAX WIND +12HR: WWW KT

FCST PSN +18HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo\* FCST MAX WIND +18HR: YY/GGgg Z NLaLa.LaLa ELoLoLo.LoLo\* FCST PSN +24HR: YY/GGgg Z N LaLa.LaLa E LoLoLo.LoLo

FCST MAX WIND +24HR: WWW KT RMK: NIL =

NXT MSG: yyyymmdd/time Z

#### **Notes:**

#### Underlined parts are fixed.

Abbreviations

DTG Date and time

**TCAC** Tropical Cyclone Advisory Centre

TC Tropical Cyclone

NR Number PSN Position MOV Movement C Central pressure MAX WIND Maximum wind **FCST** Forecast RMK Remarks NXT MSG Next message

c. Symbolic letters

'30', '31', '32', '33', '34' or '35' ii

Date(YY), hour(GG) and minute(gg) in UTC (Using "Z") YYGGgg

Year(yyyy), month(mm), date(dd), hour and minute (time) in UTC (Using "Z") yyyymmdd/time Name assigned to the tropical cyclone by RSMC Tokyo-Typhoon Center name

Advisory number (starting with "01" for each cyclone) Number

LaLa.LaLa Latitude of the center position LoLoLo.LoLo Longitude of the center position

Direction of movement given in 16 azimuthal direction such as 'N', 'NNE', 'NE' and 'ENE' direction

Speed of movement. "SLW" for less than 3 kt "STNR" for less than 1 kt. SpSpSp

PPPP Central pressure

WWW Maximum sustained wind

#### Example:

FKPQ30 RJTD 271200

TC ADVISORY DTG: 20080927/1200Z TCAC: TC: TOKYO JANGMI NR: 15 N2120 E12425 PSN: NW 13KT MOV: 910HPA

C: MAX WIND: FCST PSN +6HR: FCST MAX WIND +6HR: FCST PSN +12HR: FCST MAX WIND +12HR: FCST PSN +18HR: FCST MAX WIND +18HR: FCST PSN +24HR: FCST MAX WIND +24HR: RMK: 115KT 27/1800Z N2200 E12330

115KT 28/0000Z N2240 E12250

115KT 28/0600Z N2340 E12205

95KT

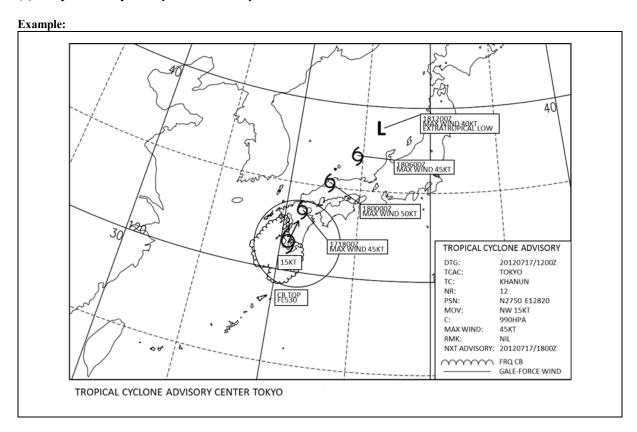
28/1200Z N2440 E12105

80KT RMK: NIL.

NXT MSG: 20080927/1800Z =

<sup>\* 6</sup> hour and 18 hour forecasts are added from 22 May 2008.

## (7) Graphical Tropical Cyclone Advisory for SIGMET



# Appendix 7 Specifications of JMA's NWP Models (GSM, GEPS)

The Global Spectral Model (GSM) and the Global Ensemble Prediction System (GEPS) are used in JMA as a primary basis for TC forecasts. The general specifications of GSM and GEPS are summarized in Table A7.1.

Table A7.1 Specifications of GSM and GEPS

NWP Models	GSM (Global Spectral Model), TQ959L128	GEPS (Global Ensemble Prediction System), TQ479L128
Resolution	13 km, 128 layers (Top: 0.01hPa)	27 km, 128 layers (Top: 0.01hPa)
Area	Global	Global
Method for	Global Data Assimilation System	Unperturbed condition: Truncated
initial value	(Hybrid-4DVAR)	GSM initial condition
	Outer resolution: TQ959L128	Initial perturbation: LETKF-based
	Inner resolution: TL319L128	perturbation and SV-based
	Window: Init-3h to Init + 3h	perturbation
		Ensemble size: 51 (50 perturbed
		members and 1 control member)
		SV target areas: Northern
		Hemisphere (30 – 90°N), Tropics
		$(30^{\circ}S - 30^{\circ}N)$ , Southern
		Hemisphere (90 – 30°S)
Forecast length	264 hours (00, 12 UTC)	432 hours (12 UTC)
(initial times)	132 hours (06, 18 UTC)	264 hours (00, UTC)
		132 hours (06, 18 UTC)
Operational as	14 March 2023	14 March 2023
from	17 Water 2023	17 Waten 2023

GSM (TQ959L128) has a horizontal resolution of approximately 13 km and 128 vertical layers. Details of the model can be found in JMA (2024) and Yonehara et al. (2023).

GEPS (TQ479L128) is an ensemble prediction system used for TC track forecasts up to five days ahead, one-week forecasts, early warning information on extreme weather, and one-month forecasts. It has 51 members and a horizontal resolution of approximately 27 km along with 128 vertical layers for the first 18 days of forecasts. Details of the system can be found in JMA (2024) and Ota et al. (2023). A combination of a Local Ensemble Transform Kalman Filter (LETKF; Hunt et al. 2007) and a singular vector (SV) method (Buizza and Palmer 1995) is employed for the initial perturbation setup. In addition, a stochastically perturbed physics tendency scheme (Buizza et al. 1999) is incorporated in consideration of model uncertainties associated with physical parameterizations, and a perturbation technique for sea surface temperature (SST) is incorporated to represent uncertainty in the prescribed SST.

[Recent upgrades to GSM, Global Data Assimilation System and GEPS] GSM:

- Horizontal resolution enhancement from 20 to 13 km (March 2023)
- Replacement of the source data set for orographic ancillary files (March 2023)
- Revision of non-orographic gravity wave, boundary layer, orographic drag and radiation (March

2023)

- Improvement of lake surface process (March 2023)

#### Global Data Assimilation System:

- Enhancement of snow depth analysis (March 2023)
- Assimilation of Suomi-NPP, NOAA-20/VIIRS AMV was started (March 2023)
- Assimilation of AMV and CSR from GOES-18 was started (May 2023)
- Assimilation of AMV and CSR from Meteosat-10 switching from Meteosat-11 was started (May 2023)

#### GEPS:

- Incorporation of the latest GSM (March 2023)
- Enhancement of SST boundary conditions (March 2023)

#### [References]

- Buizza, R., M. Miller, and T. N. Palmer, 1999: Stochastic representation of model uncertainties in the ECMWF Ensemble Prediction System. Quart. J. Roy. Meteor. Soc., 125, 2887–2908.
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- Hunt, B. R., E. J. Kostelich and I. Szunyogh, 2007: Efficient data assimilation for spatiotemporal chaos: a local ensemble transform Kalman filter. Physica. D., 230, 112 126.
- Japan Meteorological Agency, 2024: Outline of the Operational Numerical Weather Prediction at the Japan Meteorological Agency. Japan Meteorological Agency, Tokyo, Japan.
- Ota, Y., J. Chiba, Y. Ichikawa, H. Oashi, T. Takakura and H. Yamaguchi, 2023: Upgrade of JMA's Global Ensemble Prediction System. WGNE Res. Activ. Earth system Modell., 53, 06.11-12.
- Yonehara, H., Y. Kuroki, M. Ujiie, C. Matsukawa, T. Kanehama, R. Nagasawa, K. Ochi, M. Higuchi, Y. Ichikawa, R. Sekiguchi and S. Hirahara, 2023: Upgrade of JMA's Operational Global Numerical Weather Prediction System. WGNE Res. Activ. Earth system Modell., 53, 06.15-16.

# Appendix 8 Products on WIS GISC Tokyo Server

(Available at https://www.wis-jma.go.jp/cms/)

## NWP products (GSM and GEPS with GRIB formatted data)

Model	GSM	GSM	GSM
Area and resolution	Whole globe, 1.25°×1.25°	20°S–60°N, 60°E–160°W 1.25°×1.25°	Whole globe, 2.5°×2.5°
Levels and elements	10 hPa: Z, U, V, T 20 hPa: Z, U, V, T 30 hPa: Z, U, V, T 50 hPa: Z, U, V, T 70 hPa: Z, U, V, T 100 hPa: Z, U, V, T 150 hPa: Z, U, V, T 200 hPa: Z, U, V, T 200 hPa: Z, U, V, T, Ψ, χ 250 hPa: Z, U, V, T, H, ω 400 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 700 hPa: Z, U, V, T, H, ω 850 hPa: Z, U, V, T, H, ω 850 hPa: Z, U, V, T, H, ω 925 hPa: Z, U, V, T, H, ω 1000 hPa: Z, U, V, T, H, ω Surface: P, U, V, T, H, R†	10 hPa: Z, U, V, T 20 hPa: Z, U, V, T 30 hPa: Z, U, V, T 50 hPa: Z, U, V, T 70 hPa: Z, U, V, T 100 hPa: Z, U, V, T 150 hPa: Z, U, V, T 200 hPa: Z, U, V, T 200 hPa: Z, U, V, T 300 hPa: Z, U, V, T 300 hPa: Z, U, V, T, D 400 hPa: Z, U, V, T, D 500 hPa: Z, U, V, T, D 500 hPa: Z, U, V, T, D 500 hPa: Z, U, V, T, D \$500 hPa: Z, U, V, T, D \$500 hPa: Z, U, V, T, D \$500 hPa: Z, U, V, T, D, ω 1000 hPa: Z, U, V, T, D, ω 1000 hPa: Z, U, V, T, D Surface: P, U, V, T, D	10 hPa: Z*, U*, V*, T* 20 hPa: Z*, U*, V*, T* 30 hPa: Z°, U°, V°, T° 50 hPa: Z°, U°, V°, T° 70 hPa: Z°, U°, V°, T° 100 hPa: Z°, U°, V°, T° 150 hPa: Z*, U*, V*, T* 200 hPa: Z, U, V, T 250 hPa: Z, U, V, T 300 hPa: Z, U, V, T, D*; 400 hPa: Z, U, V, T, D*; 500 hPa: Z, U, V, T, D*; 700 hPa: Z, U, V, T, D*; 700 hPa: Z, U, V, T, D 850 hPa: Z, U, V, T, D 1000 hPa: Z, U*, V*, T*, D*; Surface: P, U, V, T, D*; R†
Forecast hours	0–84 every 6 hours and 96–192 every 12 hours for 12UTC initial † Except analysis	0-84 (every 6 hours)  § 96-192 (every 24 hours) for 12UTC initial  ¶90-192 (every 6 hours) for 12UTC initial	0–72 every 24 hours and 96–192 every 24 hours for 12UTC ° 0–120 for 12UTC † Except analysis * Analysis only
Initial times	00, 06, 12, 18UTC	00, 06, 12, 18UTC	00UTC and 12UTC ‡ 00UTC only

Model	GEPS
Area and resolution	Whole globe, 2.5°×2.5°
Levels and elements	250 hPa: μU, σU, μV, σV 500 hPa: μZ, σZ 850 hPa: μU, σU, μV, σV, μT, σT 1000 hPa: μZ, σZ Surface: μP, σP
Forecast hours	0–192 every 12 hours
Initial times	00, 12UTC

## NWP products (GSM and GEPS with GRIB2 formatted data)

Model	GSM	GSM	GSM
Area and resolution	5S-90N and 30E-165W, Whole globe 0.25° × 0.25°	5S-90N and 30E-165W, Whole globe 0.5° × 0.5°	Whole globe $1.25^{\circ} \times 1.25^{\circ}$
Levels and elements	Surface: U, V, T, H, P, Ps, R, Cla, Clh, Clm, Cll	10 hPa: Z, U, V, T, H, ω 20 hPa: Z, U, V, T, H, ω 30 hPa: Z, U, V, T, H, ω 50 hPa: Z, U, V, T, H, ω 70 hPa: Z, U, V, T, H, ω 100 hPa: Z, U, V, T, H, ω 150 hPa: Z, U, V, T, H, ω 200 hPa: Z, U, V, T, H, ω 200 hPa: Z, U, V, T, H, ω 300 hPa: Z, U, V, T, H, ω 300 hPa: Z, U, V, T, H, ω 400 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω 700 hPa: Z, U, V, T, H, ω 800 hPa: Z, U, V, T, H, ω 850 hPa: Z, U, V, T, H, ω 950 hPa: Z, U, V, T, H, ω 975 hPa: Z, U, V, T, H, ω 975 hPa: Z, U, V, T, H, ω 975 hPa: Z, U, V, T, H, ω Surface: U, V, T, H, P, Ps, R, Cla, Clh, Clm, Cll	10 hPa: Z, U, V, T 20 hPa: Z, U, V, T 30 hPa: Z, U, V, T 30 hPa: Z, U, V, T 50 hPa: Z, U, V, T 70 hPa: Z, U, V, T 100 hPa: Z, U, V, T 150 hPa: Z, U, V, T 200 hPa: Z, U, V, T, ψ, χ 250 hPa: Z, U, V, T, ψ, χ 300 hPa: Z, U, V, T, H, ω 400 hPa: Z, U, V, T, H, ω 500 hPa: Z, U, V, T, H, ω, ζ 600 hPa: Z, U, V, T, H, ω, ζ 600 hPa: Z, U, V, T, H, ω, ζ, ∇ 850 hPa: Z, U, V, T, H, ω, ψ, χ 925 hPa: Z, U, V, T, H, ω, ψ, χ 925 hPa: Z, U, V, T, H, ω, ζ, ∇ 1000 hPa: Z, U, V, T, H, ω Surface: P, U, V, T, H, R
Forecast hours	0–132 (every 3 hours) 138–264 (every 6 hours) are available for 00 UTC and 12 UTC initial	0–132 (every 3 hours) 138–264 (every 6 hours) are available for 00 UTC and 12 UTC initial	0-132 (every 3 hours) 138-264 (every 6 hours) are available for 00 UTC and 12 UTC initial
Initial times	00, 06, 12 and 18 UTC	00, 06, 12 and 18 UTC	00, 06, 12 and 18 UTC

Model	GEPS		
Area and resolution	Whole globe, 1.25°×1.25°		
Levels and elements	250 hPa: μU, σU, μV, σV 500 hPa: μZ, σZ 850 hPa: μU, σU, μV, σV, μT, σT 1000 hPa: μZ, σZ Surface: μP, σP Probability of precipitation [1,5,10,25,50,100 mm/24hour], Probability of 10m sustained wind and gusts[10,15,25 m/s], Probability of temperature anomalies [±1, ±1.5, ±2σ]		
Forecast hours	0-264 every 12 hours		
Initial times	00UTC and 12UTC		

Notes:	Z: geopotential height	U: eastward wind	V: northward wind
	T: temperature	D: dewpoint depression	H: relative humidity
	ω: vertical velocity	ζ: vorticity	ψ: stream function
	χ: velocity potential	$\nabla$ : divergence	P: sea level pressure
	Ps: pressure	R: rainfall	Cla: total cloudiness
	Clh: cloudiness (upper layer)	Clm: cloudiness (middle laye	er)
	Cll: aloudings (lower lover)		

Cll: cloudiness (lower layer)

The prefixes  $\mu$  and  $\sigma$  represent the average and standard deviation of ensemble prediction results respectively. The symbols °, \*, ¶, §, ‡ and † indicate limitations on forecast hours or initial time as shown in the tables.

# Other products

Data	Contents / frequency (initial time)		
	High density atmospheric motion vectors (BUFR) Himawari-8/9 (VIS, IR, WVx3: every hour), 60S-60N, 90E-170W		
Satellite products	Clear Sky Radiance (CSR) data (BUFR)		
	Himawari-8/9 radiances and brightness temperatures		
	averaged over cloud-free pixels: every hour		
Tropical cyclone	Tropical cyclone related information (BUFR)		
Information	• tropical cyclone analysis data (00, 06, 12 and 18 UTC)		
	Global Wave Model (GRIB2)		
	• significant wave height		
	prevailing wave period		
Wave data	wave direction		
	Forecast hours:		
	0–84 every 6 hours (00, 06 and 18UTC)		
	0–84 every 6 hours and 96-192 every 12 hours (12 UTC)		
	(a) Surface data (TAC/TDCF)		
Observational	SYNOP, SHIP, BUOY: Mostly 4 times a day		
data	(b) Upper-air data (TAC/TDCF)		
	TEMP (parts A-D), PILOT (parts A-D): Mostly twice a day		
	(a) Satellite imagery (SATAID)		
	Himawari-8/9		
SATAID service	(b) Observation data (SATAID)		
	SYNOP, SHIP, METAR, TEMP (A, B) and ASCAT sea-surface wind		
	(c) NWP products (SATAID)		
	GSM		
	(Available at https://www.wis-jma.go.jp/cms/sataid/)		

# Appendix 9 RSMC Tokyo Products and Services Provided Through the Internet

List of products provided on the Numerical Typhoon Prediction (NTP) website

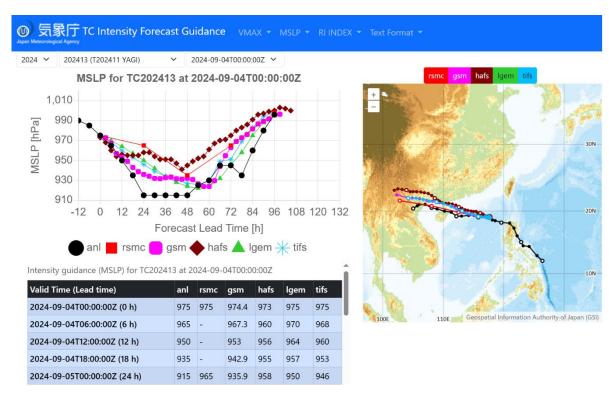
Products	Frequency	Details		
RSMC Advisories				
RSMC TC Advisory	At least 8 times/day	The Center's TC analysis and forecasts up to 120 hours ahead (linked to the JMA website at https://www.jma.go.jp/en/typh/)		
Storm Wind Probability Map	4 times/day	• Probabilistic forecast map for sustained wind of 50-kt or more for 1, 2, 3, 4 and 5 days ahead		
Prognostic Reasoning	4 times/day	RSMC Tokyo Tropical Cyclone Prognostic Reasoning (WTPQ3X)		
Graphical TC Advisory	4 times/day	Graphical TC Advisory including the Center's TC analysis, track and intensity forecasts up to 24-hours and horizontal extents of cumulonimbus cloud and cloud top height associated with TCs potentially affecting aviation safety (linked to the Tropical Cyclone Advisory Center Tokyo Website)		
Remote Sensing	3			
Satellite Analysis	At least 4 times/day	Results and historical logs of the Center's TC analysis conducted using satellite images (Conventional Dvorak analysis and Early-stage Dvorak analysis)		
Satellite Imagery	Every 10 minutes	Satellite imagery of Himawari-8/9 (linked to the JMA website at https://www.jma.go.jp/bosai/map.html#elem=ir⟨=en&contents=himawari)		
Satellite Microwave Products		<ul> <li>TC snapshot images</li> <li>Warm-core-based TC intensity estimates</li> <li>Weighted consensus TC intensity estimates made using Dvorak analysis and satellite microwave warm-core-based intensity estimates</li> </ul>		
Sea-surface AMV (ASWind)	Every 10 / 30 minutes	AMV-based Sea-surface Wind in the vicinity of TC (linked to the Meteorological Satellite Center web site)		
Radar Composite Imagery	Every hour	Radar composite imagery of the Typhoon Committee Regional Radar Network		
Atmospheric Ci	rculation			
Weather Charts	4 times/day	Weather maps for surface analysis, 24- and 48-hour forecasts (linked to the JMA website at https://www.jma.go.jp/en/g3/)		
NWP Multi Center Weather Charts	Twice/day	• Mean sea level pressure and 500 hPa Geopotential height (up to 168 hours) of deterministic NWP models from nine centers (BoM, CMA, CMC, DWD, ECMWF, KMA, NCEP, UKMO and JMA)		
JMA GSM Analysis and Forecast	4 times/day	<ul> <li>Upper-air analysis and forecast data based on JMA-GSM</li> <li>Streamlines at 850, 500 and 200 hPa</li> <li>Divergence at 200 hPa</li> <li>Velocity potential at 200 hPa</li> <li>Vertical Velocity in Pressure Coordinate at 500 hPa</li> <li>Dew Point Depression at 600 hPa</li> <li>Curvature Vorticity at 850 hPa</li> <li>Vertical wind shear between 200 and 850 hPa</li> <li>Sea Level Pressure</li> <li>Genesis Potential Index</li> </ul>		
MJO Phase Diagram	Daily	<ul> <li>MJO phase and amplitude diagram</li> <li>MJO Hovmöller diagram</li> <li>(linked to the Tokyo Climate Center web site)</li> </ul>		

Products	Frequency	Details			
Asian Monsoon Monitoring Indices	Daily, only during Apr Oct.	Time series of vertical wind shear, OLR and other indices associated with SW Asian Monsoon (linked to the Tokyo Climate Center web site)			
Ocean Conditi	Ocean Condition				
SST	Once/day	Sea surface temperature and related differences from 24 hours ago			
ТСНР	Once/day	Tropical cyclone heat potential and related differences from 24 hours ago			
Numerical TC	Numerical TC Prediction				
Track Bulletin	4 times/day	RSMC Tokyo Tropical Cyclone Track Forecast Bulletin     Track forecast by GSM (FXPQ2X)     Track forecast by GEPS (FXPQ3X)			
TC intensity (TIFS monitor)	4 times/day	• TC Intensity prediction of TIFS, LGEM, HAFS and GSM			
TC Track Prediction	4 times/day	<ul> <li>TC track prediction of deterministic NWP models from nine centers (BoM, CMA, CMC, DWD, ECMWF, KMA, NCEP, UKMO and JMA)</li> <li>TC track prediction of EPS models from four centers (ECMWF, NCEP, UKMO and JMA)</li> </ul>			
TC Activity Prediction	Twice/day	• Two- and five-day TC activity prediction maps based on EPS models from four centers (ECMWF, UKMO, NCEP and JMA) and a related consensus			
TC forecast Verification	4 times/day	• Real-time verification of TC track and intensity forecast of numerical forecast models and related products.			
Marine Foreca	st				
Storm Surge Forecasts	4 times/day	<ul> <li>Distribution maps of storm surge for the Center's TC track forecast and each of five TC track forecasts selected from GEPS ensemble members and maximum storm surge among these six TC track forecasts (up to 132 hours)</li> <li>Time-series storm surge forecast charts for the Center's TC track forecast and TC track forecasts from GEPS ensemble prediction (up to 132 hours)</li> <li>Time-series representations of sea levels, related anomalies, and wind and sea level pressure based on official forecasts for stations of Typhoon Committee Members (up to 132 hours)</li> <li>Time-series storm surge forecast charts for the Center's ensemble TC track forecasts with box-and-whisker plots and probabilities of 1-, 2- and 3m-exceeding storm surges (up to 132 hours)</li> </ul>			
Ocean Wave Forecasts	Twice/day	<ul> <li>Distribution maps for ensemble mean, maximum, probability of exceeding various thresholds and ensemble spread of wave height and period based on the Wave Ensemble System (WENS) (up to 264 hours)</li> <li>Time-series representations with box-and-whisker plots for wave height/period and probability of exceeding various wave height/period thresholds based on the WENS (up to 264 hours)</li> </ul>			

List of services provided on the TC communication platform

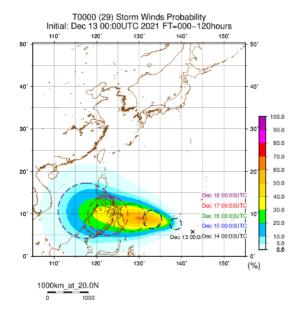
Services	Details
	Advance notice on TC status change from the Center
Advance notice	*Supplemental information to RSMC advisories (It may not be provided in certain situations and
	should not be considered as an official RSMC advisory and/or its replacement)
Enhanced	A platform on which Committee Members can post inquiries or comments related to tropical cyclone
communication	analysis and forecasts

### RSMC Tokyo - Typhoon Center product examples



### Website on the TIFS (Typhoon Intensity Forecast scheme based on SHIPS) monitor<sup>11</sup>

The upper figure shows TIFS, LGEM, HAFS and GSM intensity prediction values at each initial time for individual TCs with analysis data in line graphs as well as a map of tracks. The table shows intensity prediction values at each valid time with analysis data.



Five-day storm wind probability product (50 kt and above) for Tropical Depressions (TDs) expected to reach tropical storm (TS) intensity or higher within 24 hours.

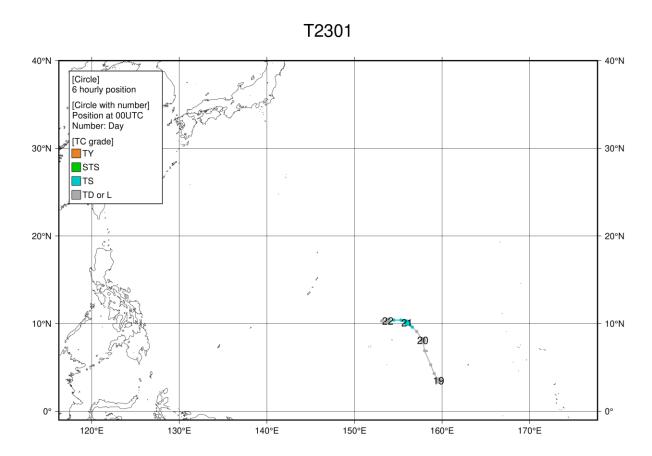
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<sup>&</sup>lt;sup>11</sup> Website updated in March 2024.

# Appendix 10 Tropical Cyclones in 2023

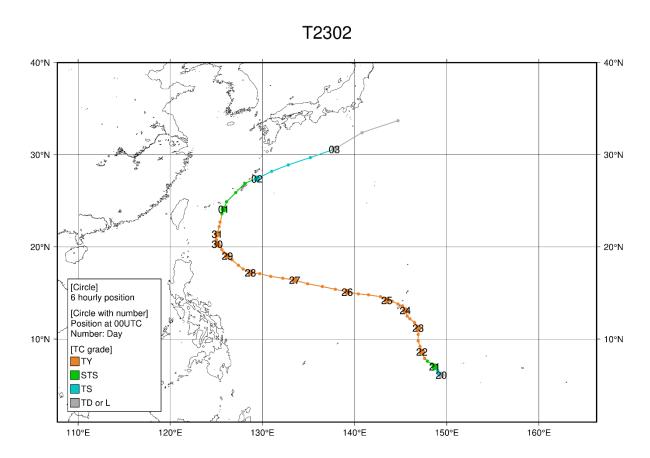
### **SANVU (2301)**

SANVU formed as a tropical depression (TD) over the sea southwest of the Marshall Islands at 00 UTC on 19 April 2023 and moved north-northwestward. SANVU was upgraded to tropical storm (TS) intensity at 12 UTC the next day over the sea around the Marshall Islands and moved northwestward. Gradually turning west-northwestward, it reached its peak intensity with maximum sustained winds of 45 kt and a central pressure of 996 hPa over the same waters at 06 UTC on 21 April. After moving westward, SANVU weakened to TD intensity over the sea around the Chuuk Islands at 00 UTC the next day. It dissipated over the same waters at 12 UTC on 22 April.



### **MAWAR (2302)**

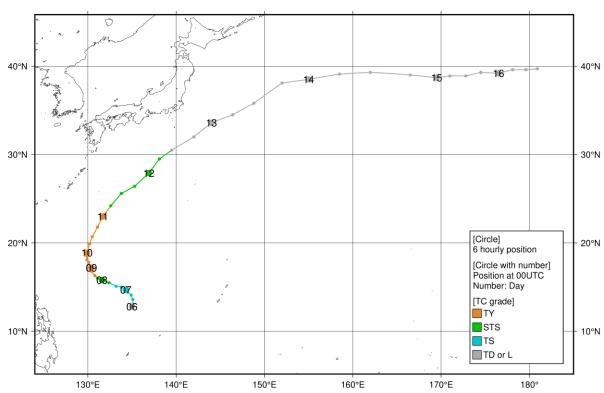
MAWAR formed as a tropical depression (TD) over the sea around the Caroline Islands at 18 UTC on 19 May 203 and moved westward. It was upgraded to tropical storm (TS) intensity over the same waters at 12 UTC on 20 May and moved northwestward. It was upgraded to severe tropical storm (STS) intensity at 00 UTC and was upgraded to typhoon (TY) intensity at 18 UTC on 21 May over the same waters and moved northwestward. It reached its peak intensity with maximum sustained winds of 115 kt and a central pressure of 900 hPa near the Mariana Islands at 12 UTC on 25 May and moved westward. After turning northward, it was downgraded to STS intensity over the sea south of Okinawa at 18 UTC on 31 May and moved northward. It was weakened to TS intensity over the same waters at 00 UTC on 2 June and moved east-northeastward. It transitioned into an extratropical cyclone over the sea south of Japan at 00 UTC on 3 June. It dissipated over the sea east of Japan at 18 UTC on 3 June.



## **Guchol (2303)**

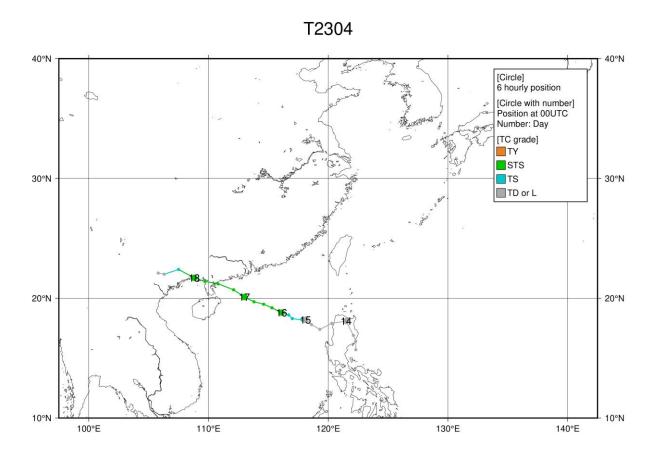
Guchol formed as a tropical depression (TD) over the sea east of the Philippines at 00 UTC on 06 June 2023 and moved northward. It was upgraded to tropical storm (TS) intensity over the same waters at 12 UTC the same day. After moving west-northwestward, it was upgraded to severe tropical storm (STS) intensity at 18 UTC on 07 June and further upgraded to typhoon (TY) intensity at 12 UTC next day. Gradually turning northeastward slowly, it reached its peak intensity with maximum sustained winds of 80 kt and a central pressure of 960 hPa over the sea east of the Philippines at 18 UTC on 09 June. Accelerating northeastward over the sea south of Japan, it was downgraded to STS intensity at 06 UTC on 11 June and transitioned into an extratropical cyclone by 12 UTC next day. After continuously moving northeastward and eastward, it entered the sea south of Aleutians and crossed longitude 180 degrees east before 18 UTC on 16 June.





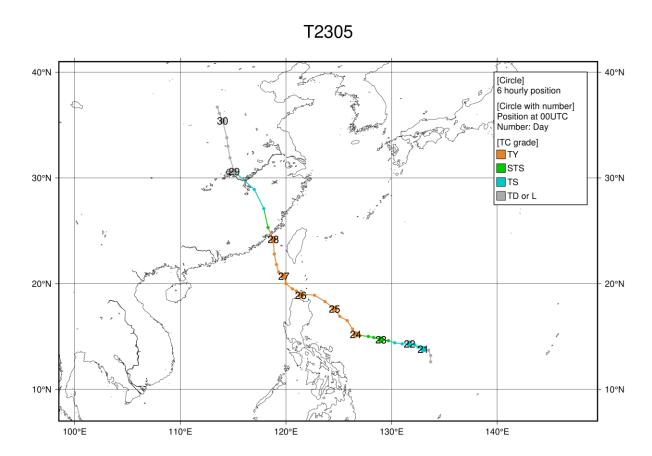
## **TALIM (2304)**

TALIM formed as a tropical depression (TD) over the sea east of the Philippines at 06 UTC on 13 July 2023 and moved north-northwestward. It hit the Philippines with TD intensity around 12 UTC the same day before turning westward on 14 July. After entering the South China Sea, it was upgraded to tropical storm (TS) intensity over the same waters at 06 UTC on 15 July. It was further upgraded to severe tropical storm (STS) intensity over the same waters at 00 UTC on 16 July. It reached its peak intensity with maximum sustained winds of 60 kt and a central pressure of 970 hPa over the same waters at 00 UTC on 17 July. It hit the Leizhou Peninsula with STS intensity by 18 UTC the same day. It was downgraded to TS intensity in South China at 06 UTC on 18 July and then weakened to TD intensity in Viet Nam at 12 UTC the same day. TALIM dissipated in the same area at 00 UTC on 19 July.



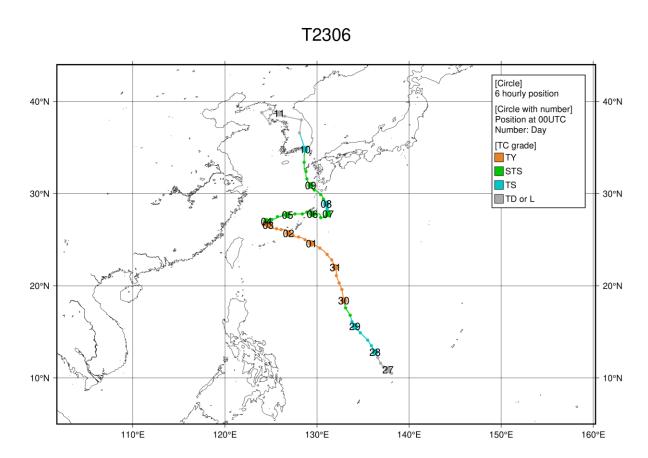
## **DOKSURI (2305)**

DOKSURI formed as a tropical depression (TD) over the sea east of the Philippines at 06 UTC on 20 July 2023 and moved northward and then westward. Moving westward, over the same waters, it was upgraded to tropical storm (TS) intensity at 00 UTC the next day and was further upgraded to typhoon (TY) intensity at 18 UTC on 23 July. After turning sharply northwestward, over the same waters, it developed rapidly and reached its peak intensity with maximum sustained winds of 100 kt and a central pressure of 925 hPa at 18 UTC on 24 July. After reaching its peak intensity, DOKSRI gradually turned westward and entered the Bashi channel. Gradually weakening, it turned northward and entered the Taiwan strait before it hit South China with TY intensity early on 28 July. Rapidly weakening, it moved north-northwestward and downgraded to TD intensity in Central China at 00 UTC the next day and then dissipated in North China at 18UTC on 30 July.



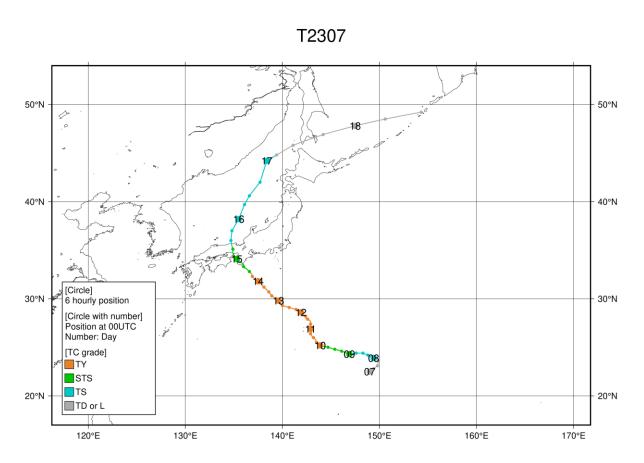
#### **KHANUN (2306)**

KHANUN formed as a tropical depression (TD) over the sea east of the Philippines at 18 UTC on 26 July 2023 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the same waters at 00 UTC on 28 July, to severe tropical storm (STS) intensity at 12 UTC the next day and to typhoon (TY) intensity at 00 UTC on 30 July while moving northwestward to northward. It reached its peak intensity with maximum sustained winds of 95 kt and a central pressure of 930 hPa over the sea south of Okinawa Island at 00 UTC on 01 August. While gradually turning westward and entering the East China Sea, it gradually weakened. It remained almost stationary over the same waters and then moved eastward. It developed again over the sea south of Kyushu Island at 06 UTC on 08 August while gradually turning northward. It hit Korea with TS intensity after 00 UTC on 10 August and transformed into an extratropical cyclone by 06 UTC the same day. After turning west-northwestward and entering the Yellow Sea on 11 August, it dissipated at 00UTC the next day.



#### LAN (2307)

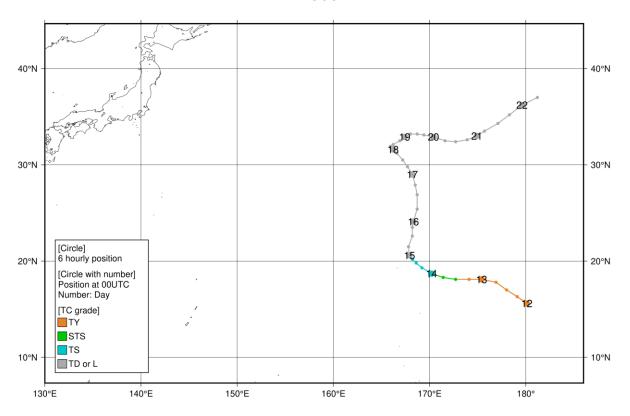
LAN formed as a tropical depression (TD) over the sea west of Minamitorishima Island at 00 UTC on 07 August 2023 and moved northeastward. It was upgraded to tropical storm (TS) intensity over the same waters at 00 UTC on 08 August and moved west-northwestward. It was upgraded to severe tropical storm (STS) intensity over the sea around the Ogasawara Islands at 00 UTC on 09 August and moved west-northwestward. It was upgraded to typhoon (TY) intensity over the same waters at 00 UTC on 10 August and moved northwestward. It reached its peak intensity with maximum sustained winds of 90 kt and a central pressure of 940 hPa over the same waters at 18 UTC the same day and moved northwestward. It turned west-northwestward around 00 UTC on 12 August over the same waters. It was downgraded to STS intensity over the sea south of Japan at 12 UTC on 14 August and moved north-northwestward. It made landfall near Shionomisaki, Wakayama Prefecture before 20 UTC on 14 August and made landfall again near Akashi city, Hyogo Prefecture around 04 UTC on 15 August respectively with STS intensity and moved northwestward. It weakened to TS intensity in Hyogo Prefecture about 5 hours later and moved northward. It turned north-northeastward and transitioned into an extratropical cyclone over the Sea of Japan by 06 UTC on 17 August and moved northeastward. It dissipated over the sea around the Kuril Islands at 18 UTC on 18 August.



#### **DORA (2308)**

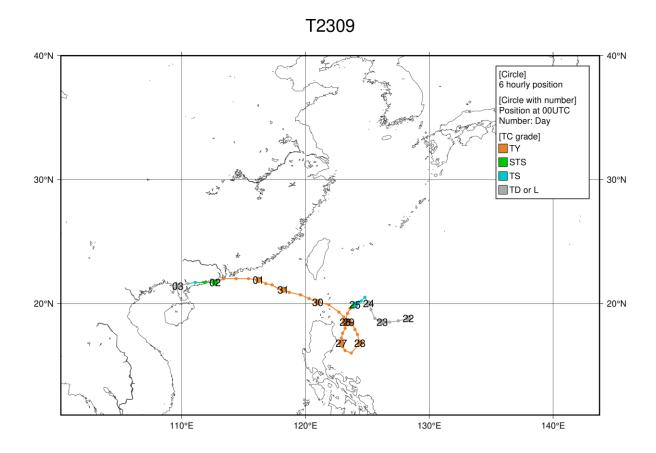
DORA crossed longitude 180 degrees east over the sea south of Midways with typhoon (TY) intensity after 00 UTC on 12 August 2023 and entered the western North Pacific. After reaching its peak intensity with maximum sustained winds of 75 kt and a central pressure of 980 hPa at 06 UTC the same day, it moved west-northwestward and then moved westward weakening in intensity. It was downgraded to severe tropical storm (STS) intensity east of Wake Island at 12 UTC on 13 August and downgraded to tropical storm (TS) intensity at 00UTC the next day. Gradually turning northward, it weakened to tropical depression (TD) intensity around Wake Island at 00 UTC on 15 August. It moved northward and then turned sharply eastward over the sea far east of Japan on 18 August. Moving east-northeastward, it transitioned into an extratropical cyclone northwest of Midways by 12 UTC on 21 August. It entered the sea south of Aleutians and crossed longitude 180 degrees east before 06 UTC the next day.





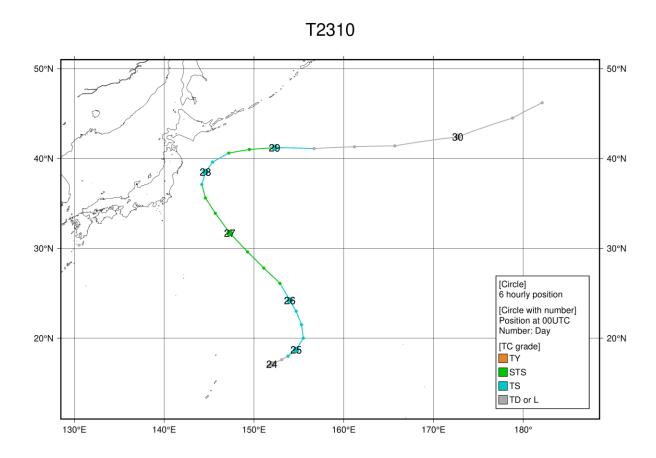
## **SAOLA (2309)**

SAOLA formed as a tropical depression (TD) over the sea east of the Philippines at 00 UTC on 22 August 2023 and moved westward. It was upgraded to tropical storm (TS) intensity over the sea south of Okinawa at 06 UTC on 24 August and moved southwestward. It developed rapidly and was upgraded to typhoon (TY) intensity over the sea east of the Philippines at 12 UTC on 25 August. It turned in a counterclockwise direction to circle from 26 to 29 August. It reached its peak intensity with maximum sustained winds of 105 kt and a central pressure of 920 hPa over the Bashi Channel at 00 UTC on 30 August. It downgraded to severe tropical storm (STS) intensity over the sea south of South China at 00 UTC on 2 September and then hit the South China six hours later. It downgraded to TS intensity in the same area at 12 UTC on 2 September and then weakened to TD intensity six hours later. SAOLA dissipated over the Gulf of Tonkin at 18 UTC on 03 September.



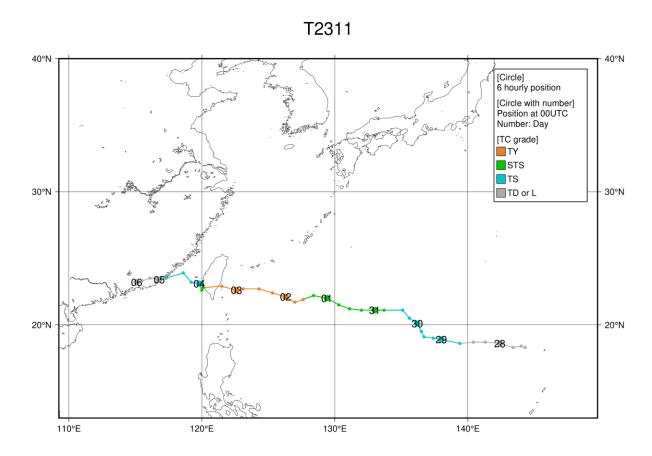
#### **DAMREY (2310)**

DAMREY formed as a tropical depression (TD) over the sea south of Minamitorishima Island at 18 UTC on 23 August 2023 and moved east-northeastward. It was upgraded to tropical storm (TS) intensity over the same waters at 18 UTC the next day. It gradually turned northwestward and was further upgraded to severe tropical storm (STS) intensity and reached its peak intensity with maximum sustained winds of 50 kt and a central pressure of 985 hPa around Minamitorishima Island at 06 UTC on 26 August. Keeping its northwestward track, it was downgraded to TS intensity east of Japan at 18 UTC the next day. It gradually turned to eastward and temporally developed to STS intensity again before it transitioned into an extratropical cyclone far off east of Japan by 06 UTC on 29 August. Gradually turning northeastward and entering the sea south of Aleutians, it crossed longitude 180 degrees east before 12UTC the next day.



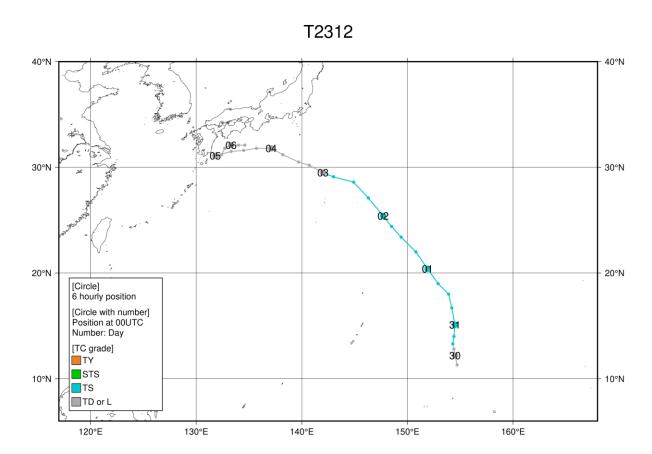
## **HAIKUI (2311)**

HAIKUI formed as a tropical depression (TD) over the sea west of the Mariana Islands at 06 UTC on 27 August 2023 and moved westward. It was upgraded to tropical storm (TS) intensity over the sea east of the Philippines at 18 UTC the next day. It moved northwestward and was upgraded to severe tropical storm (STS) intensity over the sea south of Japan at 18 UTC on 30 August. Moving westward, it was further upgraded typhoon (TY) intensity over the sea south of Okinawa at 12 UTC on 1 September and reached its peak intensity with maximum sustained winds of 85 kt and a central pressure of 945 hPa over the same waters at 18 UTC the next day. It crossed Taiwan with TY intensity on 3 September and weakened in intensity. It hit the south China and weakened to TD intensity at 00 UTC on 5 September, and then dissipated at 06 UTC the next day.



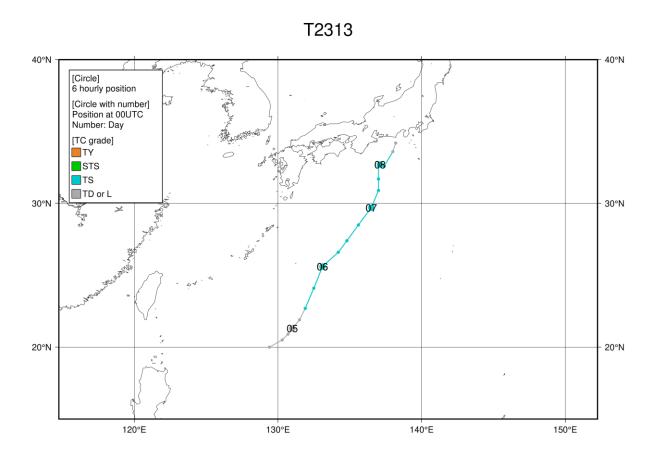
## **KIROGI (2312)**

KIROGI formed as a tropical depression (TD) around the Chuuk Islands at 18 UTC on 29 August 2023 and moved northward. It was upgraded to tropical storm (TS) intensity over the same waters at 12 UTC on 30 August and moved northward. It reached its peak intensity with maximum sustained winds of 45 kt and a central pressure of 994 hPa over the sea south of Minamitorishima at 06 UTC on 31 August and moved northward. It weakened to TD intensity over the sea around the Ogasawara Islands at 00 UTC on 3 September and moved west-northwestward. It turned east-northeastward around 12 UTC on 5 September and dissipated over the sea south of Shikoku at 18 UTC on 6 September.



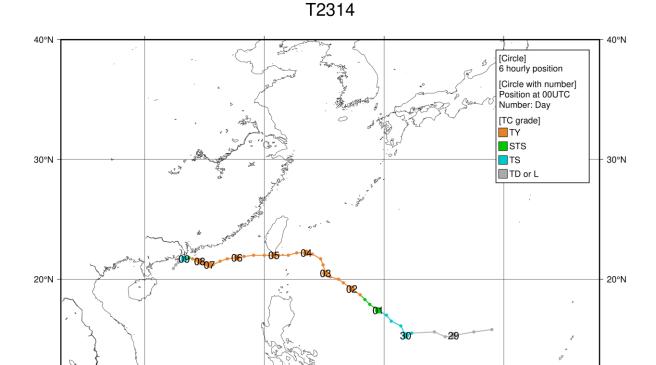
## **YUN-YEUNG (2313)**

YUN-YEUNG formed as a tropical depression (TD) over the sea south of Okinawa at 06 UTC on 4 September 2023. It moved northeastward and was upgraded to tropical storm (TS) intensity over the sea south of Japan at 12 UTC the next day. Moving north-northeastward over the same waters, it reached its peak intensity with maximum sustained winds of 40 kt and a central pressure of 998 hPa at 06 UTC on 6 September. After continuing to move north-northeastward and then moving northward, it remained almost stationary south of the Kii Peninsula around 00 UTC on 8 September. Moving again north-northeastward, it weakened to TD intensity over the sea south of Shizuoka Prefecture at 12 UTC on 8 September and dissipated at 00 UTC the next day.



## **KOINU (2314)**

KOINU formed as a tropical depression (TD) over the sea east of the Philippines at 12 UTC on 28 September 2023 and moved westward. It was upgraded to tropical storm (TS) intensity over the same waters at 18 UTC on 29 September before turning sharply northwestward. It was upgraded to typhoon (TY) intensity at 18 UTC on 1 October. It reached its first peak intensity with maximum sustained winds of 90 kt and a central pressure of 940 hPa over the sea south of Okinawa at 18 UTC on 2 October. After turning westward, it gradually weakened from the second half of 3 October. It crossed south of Taiwan with TY intensity around 00 UTC on 5 October and weakened until 18 hours later. After developing again, it reached its second peak intensity with maximum sustained winds of 85 kt and a central pressure of 955 hPa over the South China Sea at 18 UTC on 6 October. KOINU rapidly weakened to TD intensity over the sea south of South China at 06 UTC on 09 October and then dissipated 18 hours later.



130°E

120°E

10°N

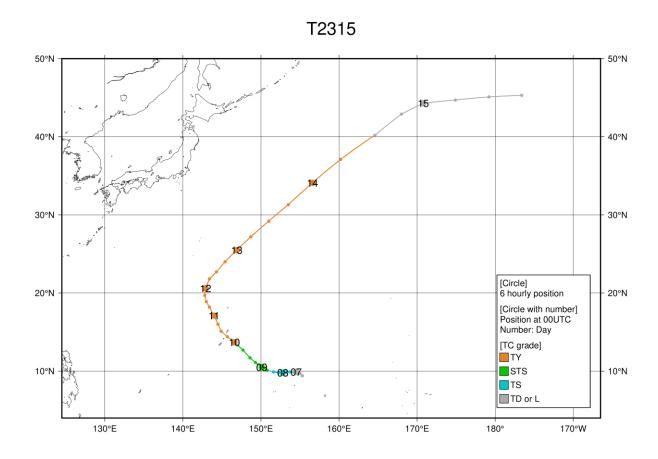
140°E

10°N

110°E

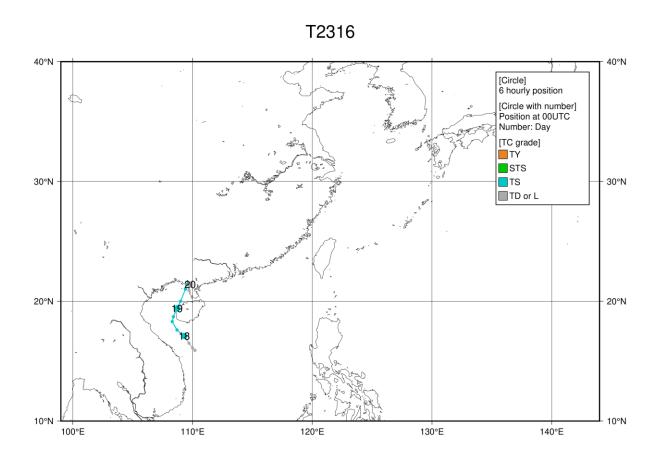
## **BOLAVEN (2315)**

BOLAVEN formed as a tropical depression (TD) over the sea west of Marshall Islands at 06 UTC on 6 October 2023 and moved northwestward slowly. Turning westward, it was upgraded to tropical storm (TS) intensity near the Chuuk Islands at 12 UTC the next day. It moved westward and was upgraded to severe tropical storm (STS) intensity over the same waters at 18 UTC on 8 October. It turned northwestward and was further upgraded to typhoon (TY) intensity near the Mariana Islands at 00 UTC on 10 October. After turning north-northwestward, it reached its peak intensity with maximum sustained winds of 115 kt and a central pressure of 905 hPa over the same waters at 12 UTC the next day. BOLAVEN turned northeastward and accelerated, transitioned into an extratropical cyclone far off east of Japan by 12 UTC on 14 October. It further moved northeastward and turned eastward and entered the sea south of Aleutians and crossed longitude 180 degrees east before 18 UTC the next day.



# **SANBA (2316)**

SANBA formed as a tropical depression (TD) over the South China Sea at 06 UTC on 17 October 2023 and moved northwestward. It was upgraded to tropical storm (TS) intensity over the same waters at 00 UTC the next day. After moving north-northeastward, it reached its peak intensity with maximum sustained winds of 40 kt and a central pressure of 1000 hPa over the Gulf of Tonkin at 12 UTC on 19 October. Turning eastward, it weakened to TD intensity over the same waters at 00 UTC on 20 October. After turning southward, it hit the Leizhou Peninsula and dissipated at 12 UTC the same day.



## **JELAWAT (2317)**

JELAWAT formed as a tropical depression (TD) around the Caroline Islands at 12 UTC on 15 December 2023 and moved westward. It was upgraded to tropical storm (TS) intensity at 06 UTC on 17 December and reached its peak intensity with maximum sustained winds of 35 kt and a central pressure of 1002 hPa over the sea east of Mindanao Island and moved westward. It weakened to TD intensity on the Mindanao Island at 00 UTC on 18 December. Moving westward, it entered the sea southwest of Mindanao Island at 06 UTC and dissipated at 12 UTC on 18 December.



